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CAPABILITY OF THE STANDARD (K,EPS) MODEL FOR SIMULATING ATMOSPHERIC DISPERSION OVER A NPP SITE

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Background:

- **Impact and safety studies**: distribution of radionuclides or other air transported pollutants on a **Nuclear Power Plant site**
- Wind tunnel experiments at **LMFA***, founded by **IRSN****, **EDF***** Bugey NPP site (Méjean 2005)

Means:

- CFD & dispersion simulation with the **STARCD** code

Objective:

- Check **capability of basic modelling options** to simulate this flow by inter-comparing with the wind tunnel data



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** Institut de Recherche sur la Sûreté Nucléaire

*** Electricité de France



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Characteristics of experiment:

- Model

- scale 1/500, similarity of \vec{V} , Re distortion 1/500
- inlet and ground devices simulate the neutral ABL
- 2 opposite wind directions, 3.7 m/s at 50m height
- 2 types of source: stack or containment building

- Measurements

- at 15 streamwise positions from the source, horizontal profiles available at 4 heights and vertical profiles available at X=0
- mean velocity components \bar{U} , \bar{V} , \bar{W} and r.m.s. of stream wise fluctuating component v' by LDA*
- instant concentration of tracer (ethane) by FID**

* Laser Doppler Anemometry

** Flame Ionisation Detector



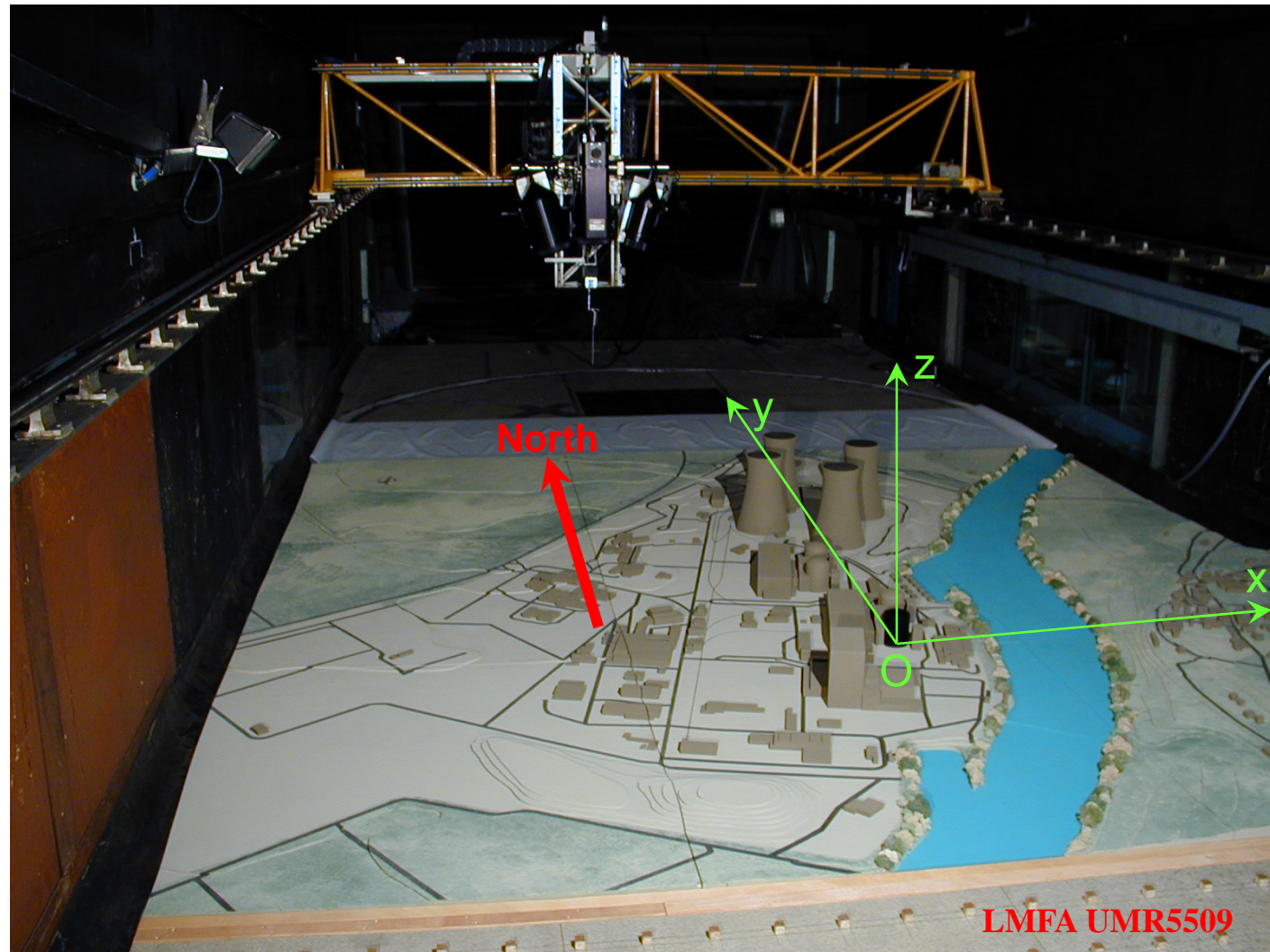
Overview of Bugey NPP model in wind tunnel



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Oy axis points
to the north

Cooling tower
height 140 m
 \varnothing_{top} 70 m



LMFA UMR5509



Location of sources



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Release from
ventilation stack

28 000 m³/h

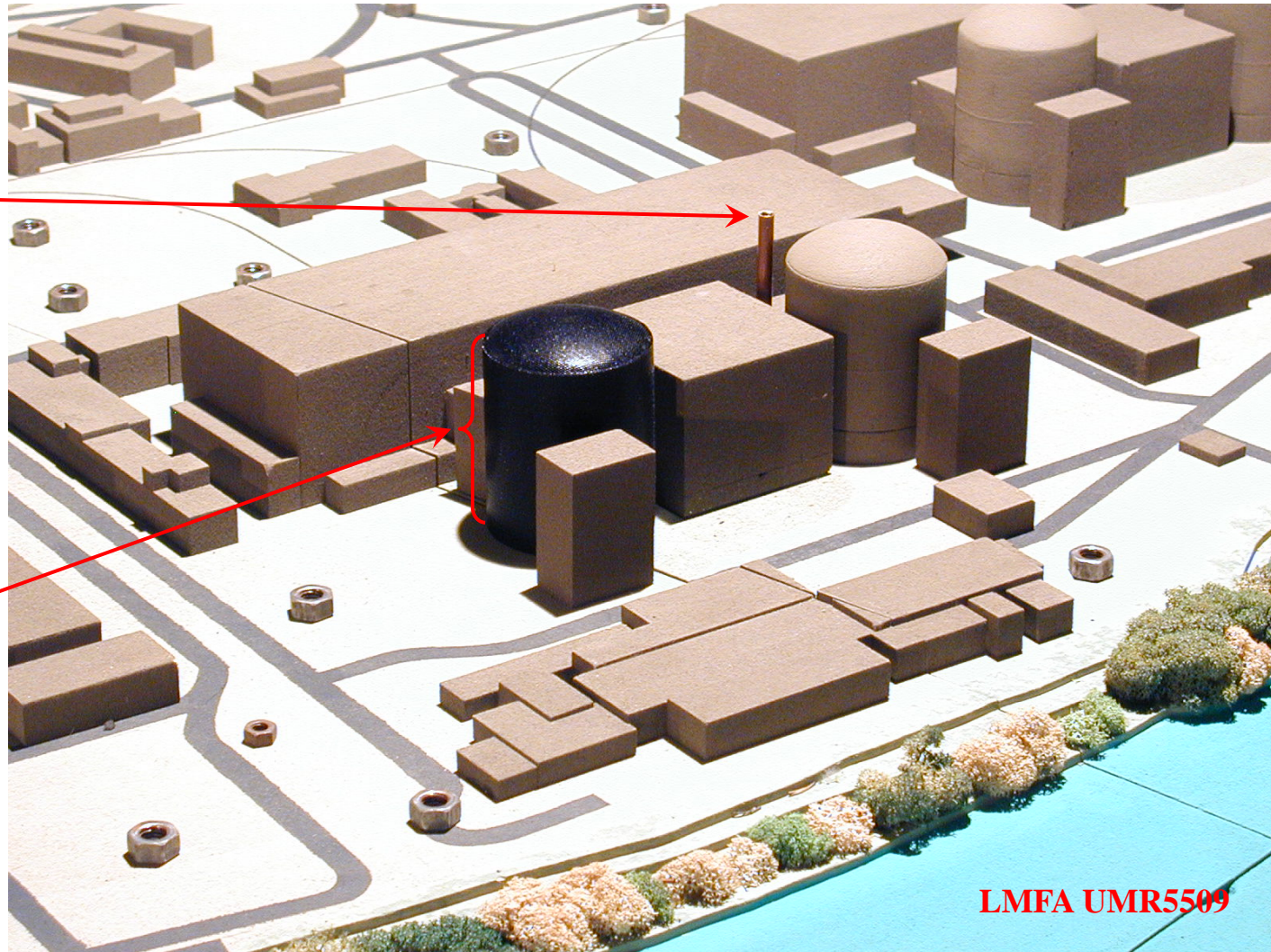
height 55 m

speed $W=20\text{m/s}$

Release from
containment
building skin

17000 m³/h

(height 50 m)



LMFA UMR5509





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Characteristics of (k,ε) computation:

- Grid

- Domain 1000m x 3000m x 300m
- Minimum cell size horizontally 0.3m, vertically 0.5m
- Total mesh comprises 0.41 to 0.65 10^6 cells

- Boundary conditions

- Simulate the neutral stability homogeneous SBL
- Inlet profiles as by Richards & Hoxey
- Rough wall at ground (aerodynamic rugosity 0.04m)
- Smooth walls on buildings
- Profile values at h=300m imposed on top boundary



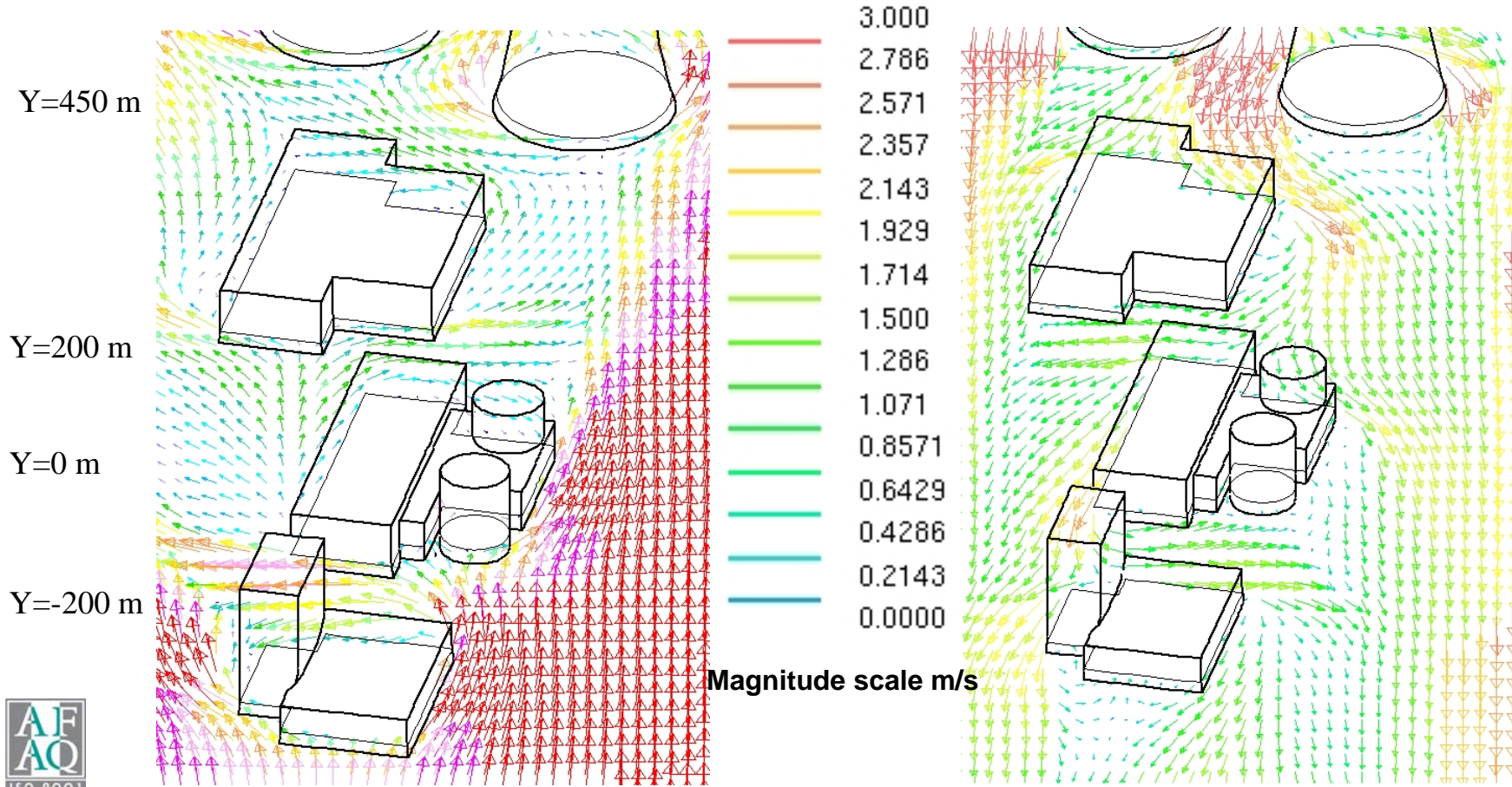


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Velocity vector field at z = 10m

• South wind

• North wind

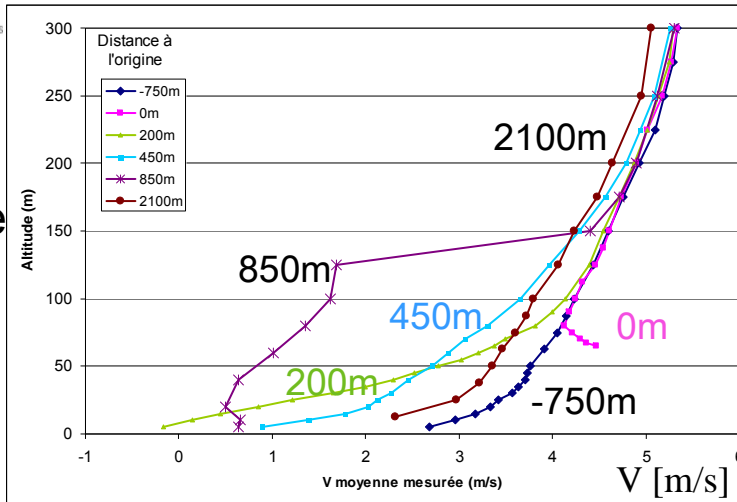




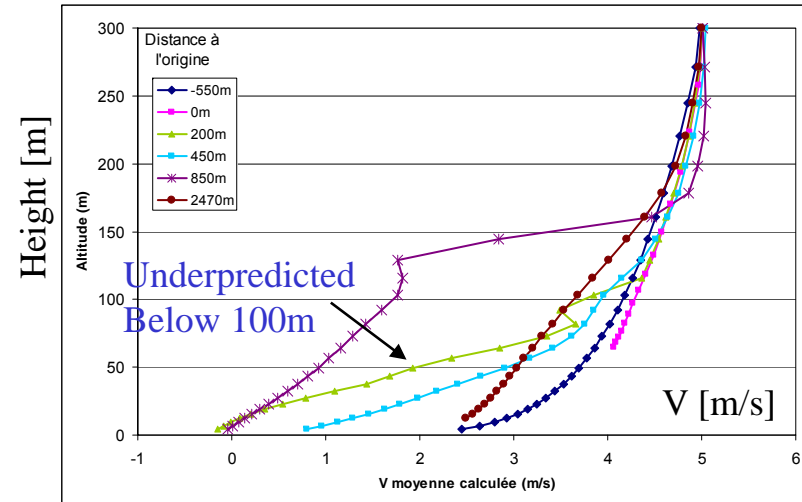
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Results for velocity field : U and V profiles by south wind

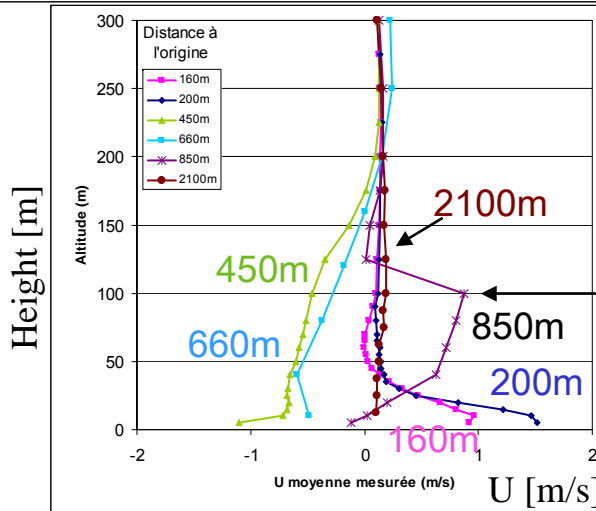
Streamwise
Wind V



computed

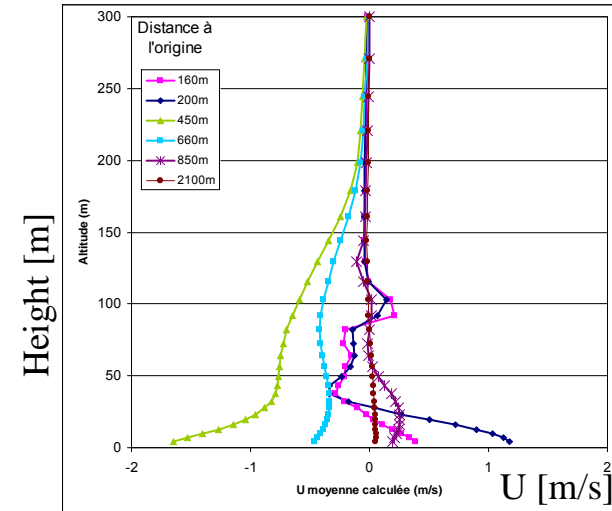


Crosswise
Wind U



Good qualitative agreement

Wake of the Cooling tower





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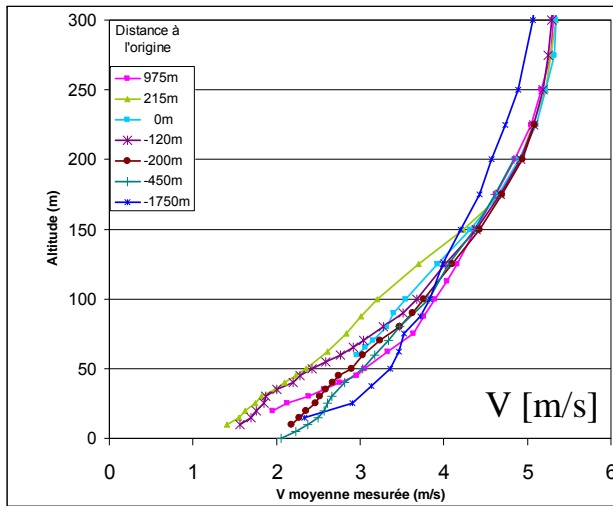
Results for velocity field : U and V profiles by north wind

measured

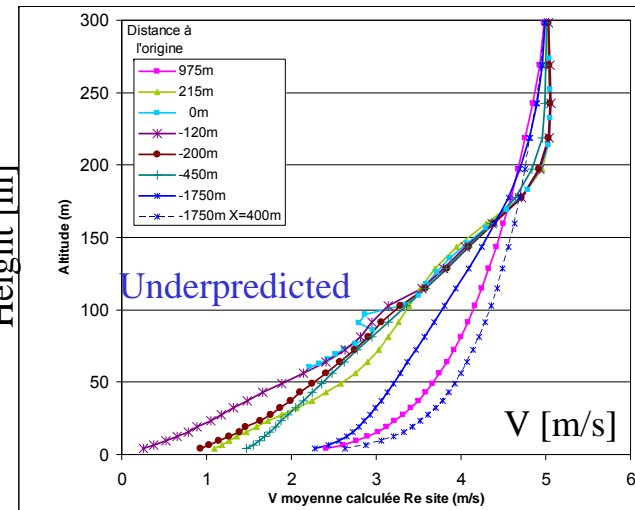
computed

Streamwise
Wind V

Height [m]

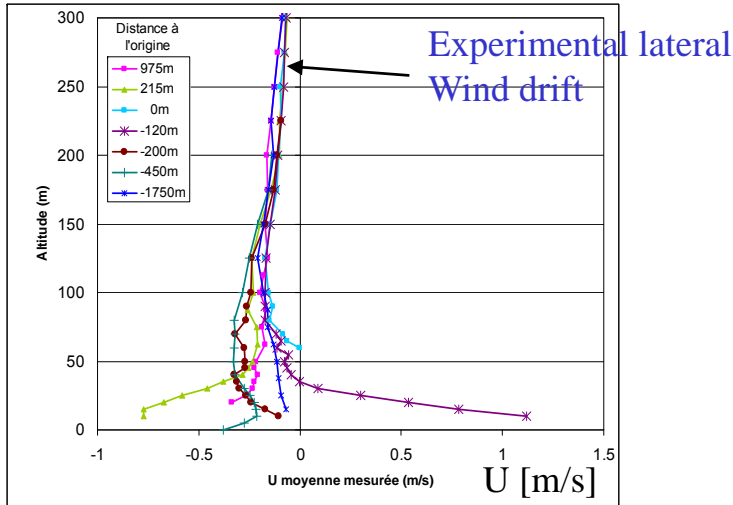


Height [m]

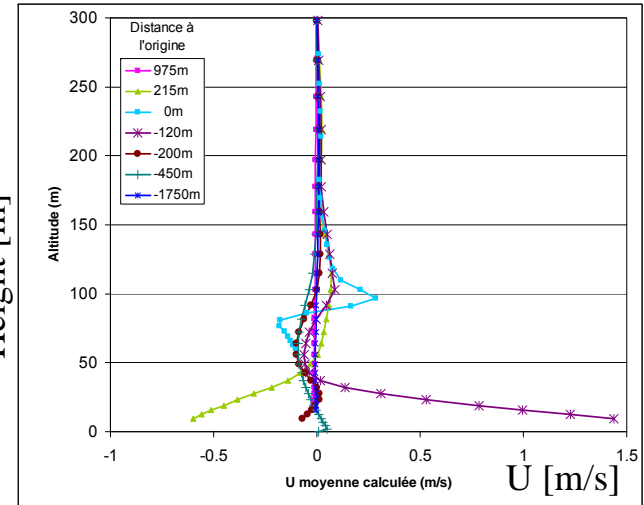


Crosswise
Wind U

Height [m]



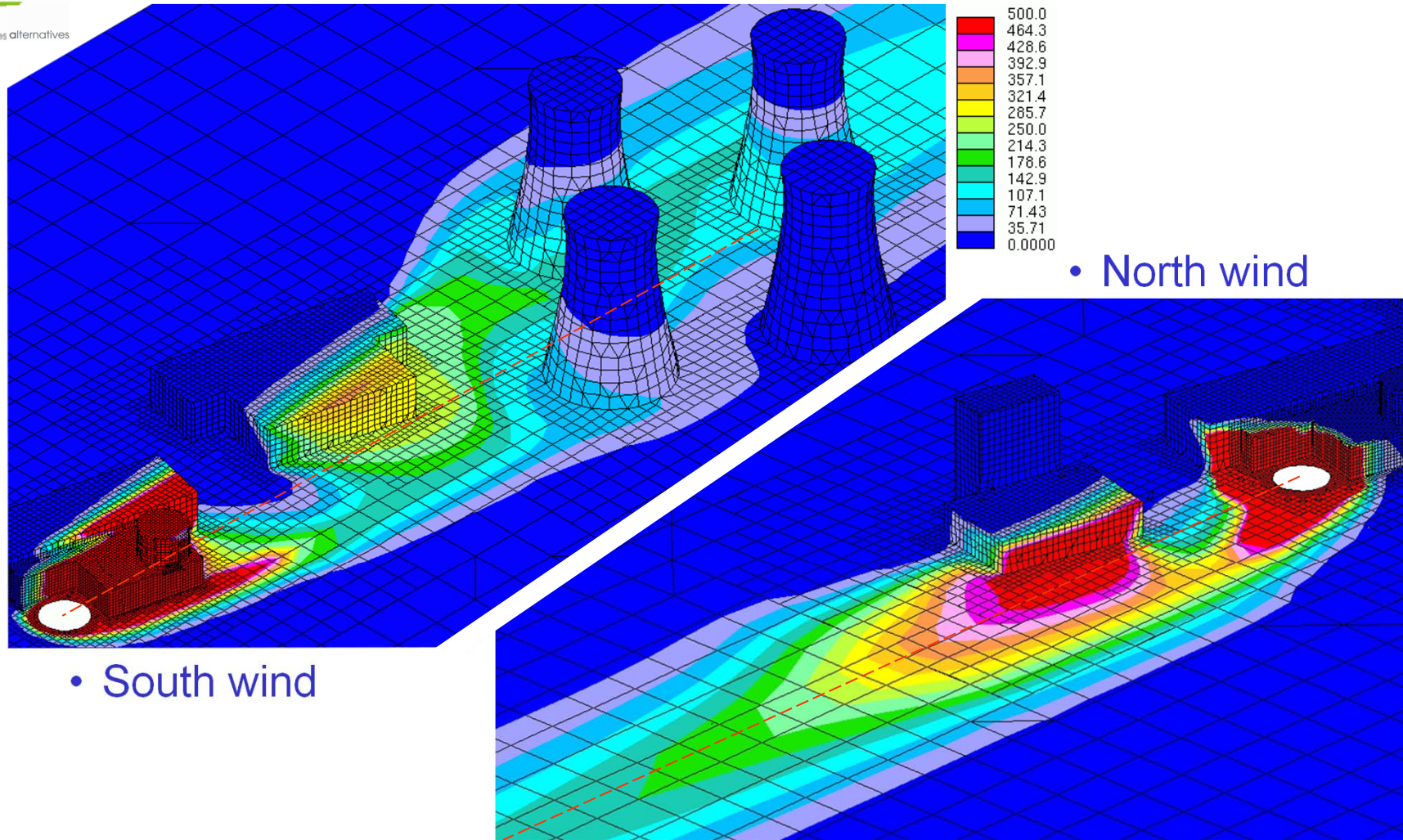
Height [m]





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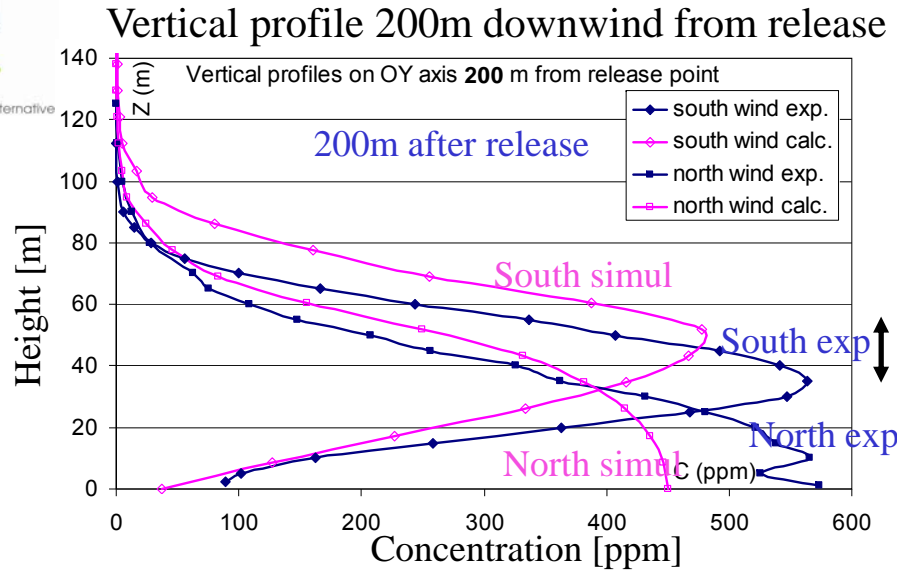
Concentration field (ppm) at z=1m for building release



Concentration profiles for building release



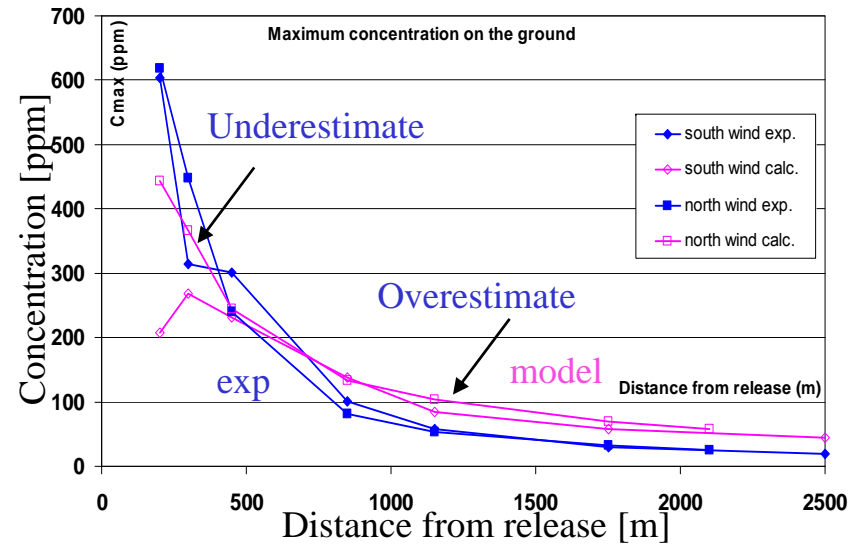
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- Qualitative agreement
- Model underestimates the near field ground concentration
- Model overestimates far field (>500m)



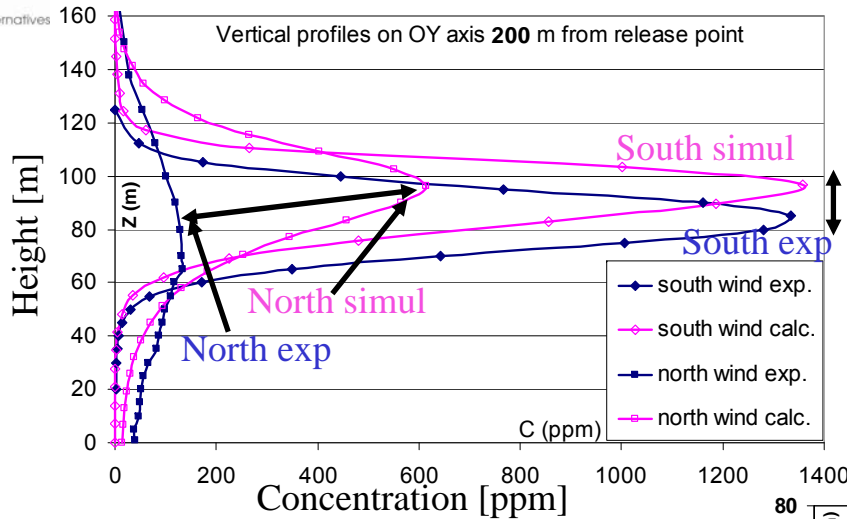
Streamwise ground concentration





Concentration profiles for **stack** release

Vertical profile 200m downwind from release



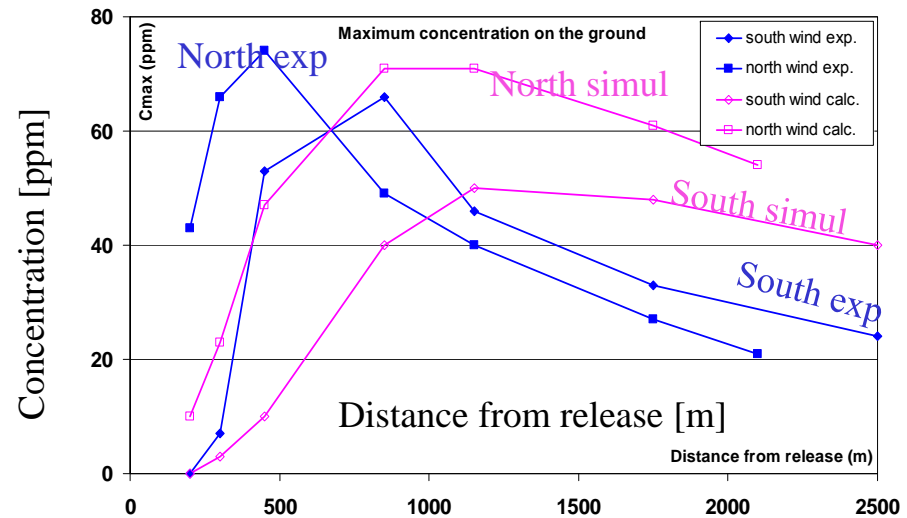
- Good agreement for South wind, simulated plume 10m higher due to lack of plume deflexion
- Poor agreement with north wind : the turbulent mixing in the wake of the cooling towers is underpredicted

On the ground :

- Underprediction in the near field : lack of mixing and plume too high
- Overprediction in the far field : lack of lateral spreading



Streamwise ground concentration





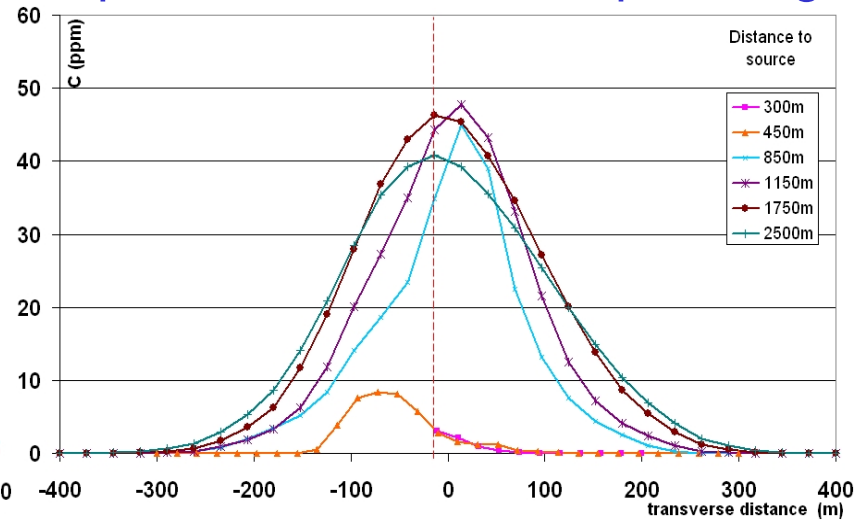
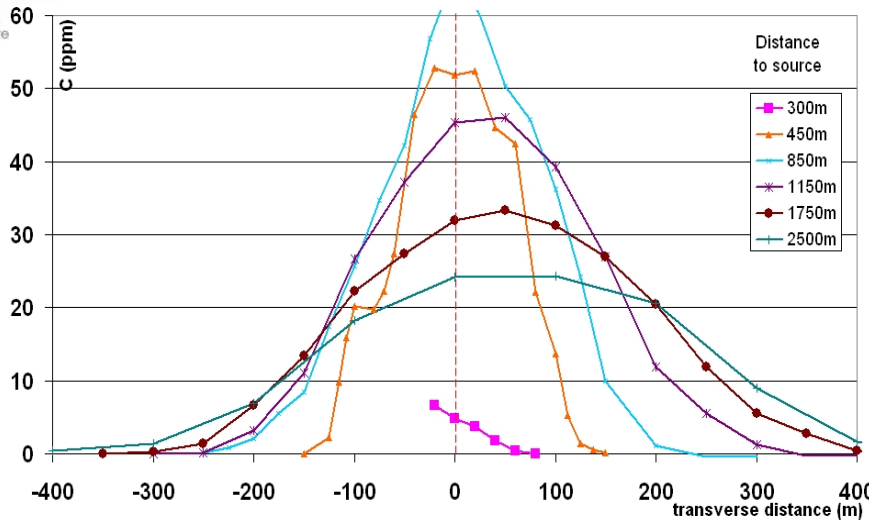
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Ground concentration spanwise profiles for stack release

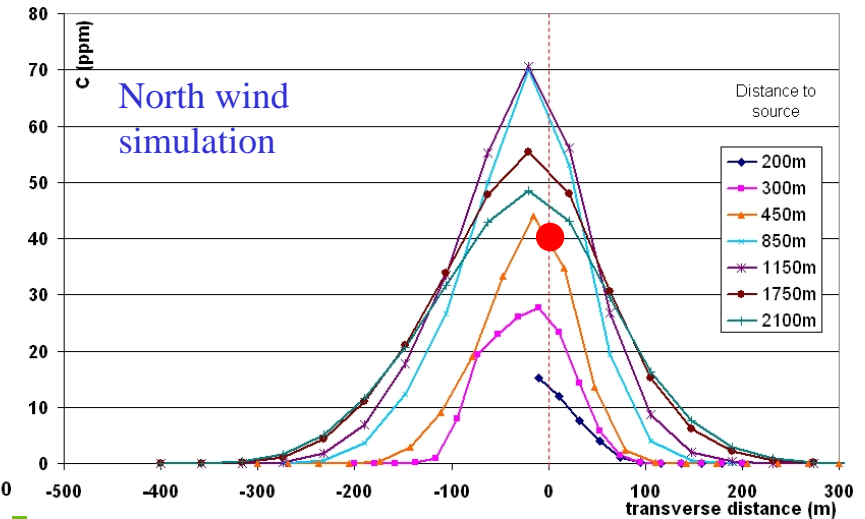
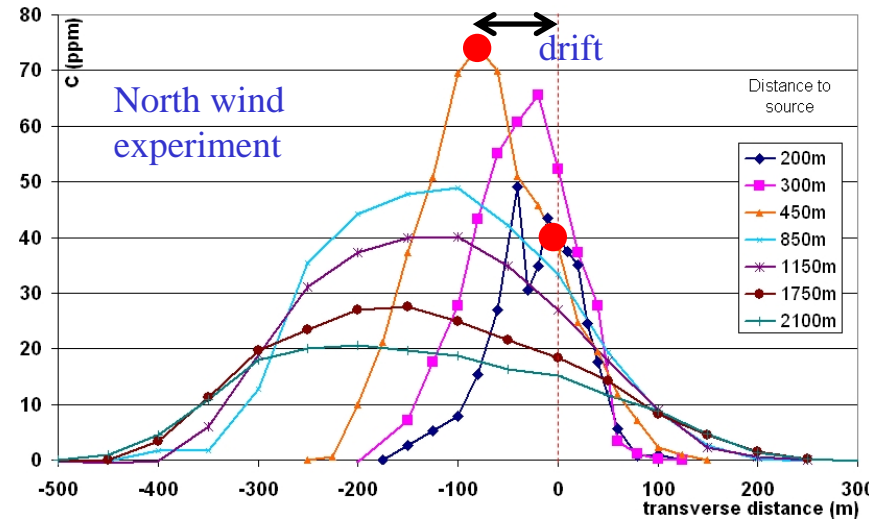
• measured

Computed: lack of lateral spreading

south wind



north wind



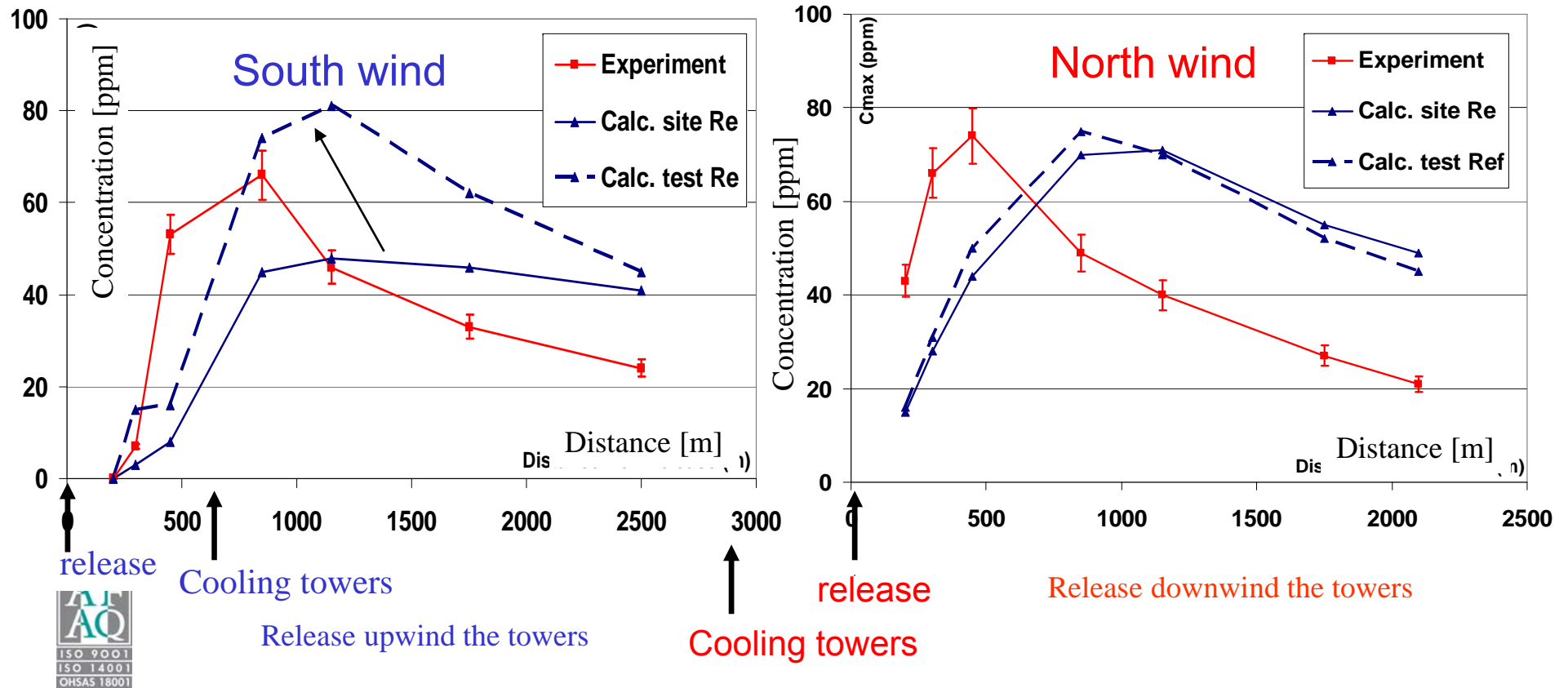


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Effect of Reynolds distortion

checked on Oy ground concentration for stack release

$Re_{tunnel} = 4 \cdot 10^4$ (subcritical), $Re_{site} = 2 \cdot 10^7$ (supercritical)



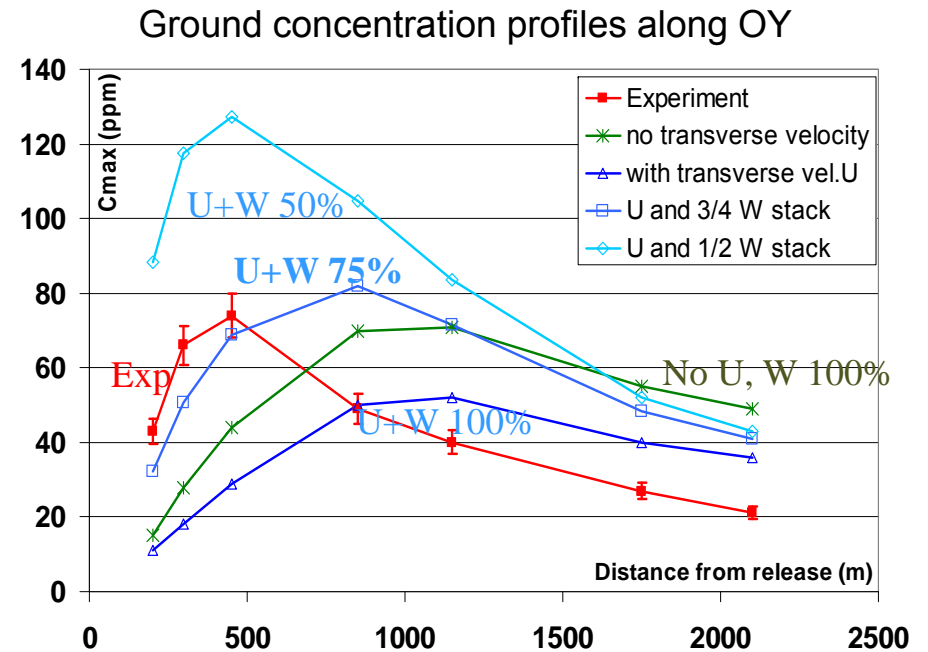
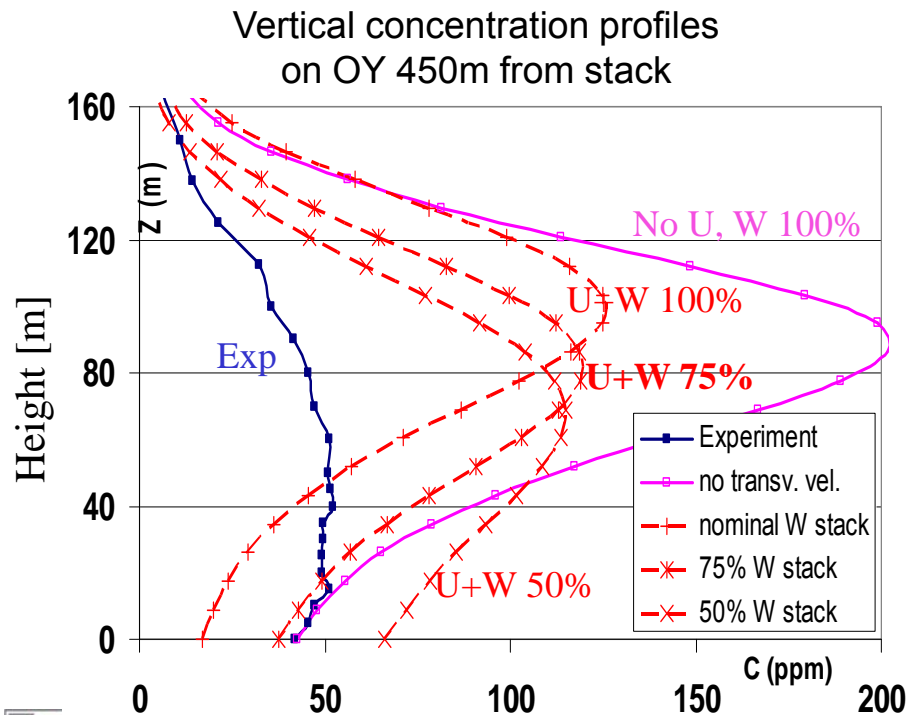


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Effect of release speed W & lateral wind U

tested for release from stack under north wind

- Less momentum for the stack release W
- Crosswind analytical function U added to the model





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Conclusions

- Effect of large buildings is crucial on an industrial site
- Maximum ground concentration is twofold underpredicted in the near field, due to underprediction of turbulent mixing in the built area
- In the far field maximum concentration is twofold overpredicted due to the lack of lateral spreading by the (k,ε) model
- In case of stack release it is essential to simulate well the initial exhaust plume deflection
- We have to pay attention to Reynolds distortion effects when applying tunnel experiments to the real world
- Effect of wind direction and source type/location is qualitatively well captured by a basic turbulence model



If I can't answer please mail to pierre.roubin@cea.fr

