Modelling the Recirculation Zone in Street Canyons with Different Aspect Ratios, using CFD Simulations

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Outline

- 1. Motivation
- 2. Hypothesis
- 3. Methodology
- 4. Preliminary results
- 5. Further work

• Dispersion depends on the wind flow and the city structure



• Dispersion depends on the wind flow and the city structure



 $U_{ref} = 2 m/s$

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• Dispersion depends on the wind flow and the city structure



$$U_{ref} = 3 m/s$$

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• Dispersion depends on the wind flow and the city structure



$$U_{ref} = 4 m/s$$

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• Dispersion depends on the wind flow and the city structure



$$U_{ref} = 5 m/s$$

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• Dispersion depends on the wind flow and the city structure



 $U_{ref} = 6 m/s$

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Instantaneous and average velocity flow fields

- Flow in street canyons is complex
- The hour average velocity field is considered in most models

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• Popular description - 3 flow regimes identified by (Oke, 1988)

(a) Isolated roughness flow



- This concept was used in models like OSPM (Berkowicz et al., 1997)
- The recirculation zone is represented by a trapezium



- The base is two times the upwind building height, $L_{rec} = 2 \cdot H_{upwind}$
- Recirculation zone is the 3rd most sensitive factor (Ottosen et al., 2014)

2. Hypothesis

- Is there any quasi-universal expression for the "recirculation zone", that could expand the applicability of the typical street canyon models?
- The goals are to study the recirculation zone formation
 - ➢in irregular street canyons
 - ➤in arbitrary wind direction
 - ➤variable meteorology
 - ➤ scale of street canyons
- Not intended to repeat the flow pattern study in street canyons, but improve the approach in empirical models.

3. Methodology

- 1. Review of the recirculation zone
- 2. General setup of CFD simulations
- 3. Validation of the CFD simulation setup
- 4. Use of vortex identification methods, to determine the vortex structure

- Small scale street canyon dispersion models
- STREET-SR or ARPAC-1A (Johnson et al., 1973)



- The first notion of recirculation
- Two different concentrations for upwind and downwind receptors
- ➤ Calibration using field data
- Implicit modelling of the recirculation, through the empirical parameters

• Canyon Plume Box Model (Yamartino and Wiegand, 1986)



- Explicit use of a box model for the recirculation
- It covers the whole street
- The downwind receptor accounts for the "clean air injection"
- Calibration of parameters using field and wind tunnel data

• OSPM (Berkowicz et al., 1997)



Introduced the trapeze shape
Numerical condition, not physical

Other models using similar formulation →AEOLIUS (Buckland, 1998) →ADMS – Urban (Sabatino *et al.*, 2007) →L_{rec} = 3·H_{upwind} (Harman *et al.*, 2004) →L_{rec} = 2·H_{upwind} (Yang and Shao, 2006) →L_{rec} = 3·H_{upwind} (Cherin *et al.*, 2015)

• SIRANE (Soulhac et al., 2011)



- Uniform concentrations in each street segment
- Mass balance with the street intersections and the atmosphere
- For H/W \geq 1/3: street canyon
- For H/W < 1/3: open terrain

Available data from wind tunnel experiments and CFD simulations

- Irregular streets, wind tunnel (Addepalli and Pardyjak, 2013, 2014)
- Thermal effects, wind tunnel (Allegrini et al., 2013)
- Thermal effects, CFD (Allegrini et al., 2014)
- Thermal effects, field experiments (Dallman et al., 2014)
- Thermal effects, field experiments (ldczak et al., 2007)
- Roof shapes, CFD (Huang et al., 2014)
- Roof shapes, CFD (Takano and Moonen, 2013)
- Roof shapes, wind tunnel (Kellnerová et al., 2012)

3. Methodology: Simulation setup



- Large Eddy Simulation: large eddies are solved, small are modelled
- Transient solution of NS equations
- Fine mesh: 100 cells per 10 m
- Standard Smagorinsky model for the subgrid scales

• CFD results against experiments from (Li, 2008)

• Aspect ratio H/W = 1

• CFD results against experiments from (Li, 2008)



• Aspect ratio H/W = 1

• CFD results against experiments from (Li, 2008)



• Aspect ratio H/W = 1, excellent agreement

• CFD results against experiments from (Li, 2008)

• Aspect ratio H/W = 0.5

• CFD results against experiments from (Li, 2008)



• Aspect ratio H/W = 0.5

• CFD results against experiments from (Li, 2008)



• Aspect ratio H/W = 0.5, fair agreement

3. Methodology: Vortex identification

- Use of vortex identification methods
- Intuition: where there is a vortex, there is a recirculation zone
- Universal: analyze the whole velocity field
 - streamlines, tangent to the velocity vector curve at all points
- Local: analyze the ∇u at a finite number of points
 - $\lambda_2 < 0$ (Jeong and Hussain, 1995)
 - $\ensuremath{\mathcal{V}u}$ is decomposed in symmetric S and antisymmetric Ω
 - second largest eigenvalue of $S^2 + \Omega^2$
 - Q > 0 (Hunt et al., 1988),
 - second invariant of $\frac{1}{2}[\|\mathbf{\Omega}\|^2 \|\mathbf{S}\|^2], \|\mathbf{S}\| = [tr(\mathbf{SS}^T)]^{1/2}, \|\mathbf{\Omega}\| = [tr(\mathbf{\Omega}\mathbf{\Omega}^T)]^{1/2}$
 - vorticity, $\vec{\omega} \equiv \nabla \times \vec{u}$

4. Preliminary results: aspect ratio = 1 / 2



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4. Preliminary results: aspect ratio = 1 / 3



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4. Preliminary results: aspect ratio = 1 / 4



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5. Further work

Until now

- Application of the detection methods highlighted the big vortices
- No new insight to the size of the recirculation zone

Further steps of the study

- Pollutant dispersion as an indicator for the recirculation zone
- Irregular street canyons
- Arbitrary wind direction
- Effect of the wind speed, Reynolds number
- Effect of heated street facets
- Effect of the scale (eg. AR=1, when H=10m or 20m)

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