LES STUDY OF UNSTEADY FLOW PHENOMENA IN AN URBAN GEOMETRY -THE NEED FOR SPECIAL EVALUATION METHODS

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MOTIVATION

- When we evaluate CFD results, usually mean values are used
- Large Eddy Simulation resolves turbulence: it can also provide <u>concurrent timeseries</u>
 - Can we get extra knowledge using LES results?
 - Additional methods are needed to evaluate the results and compare with other time-dependent data (experimental or numerical). Can we identify such methods?

PRESENT OBJECTIVES

- Contribution through examination of a suitable experimental case: "MICHEL-STADT"
 - Focus on unsteady phenomena
 - Some of the unique capabilities of LES will be presented
- Try to find ways to:

- Extract useful information from a LES simulation
- Compare transient methodologies' results (e.g. exp & LES)
- Identify specific-for-LES evaluation methods

<u>Comment</u>

The present work is leaning towards the 'start' not towards the 'end' of the problem under investigation

LES EQUATIONS IN ADREA-HF Compressible volume-filtered Navier-Stokes

• Filtered equations:

$$\begin{aligned} \frac{\partial \overline{\rho}}{\partial t} &+ \frac{\partial (\overline{\rho} \, \tilde{u}_{i})}{\partial x_{i}} = 0 & \overline{p} = \overline{\rho} \, r \, \overline{T} \\ \frac{\partial (\overline{\rho} \, \tilde{u}_{i})}{\partial t} &+ \frac{\partial (\overline{\rho} \, \tilde{u}_{i} \, \tilde{u}_{j})}{\partial x_{j}} = - \frac{\partial \overline{p}}{\partial x_{i}} + \frac{\partial (\tilde{\tau}_{ij}^{l} + \tau_{ij}^{R})}{\partial x_{j}} & \tilde{\tau}_{ij}^{l} + \frac{2}{3} \mu \frac{\partial \tilde{u}_{k}}{\partial x_{k}} \delta_{ij} = 2 \mu \tilde{S}_{ij} \\ \tau_{ij}^{R} &= - \overline{\rho} \, u_{i} u_{j} + \overline{\rho} \, \tilde{u}_{i} \, \tilde{u}_{j} & \tilde{s}_{ij} = \frac{1}{2} \left(\frac{\partial \tilde{u}_{i}}{\partial x_{j}} + \frac{\partial \tilde{u}_{j}}{\partial x_{i}} \right) \end{aligned}$$

Smagorinsky model of the residual stress tensor

$$\tau_{ij}^{R} + \frac{1}{3}\tau_{kk}\delta_{ij} = 2\mu_{t}\tilde{S}_{ij}; \ \mu_{t} = \bar{\rho}\left[C_{s}\Delta\left(1 - e^{-y^{+}/25}\right)\right]^{2}\sqrt{2\tilde{S}_{ij}\tilde{S}_{ij}}$$

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MICHEL-STADT Semi-idealized city



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MICHEL-STADT Case description and setup

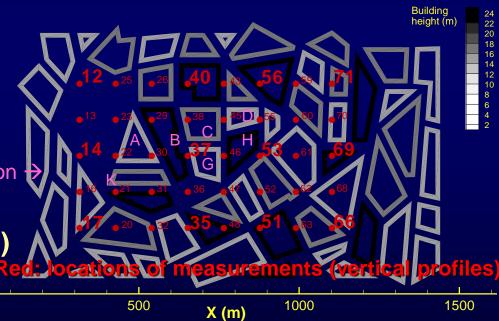
- Data from the CEDVAL-LES wind-tunnel database
 - Semi-idealized wind-tunnel city Michel-Stadt examined
 - Detailed measurements available

۲ (m)

800

600

- Case setup:
 - Full scale
 - 3 mil. cells
 - Langevin inlet BC
 - *z_o*=0.0625m
 - *dt*=0.2s Flow direction
 - 10000s run
 - 39 days run (4 cores)



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LES EQUATIONS IN ADREA-HF Langevin-type inlet boundary condition

• For the fluctuation u_i' we postulate :

$$u_i'(t + \Delta t) = \left(1 - \frac{\Delta t}{T_{u_i}}\right) u_i'(t) + \sigma_{u_i} \left(\frac{2\Delta t}{T_{u_i}}\right)^{1/2} \xi$$

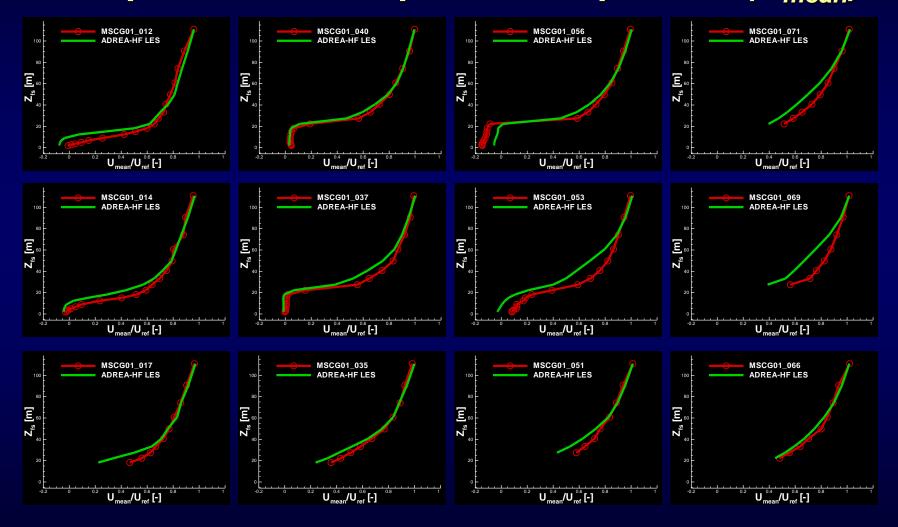
coherent part random part Needed at each boundary cell: U_{mean} , standard deviation σ_{u} , integral time scale T_{u} . ξ is a random number

• More general formulation (to achieve spatial correlation also): $u'_{i}(t + \Delta t) = \left(1 - \frac{\Delta t}{T_{u_{i}}}\right) f\left(r_{i} \cdot u'_{i}(t) + (1 - r_{i})\frac{1}{4}\sum_{\gamma=1-4}u'_{i\gamma}(t)\right) + \sigma_{u_{i}}\left(\frac{2\Delta t}{T_{u_{i}}}\right)^{1/2} \xi$

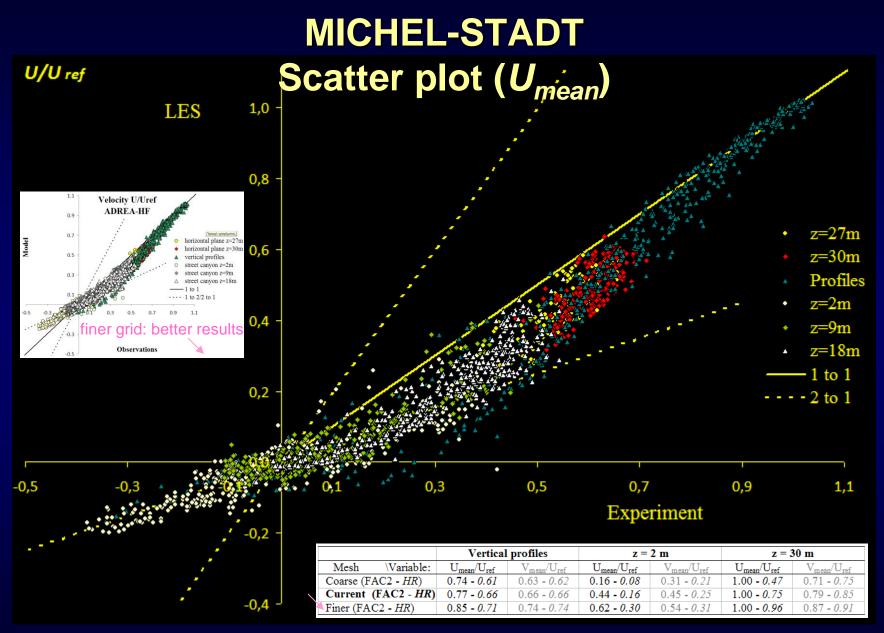
 γ : neighboring cells, r: localization factor (0-1), f: enforcing factor (default 1)

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MICHEL-STADT Comparison with experimental profiles (U_{mean})

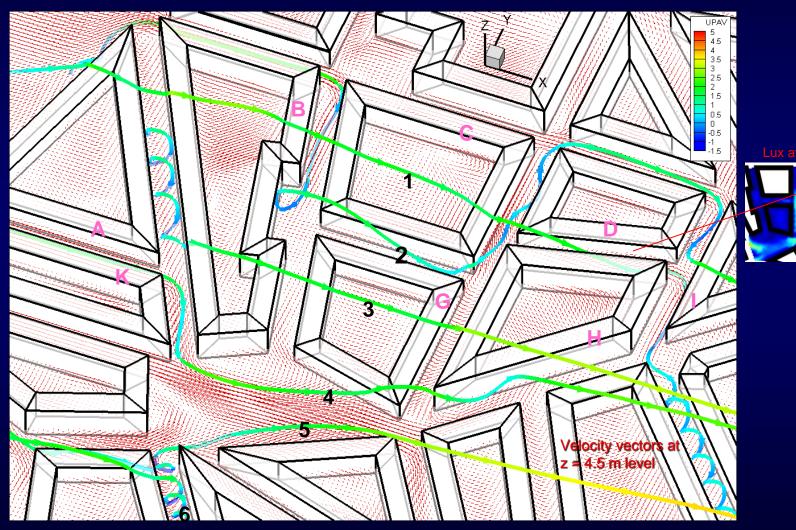


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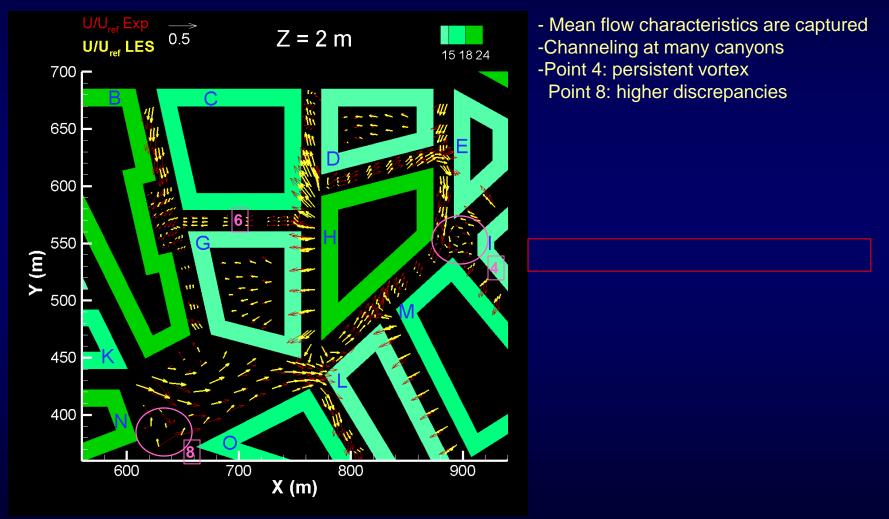
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MICHEL-STADT 3D Streamtraces of mean flow at central city



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MICHEL-STADT Mean velocity vectors at *z* = 2 m (LES vs. EXP)

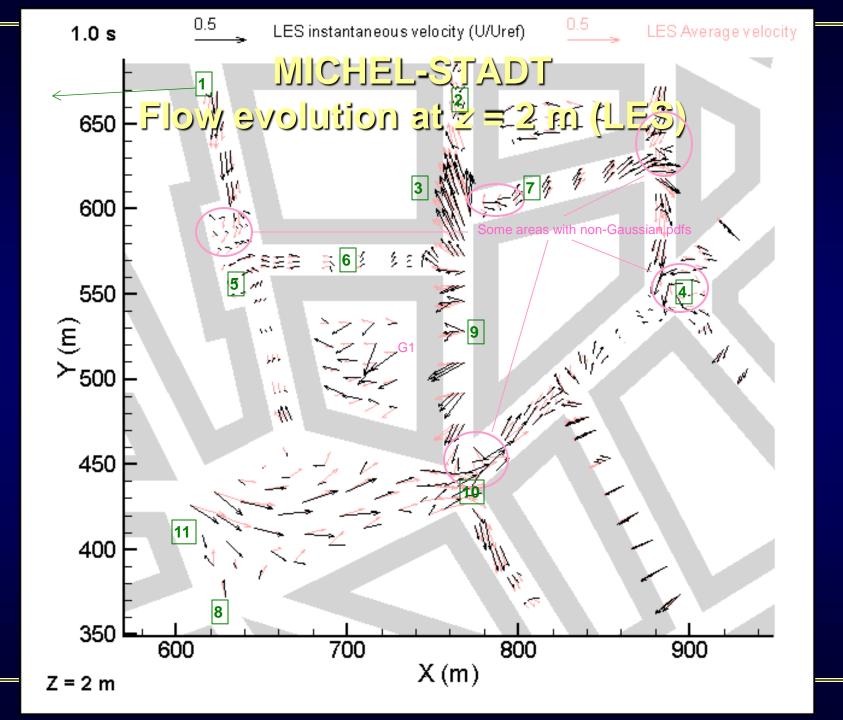


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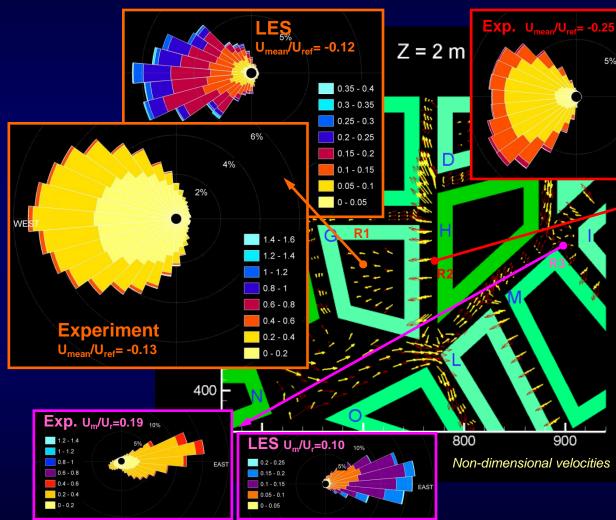
Beyond the mean flow..

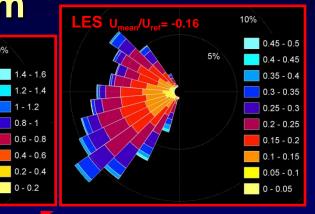
For example:

- Time evolution of velocity field
- In-depth comparison of time series characteristics: frequency distributions (e.g. direction and wind speed in terms of wind rose diagrams)
- Identification of important coherent structures (e.g. hairpin vortices, vorticity sheets etc)



MICHEL-STADT Wind roses at z = 2 m





- Colors are different due to high peak values of exp. Even with similar mean values, several differences at roses!
- Exp roses are generally "smoother"
- Chosen roses (glimpse to unsteady phenom):
- R1: High direction variability

10%

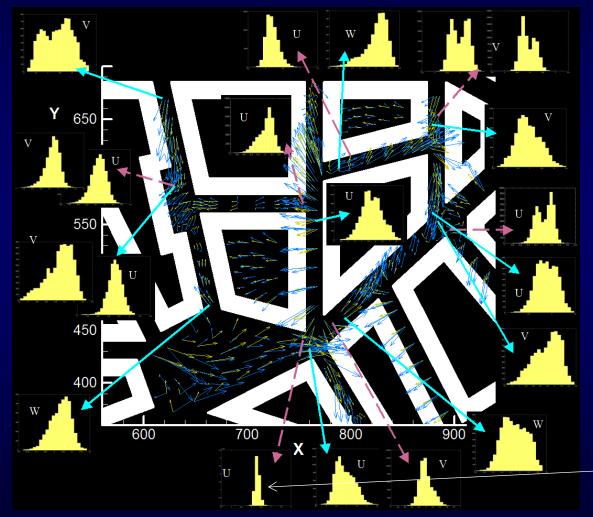
5%

- R2: Bimodal behavior in direction
- R3: Bimodal/ opposite directions (exp)

- Obviously just mean values cannot express all that information

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MICHEL-STADT z = 2 m - non-Gaussian velocity pdf



- LES can provide skewed or bimodal velocity probability density distributions (observed in EXP)

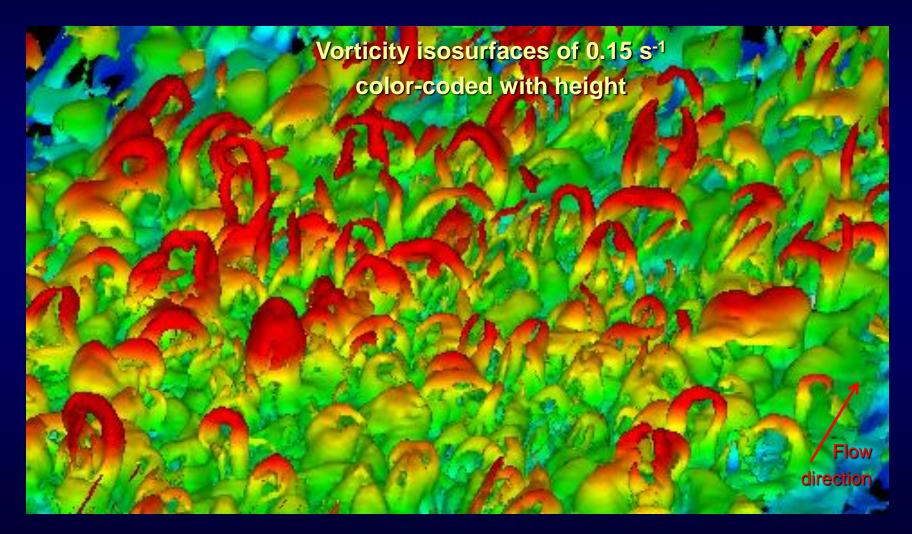
- They can usually be found in areas of high unsteadiness, like at vortex limits

-_Most non-Gaussian spots are near street junctions

- At points of bimodal (or skewed) behavior, <u>the average</u> value might not have a physical meaning

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MICHEL-STADT Hairpin vortices above the city



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6000 s

orticity magnitude 0.33 s⁻¹ isosurfaces Z:

5 10 15 20 25 30 35 40 45 50

COHERENT STRUCTURES

orticity sheets

U velocity

fluctuation

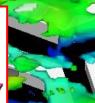
u': -1.9 0 1.9

ow-momentum areas

risosurfaces, usually de hairpin vortices)



Flow direction-



- With the vorticity isosurfaces we can investigate turbulent structures and have a deeper insight into flow dynamics

High-momentum areas u' = 1.9 m/s(white isosurfaces, usually below vorticity sheets)

DREA-HFILES simulation

ADREA-HFILES simulation

6000 s

1

ADREA-HF LES simulation

6010's

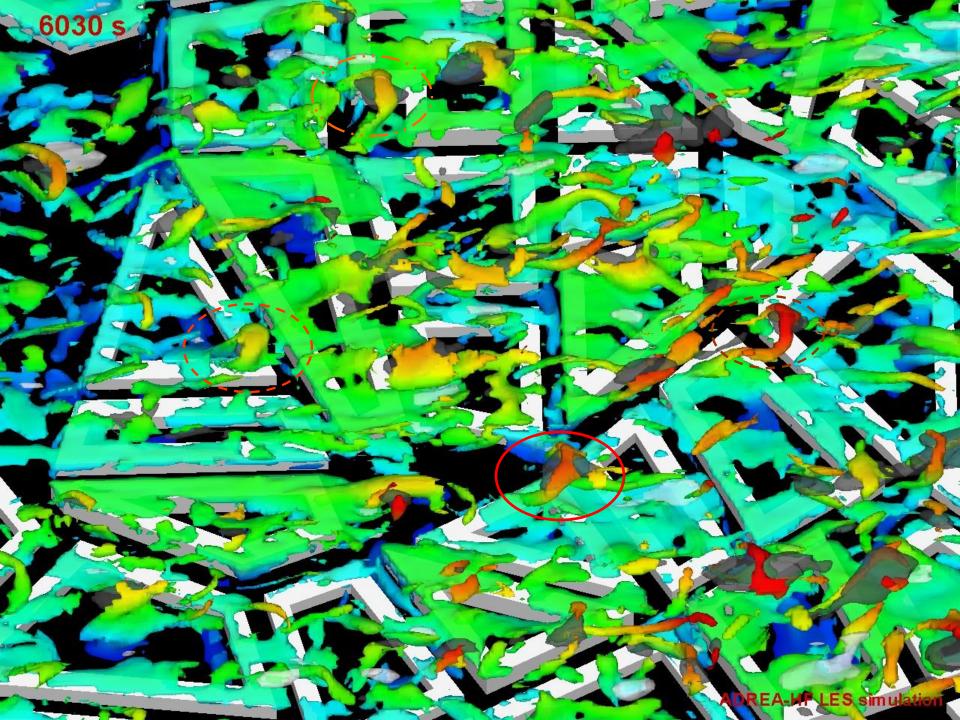
ACLAN .

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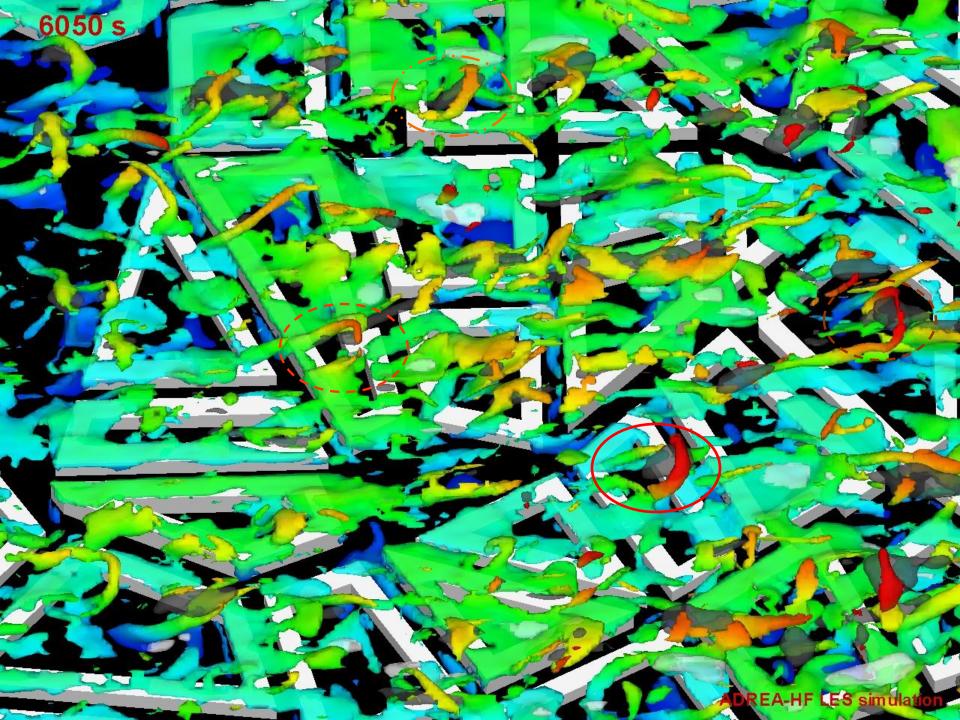
REA-HF LES simulation

6020 s

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ADREA HF LES simulation

6060 s



ADREA-HILES simulation

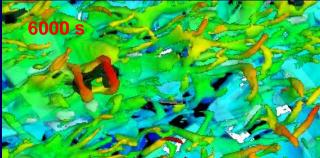
6080 s

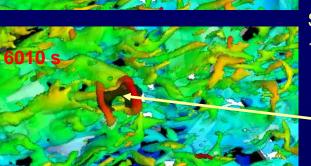
S-

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MICHEL-STADT Finer grids reveal finer structures



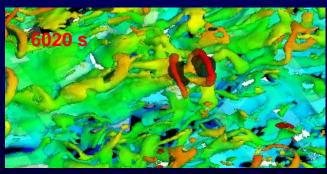


Grid of 7 million cells (preliminary results from run performed at the ARIS national Supercomputer, 190000 GFlops)

Pair of hairpin vortices



- More complicated and more detailed structures can be seen
- More interactions between structures
- Groups of hairpin vortices can be identified (so-called LSM: Large Scale Motions)



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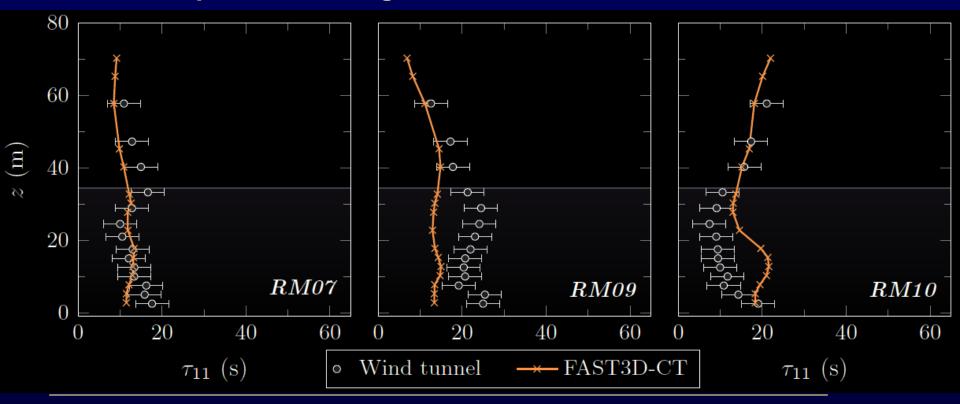
On LES Model Evaluation

- It is obvious from the above that LES has significant capabilities
- In order to assess the quality of the simulation we need to extend the validation
- e.g. look at comparison of:
 - Frequency distributions (shape parameters)
 - Eddy statistics (integral length & time scales, turbulence spectra, structure functions)
 - Flow pattern analyses (conditional resampling/averaging, joint time-frequency analysis, orthogonal decomposition, stochastic estimation)

Hertwig 2013, On aspects of large-eddy simulation validation for near-surface atmospheric flows. PhD thesis, University Hamburg Hertwig et al. 2011, J Wind Eng Ind Aerodyn 99, 296-307

EXAMPLES OF MORE EVALUATION METHODS Autocorrelation time scales

Vertical profiles of integral time scales for both LES and EXP

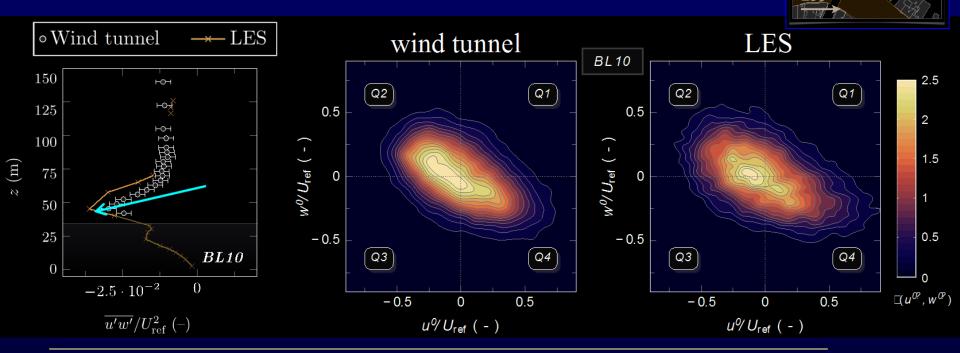


Hertwig 2013, On aspects of large-eddy simulation validation for near-surface atmospheric flows. PhD thesis, University Hamburg

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EXAMPLES OF MORE EVALUATION METHODS Joint probability distributions

- In-depth comparison of vertical momentum flux
- Joint probability distributions of *u* and *w*



Hertwig 2013, On aspects of large-eddy simulation validation for near-surface atmospheric flows. PhD thesis, University Hamburg

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CONCLUSIONS

- LES can contribute to a more fundamental understanding of turbulent flow phenomena
- New ways of evaluating results emerge
- There is a need to identify and standardize methods to analyze LES results and to compare them with experimental/reference data;
- There is a need of parallel work of experimentalists and modellers, in both the design of the experiments and the interpretation of the model results

Ευχαριστώ Thank you