

 HARMO'17

17th International Conference on  
Harmonisation within Atmospheric  
Dispersion Modelling  
for Regulatory Purposes

Budapest, Hungary, 9-12 May 2016

# Dry Deposition onto Vertical Surfaces in the Urban Environment

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# Particle Deposition

- Important consideration for dispersion modelling
  - Key sink within aerosol budget
- Vertical surfaces dominate urban environment
  - Some models only account for deposition onto horizontal surface, e.g. Bruse (2007)
- Impacts on human health – exposure pathway
- Deterioration and dirtying of built environment – cultural heritage



# Outline

1. Background: Review of past experiments
2. Experimental set-up
3. Experimental results
  - a) Micrometeorology
  - b) Deposition velocity
4. Analysis: Governing parameters
5. Conclusions

# **BACKGROUND: REVIEW OF PAST EXPERIMENTS**

# Long-term measurements

- Roed (1990) performed series of analyses on urban surfaces
- Following nuclear tests and Chernobyl disaster in 1980s
- Deposition velocities on vertical surfaces an order of magnitude (or more) less than on horizontal surfaces
- Also long-term component to Salissure de Façade (SaliFa) project (France)

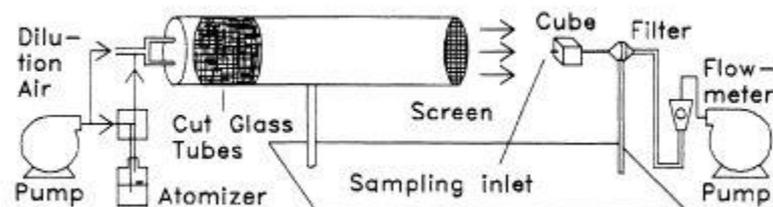
# Short-term measurements

- Pesava et al. (1999) measured deposition velocity onto surfaces of a cube placed outdoors

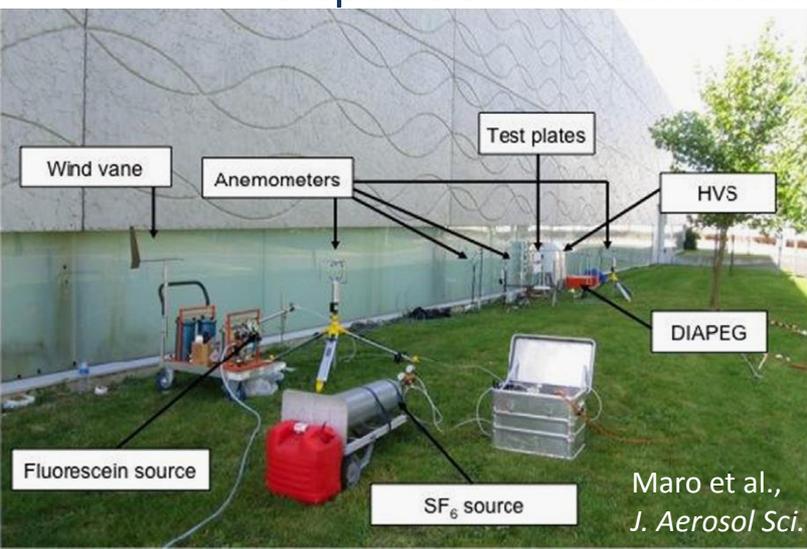
- Not a real urban surface

- SaliFa short-term experiments

- Maro et al. (2014) conducted 2 sets of experiments in 2005 and 2006
- Constructed panels of glass and plaster glazing
- Deposition of fluorescein on timescale  $\sim 1$  hour



Pesava et al., *Sci. Tot. Environ.*



Maro et al.,  
*J. Aerosol Sci.*



- Detailed observations of flow, turbulence, and aerosol concentrations

## Submicronic aerosols

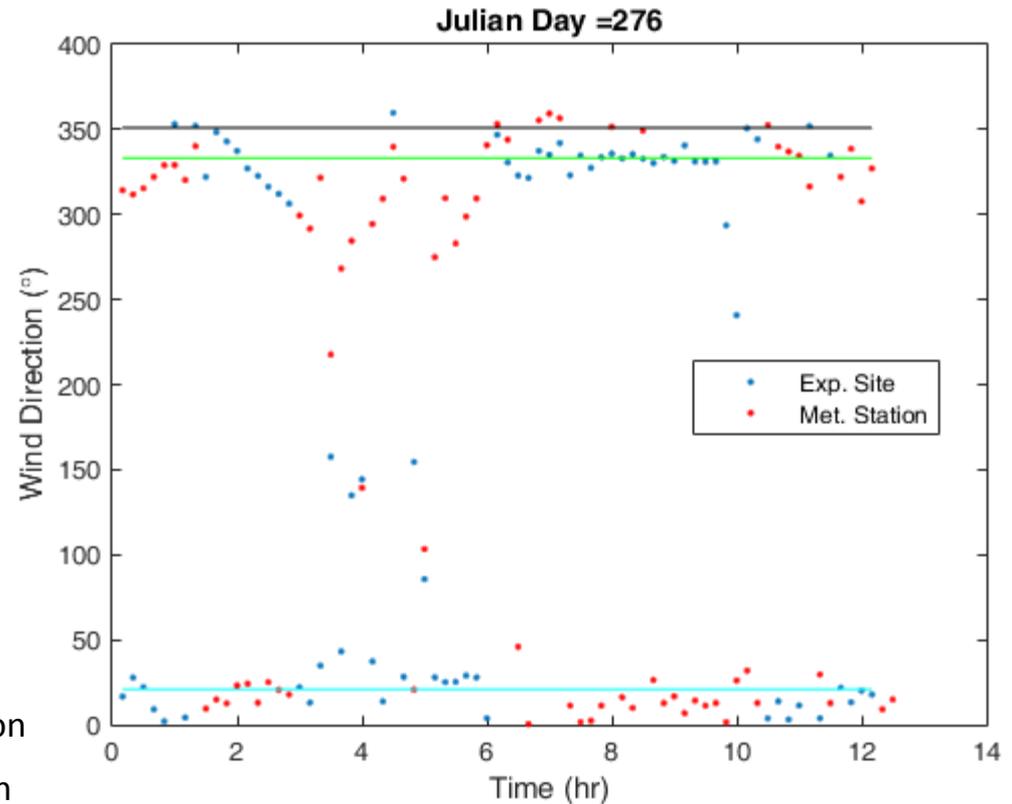
- The  $0.1-1 \mu\text{m}$  range has been focus of past studies;
- Peak range in urban areas (Horvath et al. 1996), including soot, radionuclides, etc.

# EXPERIMENTAL SET-UP

# Preliminary analyses



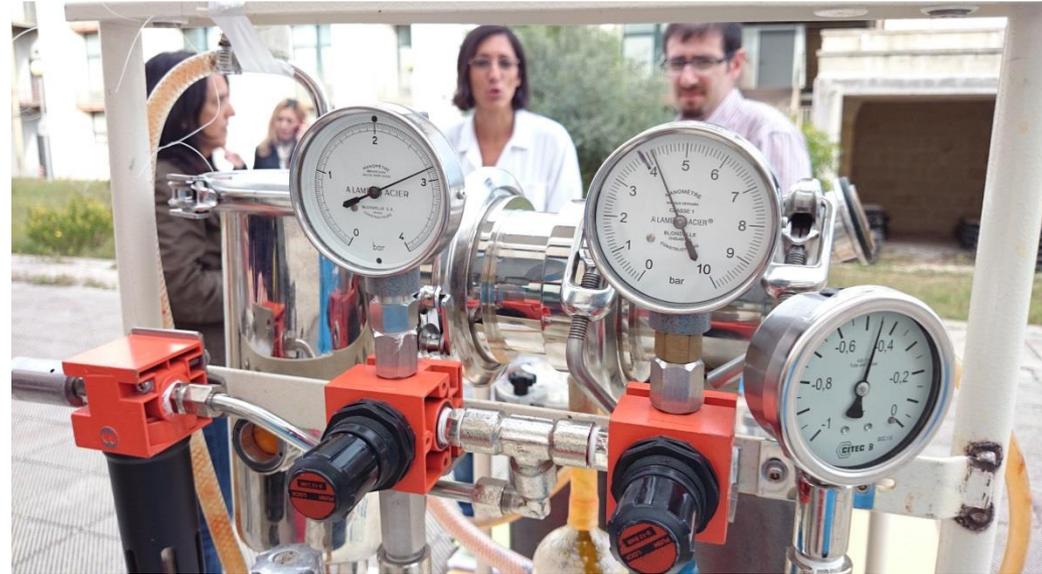
- Set up in-situ meteorological station to guide experimental design
- Input in CFD model FLUENT



- Synoptic wind direction
- Test site wind direction

# Aerosols emitted

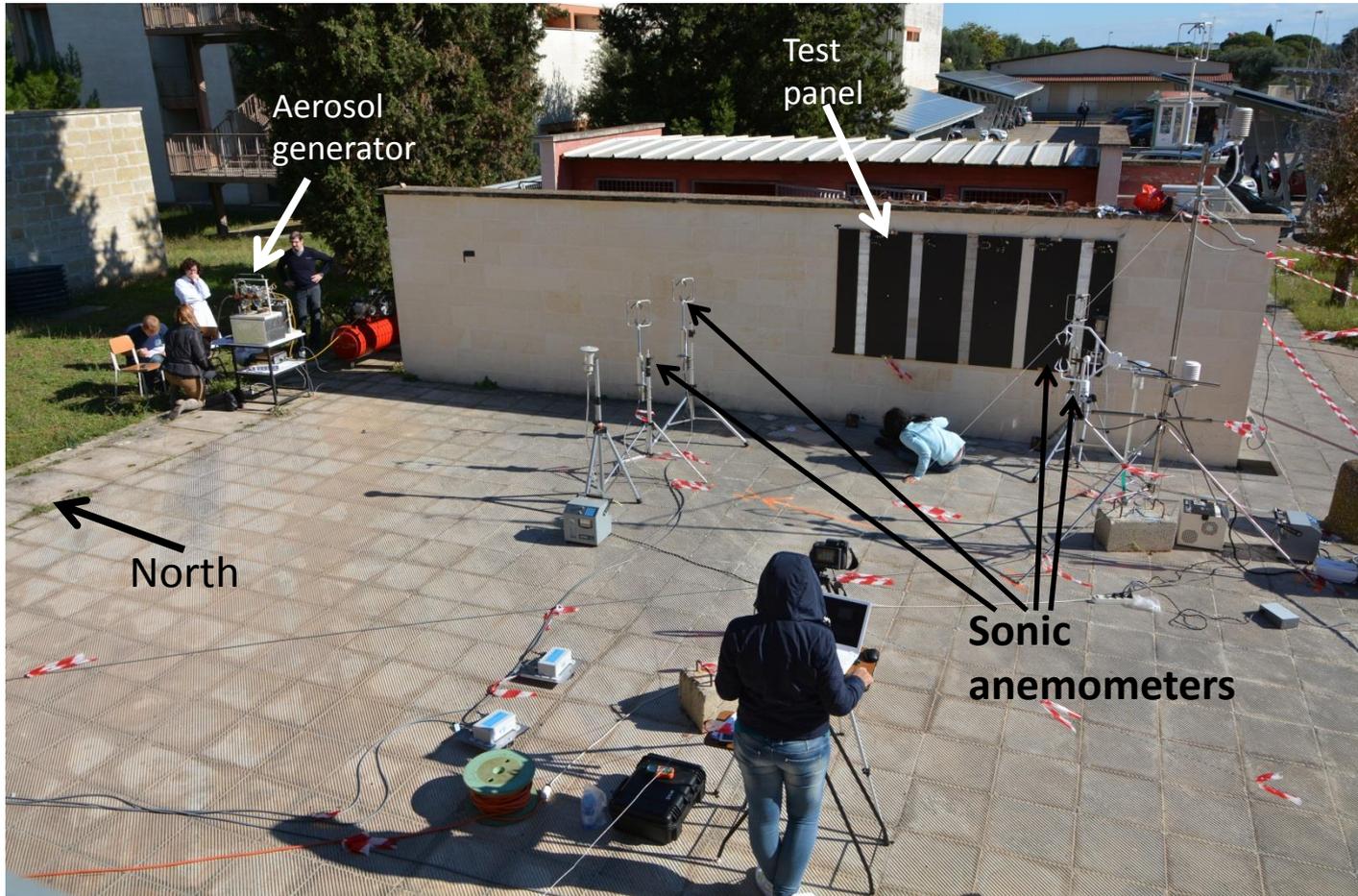
- Pneumatic generator of Fluorescein rented from TechSystemes
- Diameter:  $0.138 \mu\text{m}$
- Mass flow rate:  $33.9 \frac{\text{mg}}{\text{hr}}$
- Density:  $1.5 \frac{\text{g}}{\text{cm}^3}$



# Experimental set-up

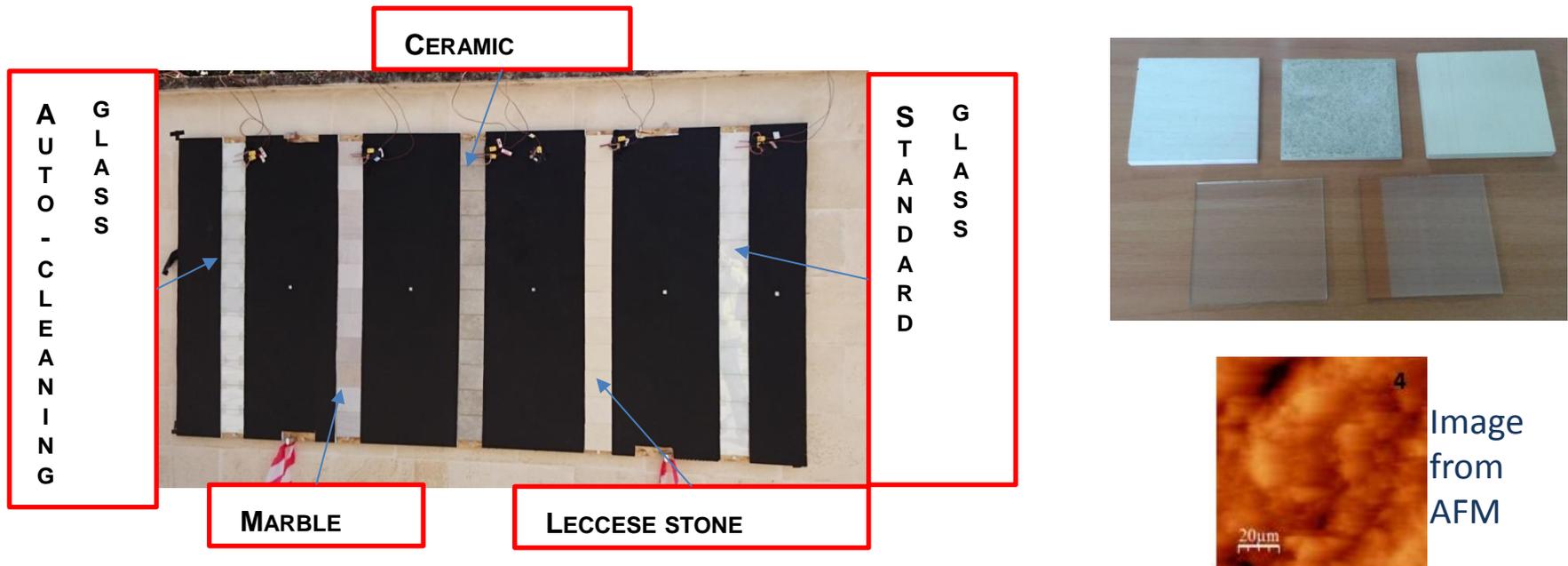


# Experimental set-up



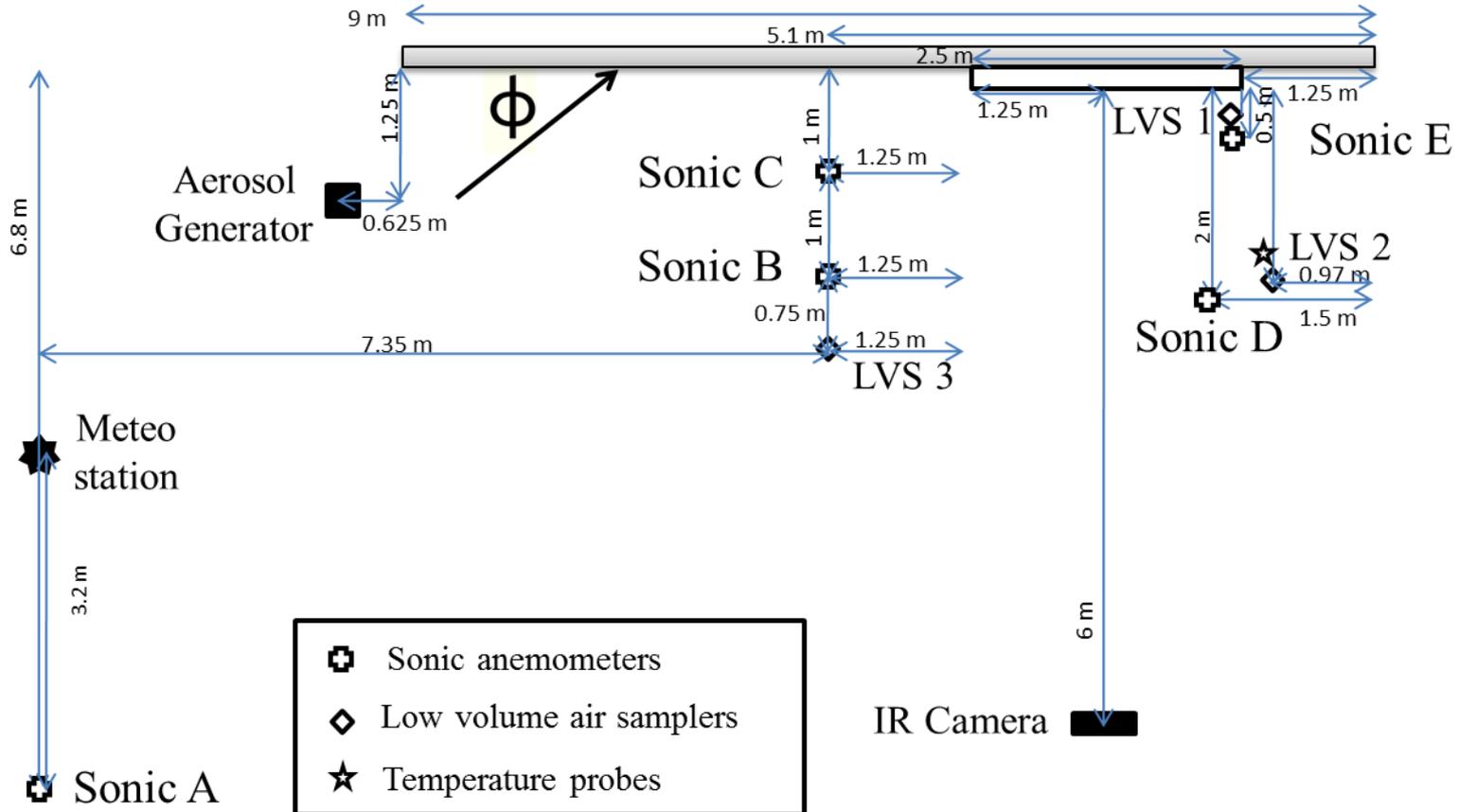
# Panel and materials

- Selected 2 glass types (same as SaliFa) and 3 additional common building materials – marble, ceramic, Lecce stone
- Constructed panel with wood and foam so no significant surface elevation changes at boundaries ( $\pm 2$  mm)



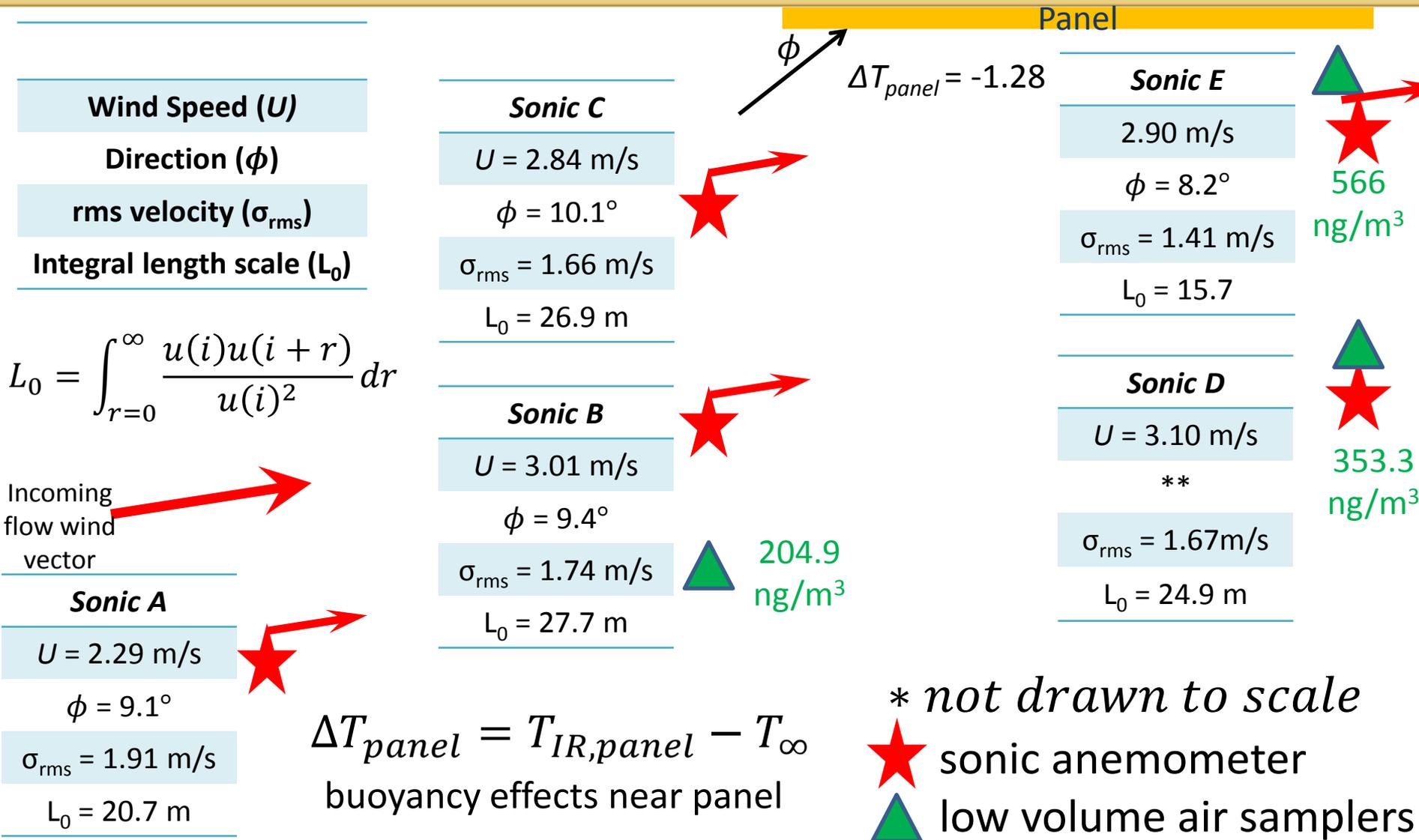
- Roughness height measurements for ceramic and marble via atomic force microscope reveals consistently  $\sim 0.8 \mu\text{m}$

# Plan view

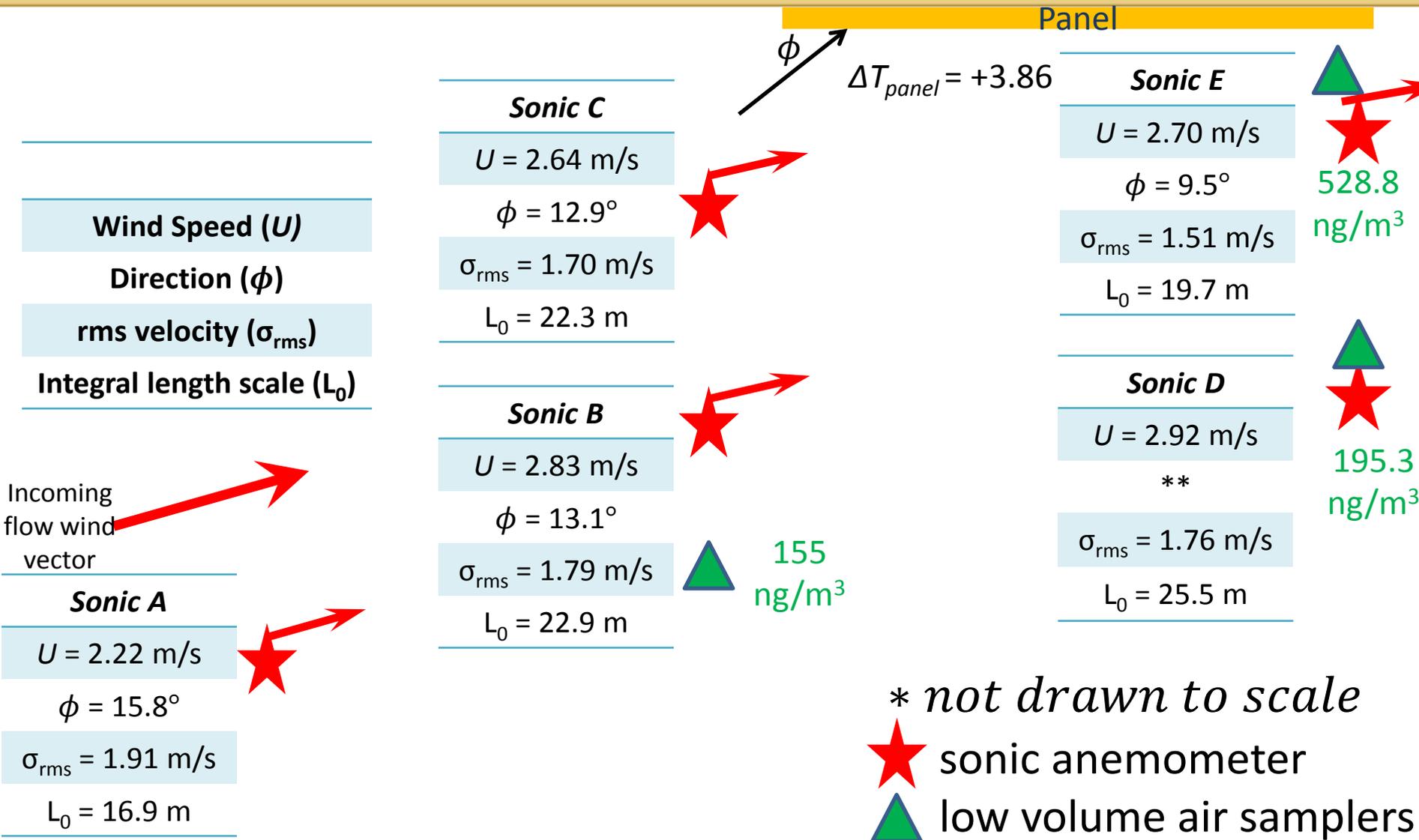


# **EXPERIMENTAL RESULTS: MICROMETEOROLOGY**

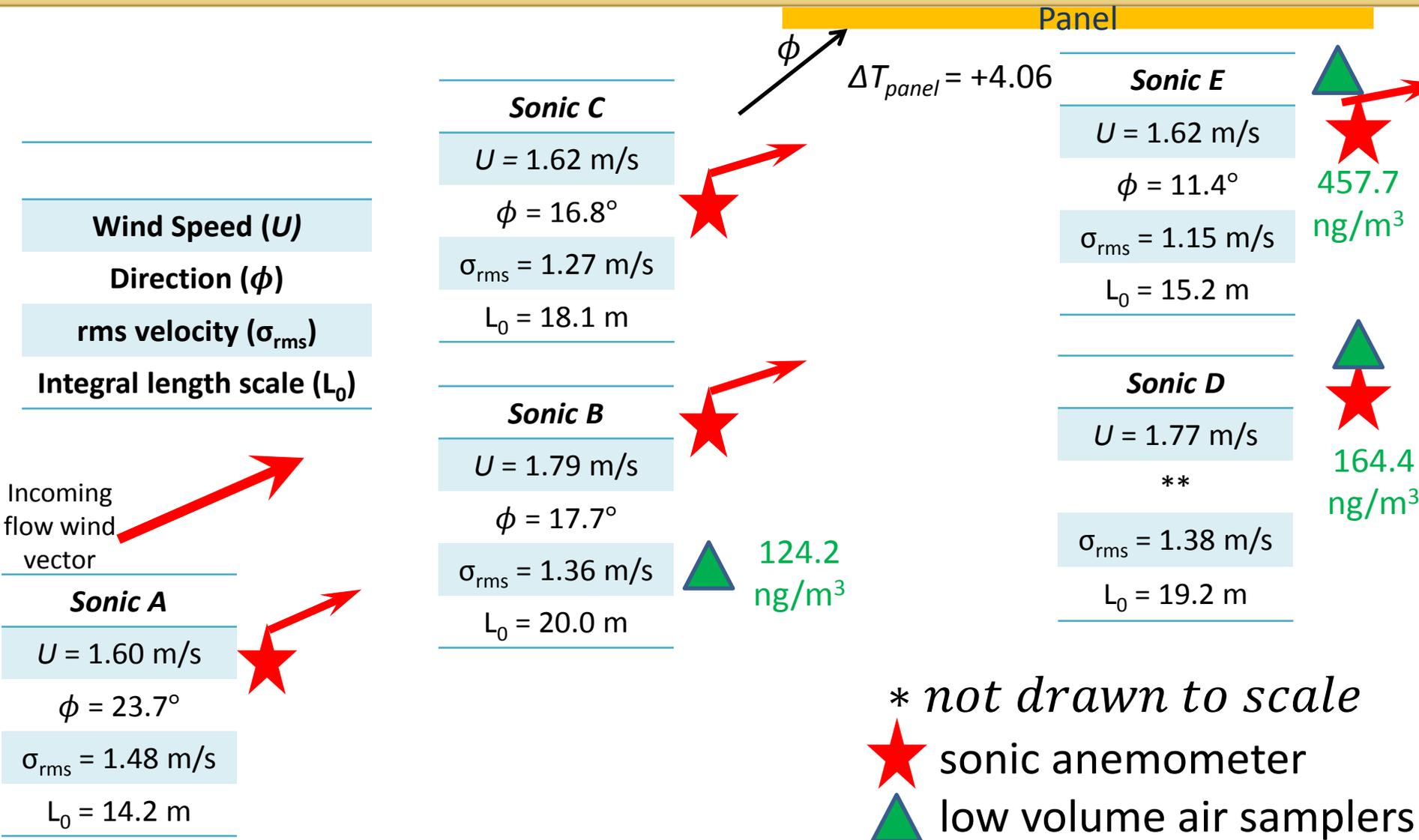
# Test 1



# Test 2



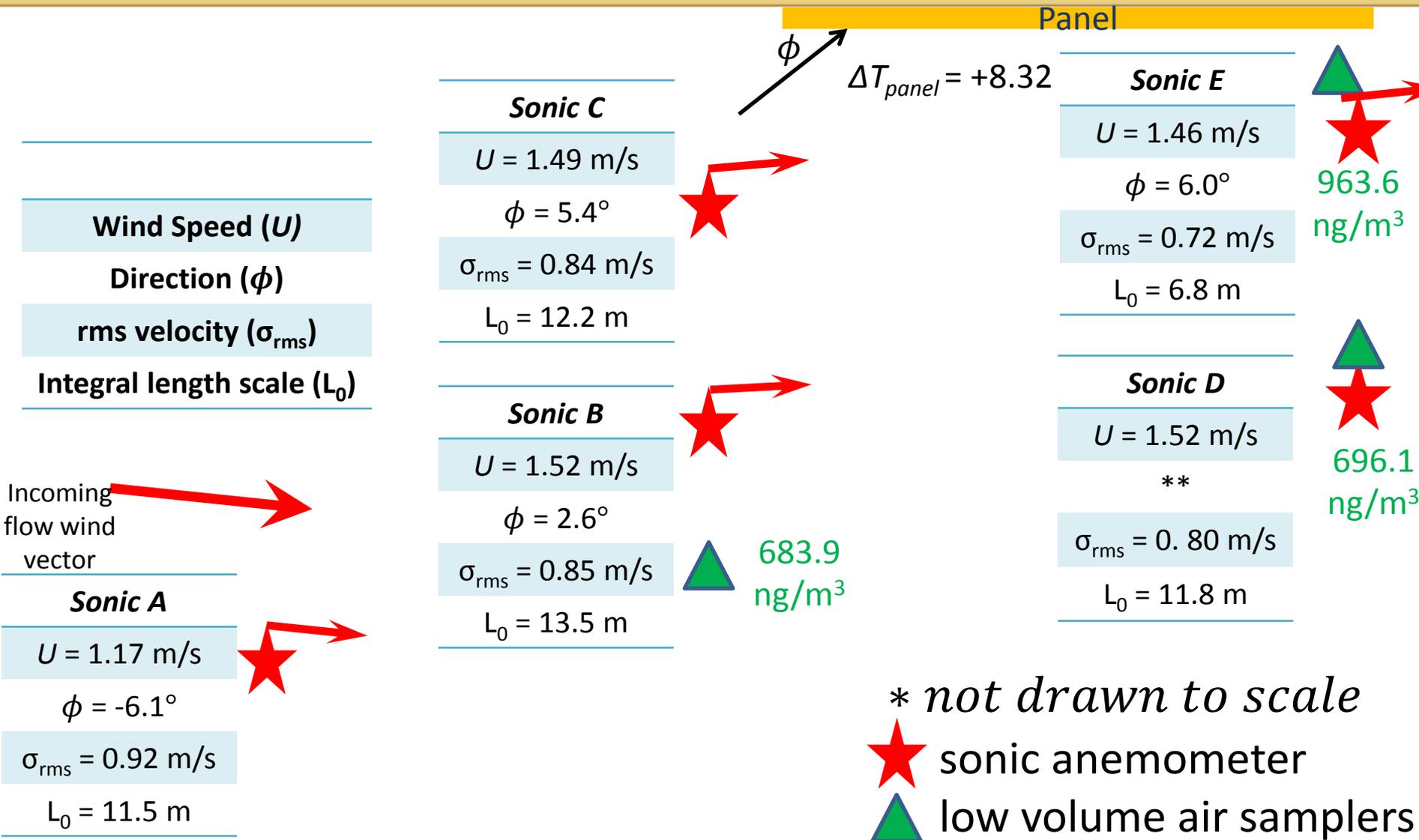
# Test 4



# Flow characteristics

- Tests 1, 2, and 4 similar
- Flow channelization along wall
- Wall acts as local sink of turbulent kinetic energy (TKE)
- Elongation of eddies parallel to wall
- Negative buoyancy in Test 1; positive buoyancy in Tests 2 & 4

# Test 3



\* not drawn to scale

-  sonic anemometer
-  low volume air samplers

# **EXPERIMENTAL RESULTS: DEPOSITION VELOCITY**

# Deposition velocity

- Material samples and LVS filters analyzed using spectrofluorometric technique
- $$V_d = -\frac{J}{C_\infty}$$
  - $J$  is mass flux onto surface ( $\text{kg m}^{-2} \text{s}^{-1}$ ), get from materials post-analysis
  - $C_\infty$  is concentration ( $\text{kg m}^{-3}$ ), take from LVS 1 assuming uniform near panel

Deposition Velocity ( $\text{m s}^{-1}$ )	Auto-cleaning glass	Standard glass	Marble	Ceramic
Test 1	$8.17 \times 10^{-3}$	$7.53 \times 10^{-3}$	$1.05 \times 10^{-3}$	$1.03 \times 10^{-3}$
Test 2	$5.27 \times 10^{-4}$	$6.71 \times 10^{-4}$	$6.56 \times 10^{-4}$	$2.94 \times 10^{-4}$
Test 3	$1.75 \times 10^{-4}$	$2.18 \times 10^{-4}$	$2.07 \times 10^{-4}$	$7.1 \times 10^{-5}$
Test 4	$4.16 \times 10^{-4}$	$5.11 \times 10^{-4}$	$2.44 \times 10^{-4}$	$2.49 \times 10^{-4}$
SaliFa2: Test 3	$\sim 1.65 \times 10^{-5}$	$\sim 2.05 \times 10^{-5}$	■	■

- Spans three orders of magnitude!

*\*\* These are preliminary results – chemical analysis is ongoing for Leccese stone results and quality control of other materials*

# **ANALYSIS: GOVERNING PARAMETERS**

# Dimensional analysis

$$V_d = F\{U, \phi, \sigma_{rms}, L_0, g\beta\Delta T_{panel}, \nu, \alpha, \xi_{mat}\}$$

$$\frac{V_d}{\sigma_{rms}} = F\left\{\phi, \xi_{mat}, \frac{UL_0}{\nu}, \frac{L_0^3 g\beta\Delta T_{panel}}{\nu^2}, \frac{\nu}{\alpha}\right\}$$

Reynolds, Grashof, and Prandtl numbers

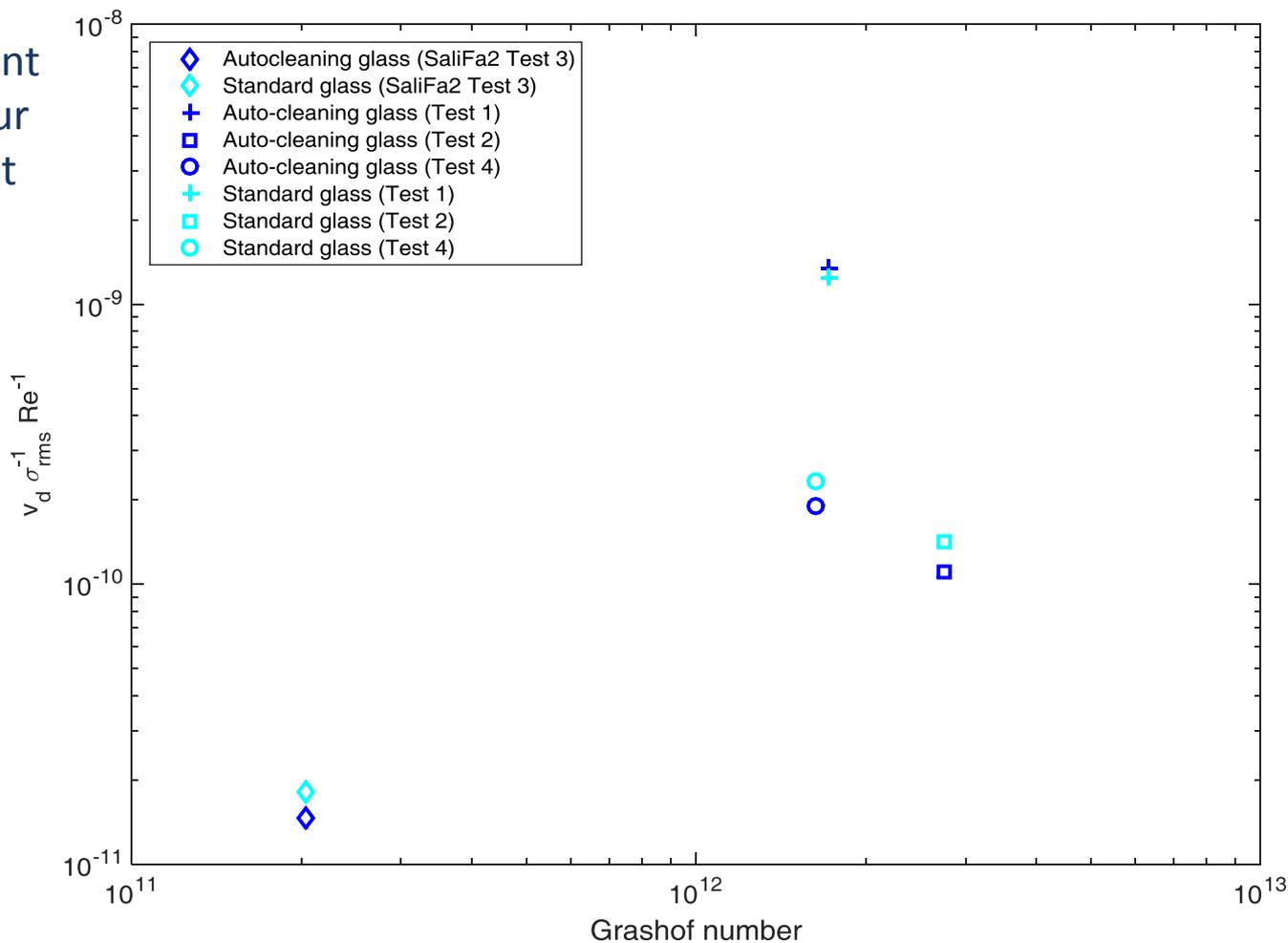
# Applying to our case

- $V_d = F\{U, \phi, \sigma_{rms}, L_0, g\beta\Delta T_{panel}, v, \alpha, \xi_{mat}\}$
- $\frac{V_d}{\sigma_{rms}} = F\left\{\phi, \xi_{mat}, \frac{UL_0}{v}, \frac{L_0^3 g\beta\Delta T_{panel}}{v^2}, \frac{v}{\alpha}\right\}$
- For Tests 1, 2, and 4,  $\phi$  was approximately constant ( $\sim 15^\circ$ )
- Can extract all needed parameters for single test from Maro et al. (2014) except  $L_0$  for which assumed constant energy dissipation ( $\sigma_{rms}^3 / L_0$ ) between our Test 4 and SaliFa2 Test 3

Test #	Reynolds Number (Re)	Grashof Number (Gr)	Wind Angle ( $\phi$ )
1	$3.2 \times 10^6$	(-) $1.7 \times 10^{12}$	9.1
2	$2.5 \times 10^6$	$2.7 \times 10^{12}$	15.8
3	$9.8 \times 10^5$	$2.4 \times 10^{12}$	-6.1
4	$1.5 \times 10^6$	$1.6 \times 10^{12}$	23.7
SaliFa2_3	$8.9 \times 10^5$	$2.0 \times 10^{11}$	? $\sim \geq 0$

# Relating dimensionless parameters

$\xi_{mat}$  constant  
between our  
experiment  
and SaliFa

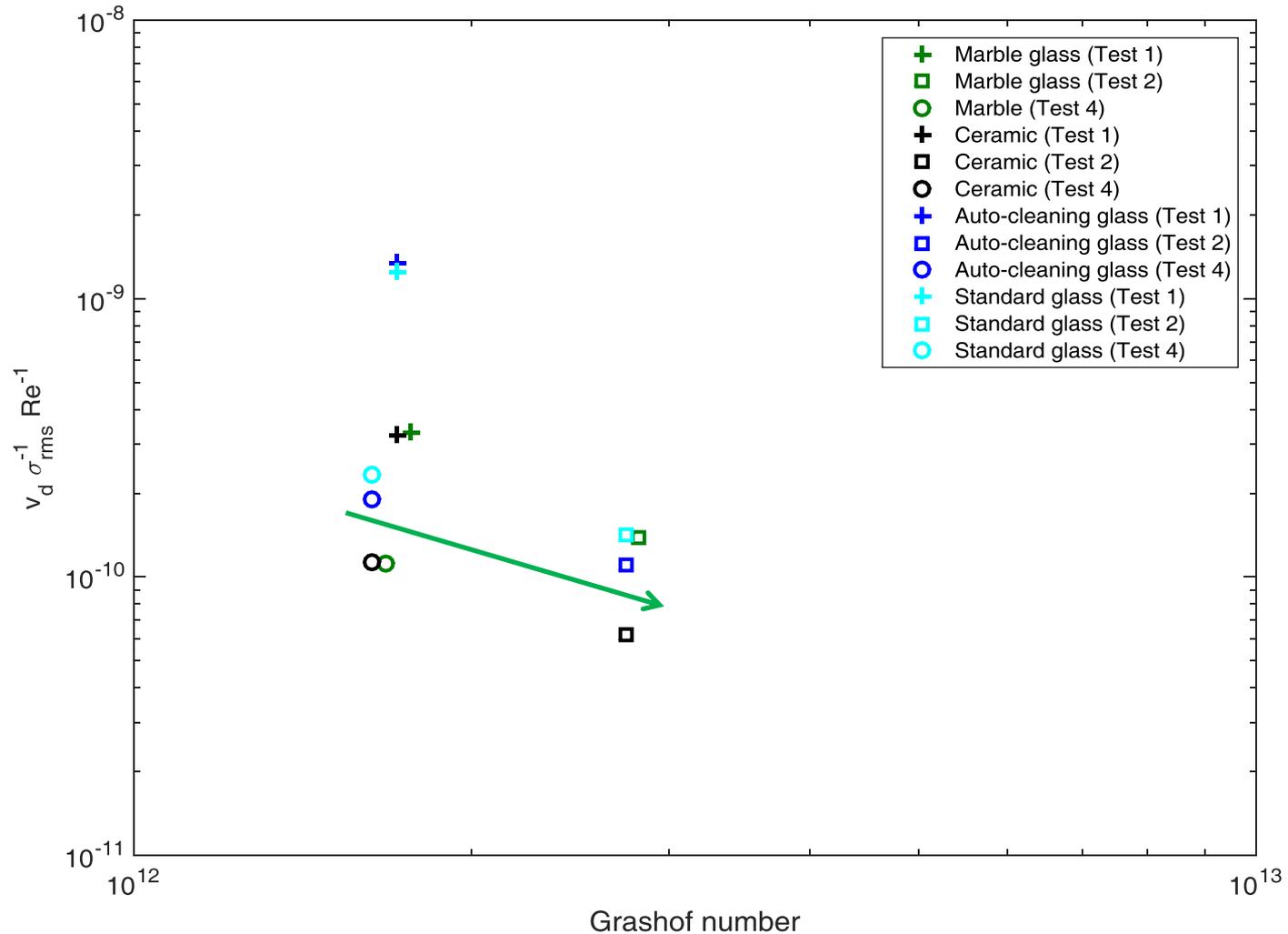


$$\frac{V_d}{\sigma_{rms}} \propto Re^m Gr^n$$

# Relating dimensionless parameters

- Test 1 stands out because only case where  $\Delta T_{panel}$  is negative so divergence is attributable to thermophoresis (Di Nicola et al. 2016)
- Consistent trend between standard and auto-cleaning glass (except Test 1) – self-cleaning properties rely on sunlight (Parkin and Palgrave 2005)
- SaliFa order of magnitude difference with our experiments on x-axis and y-axis

# Relating dimensionless parameters



# CONCLUSIONS

# Conclusions

- At large Grashof numbers ( $>10^{12}$ ), the deposition velocity depends principally on sign (+/-) of buoyancy due to thermophoretic effects
- When surface heated, at high Gr and Re, deposition velocity may be approximately constant, independent on Gr and even the material properties
- More experiments are needed at intermediate Gr to address discrepancies between results
- Just addressed principally one micrometeorological scenario – there are many more to solve with further experiments, but challenges still exist in conducting these experiments
- Introduction of an approach which helps to quantify near-wall deposition processes based on local-scale urban flow regime for dispersion modelling

# Acknowledgements

- Reseaux ([www.reseaux.it](http://www.reseaux.it)) for funding most of the project costs



- I was supported by the US Department of Defense (DoD) through the National Science & Engineering Graduate Fellowship (NDSEG) Program
- The Graduate School of the University of Notre Dame supported my participation via Notebaert Professional Development Awards

**Thank you**



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