



IMPACT OF ALTERNATIVE DISPERSION MODEL VALIDATION METHODS:

A Case Study on the LNG Model Validation Database using DRIFT

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Regulation of LNG Facilities



- US Federal Regulation 49 CFR 193 on Liquefied Natural Gas (LNG) facilities
- NFPA 59A (2001) "Standard for the Production, Storage, and Handling of LNG"
- Applicants required to calculate size of exclusion zones, based on vapour cloud dispersion distance to ½ Lower Flammability Limit (LFL) for design spills
- Approved dispersion models (until 2011): DEGADIS, FEM3A
- Alternative dispersion models approved by US Pipelines and Hazardous Materials Safety Administration (PHMSA) using the NFPA LNG Model Evaluation Protocol



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LNG Model Evaluation Protocol

- 2007 LNG Model Evaluation Protocol (Ivings *et al.*, 2007)
- 2008 LNG Model Validation Database (Coldrick *et al.,* 2008)
- 2010 LNG Model Validation Database, Version 11 (Coldrick *et al.*, 2010) PHMSA Advisory Bulletin PHMSA-2010-0226
- 2011
- **DEGADIS 2.1 Evaluation (FERC, 2011)**
- 2012 V PHAST v6.6/6.7 Evaluation (PHMSA, 2011)
- 2013 FLACS v9.1r2 Evaluation (PHMSA, 2011)
- 2014
- 2015

2016 — LNG Model Validation Database, Version 12 (Stewart *et al.*, 2016)



LNG Model Validation Database

Trial Name	Sheet number in the Database	Trial number	Field (F) or Wind tunnel (WT)	Obstructed (O) or unobstructed (U)	Atmospheric stability	Substance released	Dispersion over water (W) or land (L)
Maplin	1	27	F	U	C-D	LNG	W
Sands, 1980	2	34			D		
	3	35			D		
Burro, 1980	4	3	F	U	В	LNG	L
	5	7			D		
	6	8			E		
	7	9			D		
Coyote, 1981	8	3	F	U	B-C	LNG	L
	9	5			C-D		
Falses	10	6	-	0	D	LNC.	
1987	11	1	F	0	G	LING	L
	12	4			D.F		
Thorney	14	45	F	U	F-F	Freon 12 &	
Island		10	· ·		2.1	Nitrogen	-
1982-4	15	47			F		
CHRC, 2006	16	A	WT	U	D	Carbon Dioxide	L
	17	В		0	D		
	18	С		0	D		
BA- Hamburg	19	(DA0120)	WT	U	D	Sulfur Hexafluoride	L
	20	(DAT223)		U	D		
	21	Upwind fence (039051)		0	D		
	22	Upwind fence (039072)		0	D		
	23	Downwind fence (DA0501)		0	D		
	24	Downwind fence (DA0532)		0	D		
	25	Circular fence (039094/039095)		0	D		
	26	Circular fence (039097)		0	D		
	27	Slope (DAT647)		U	D		
	28	Slope (DAT631)		U	D		
	29	Slope (DAT632)		U	D		
	30	Slope (DAT637)		U	D		
BA-TNO	31	TUV01	WT	U	D	Sulfur Hexafluoride	L
	32	TUV02		0	D		
	33	FLS		U	D		

	Δ	В	C		_				
1	Trial Namo								
2	Durro 2								
4	Test 1								
3	lest identifier								
4	803								
5	Date of test								
6	July 2 1980								
7	Origin of data								
8	MDA/Rediphem/Ermak et al 1988								
9	Date of inclusion, last revision								
10	August 12 2008 August 07 2009								
11	Description of test	1							
	Centinueus release of 24 m ²² 2 LNC into 59	å mismeter weter henin							
	Continuous release of 34 m - 5 LING Into 56	m diameter water basin							
10									
12									
13	TRIAL DATA								
14									
15	Substance released		Units						
16	Substance	LNG							
17	Composition	92.5% methane, 6.2%	mol%						
18	Molecular weight	17.26	ka/kmol						
10	Density	/130 7	ka/m**3						
20	Normal bailing point	432.1	Ngrill J						
20	Normal bolling point	111.6	N.						
21	Latent neat of evaporation	511900	Ј/кд						
22	Specific heat for vapor	2238	J/kg-K						
23	Specific heat for liquid	3348.5	J/kg-K						
24					-				
25									
26	Release conditions		Units						
27	Exit pressure	not applicable							
28	Spill tomporature	111.6	K						
20	Opin temperature	last mean and	K			· · · · · · · · · ·	Maximum arc-wise	0	
29	Source diameter	not measured				Averaging time (s)	concentration (%)	Cloud width (m)	
30	Source elevation	-1.5	m			1	22.4		
31	Source type	evaporating pool				1	9.0		
32	Storage phase	liquid				100	7.9	20.86	
33	Spill containment diameter	58	m			100	6.1	u/a	
34	Spill rate	87.98	ka/s						
35	Spill duration	167	s						
36	Total quantity released	14712	ka			7	Averaging time (s)	Concentration (%)	Temperature (K)
27	Initial concentration	100	0/				r tronging time (o)	concentration (10)	remperatore (rt)
31	initial concentration	100	/0		6	1	1	8.6	
20	Exit pipe neight above water surface	1.0	m		7	1	1	11.2	
39					9	1	1	22.4	
40					9	1	1	20.3	
41	Atmospheric conditions		Units		7	1	1	22.4	
42	Ambient temperature	307.75	К	1	8	1	1	6.8	
43	Measuring height of ambient temperature	1	m		0	1	100	9.0	207
		18	40		-40.6	1	100	0.4	307
		19	55.6		-14.9	1	100	6.9	283
		10	55.6		14.9	1	100	7.9	200
		11	49		28.7	1	100	3.1	297
	5	2	127		-58	1	100	0.9	308
		13	140		0	1	100	6.1	298
		14							
		7 MODEL OUTPUT							
		Arc.wise data							
		19							
									Distance to
		Distance in the sec (solid)				A	Maximum arc-wise	0	experimental arc-
		unstance to arc (units)				Averaging time (s)	concentration (%)	Groud wrath (units)	wise maximum
	1	00							concentration (m)
		01	57			1			
	1	02	140			1			
		0.4	57			100			
		04 05 Point wice data	140			100			
		06							
		07 Point location (units)							
	i i	08 x		у		z	Averaging time (s)	Concentration (%)	Temperature (units)
		09	40		-40.6	1	1		
		A h h Key Master (Fig	Id trink) Marta	(Word tupp)	aD / 1#	Manlo Cande 37 / 3	# Manlin Cande 24	2# Maolio Cando 2E	A# Dunno 2 E# Dun

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Previous Evaluations



FLACS v9.1



PHAST v6.6/6.7



Example: Burro 8 sensors on arc at distance of 57 m

Model: Method 1

Maximum concentration at any circumferential position and at any height

Experiments

Experiments

Model: Method 2

Maximum concentration at any circumferential position and at height of lowest sensors

Experiments

PHMSA-2010-0226 Advisory Bulletin "The maximum arc wise concentration should be based on the location of the experimental sensor data that produced the maximum arc wise concentration relative to the cloud centerline" Model: Method 3

 \rightarrow Maximum at any of the sensor positions

Aim & Methodology

- Aim: To assess how Methods 1, 2 and 3 affect the results for the field-scale experiments in the LNG MEP
 - Does it matter which method is used?
- Methodology: DRIFT integral dispersion model

- Developed by ESR
 Technology
- Dense/passive/buoyant dispersion
- GASP pool evaporation model

Plume Meander (Method 3a)

Results: Maplin Sands 27

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Results: Coyote 6

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Results: Overall

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Results: Overall

	Method 1	Method 2	Method 3	Method 3a
Mean Relative Bias, MRB	-0.21	0.31	0.59	0.41
Mean Relative Square Error, MRSE	0.34	0.38	1.1	0.59
Geometric Mean Bias, MG	0.79	1.4	6.6	1.9
Geometric Variance, VG	1.5	1.6	2e13	15
Factor of Two	78%	61%	54%	56%

$$MRB = \left\langle \frac{C_m - C_p}{\frac{1}{2}(C_p + C_m)} \right\rangle \qquad MRSE = \left\langle \frac{\left(C_p - C_m\right)^2}{\frac{1}{4}\left(C_p + C_m\right)^2} \right\rangle$$
$$MG = exp\left\langle \ln\left(\frac{C_m}{C_p}\right) \right\rangle \qquad VG = exp\left\langle \left[\ln\left(\frac{C_m}{C_p}\right)\right]^2 \right\rangle$$

 C_m = measured concentration

 C_p = predicted concentration

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Conclusions

- Choice of method for maximum arc-wise concentrations is important
- Depending on the choice of method, a model may be found to under/overpredict the measurements on average
- Method 3 (used by PHMSA) is more likely to indicate that a model underpredicts on average than other methods for max. arc-wise concentration
 - This is a precautionary approach given uncertainties in ensemble mean concentrations (it will tend to make the ½ LFL exclusion zone larger)
 - It accounts for the strong vertical gradient in concentration near the ground
 - It accounts for sensors not being aligned to arcs in some experiments
 - It encourages development of plume meandering models
- Further work is needed to investigate the plume meandering model in DRIFT and the sensitivity of results to the cloud height in the near-field

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