

A SENSITIVITY ANALYSIS FOR A LAGRANGIAN PARTICLE DISPERSION MODEL IN EMERGENCY-RESPONSE TEST CASES

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Outline

- ***Numerical experiments in the frame of the COST ES1006 action***
- ***Class of models and specific model considered***
- ***Different setup and applications - results***
- ***Conclusions***

COST Action ES1006 (2011-2015)

Evaluation, improvement and guidance for the use of local-scale emergency prediction and response tools for airborne hazards in built environments

Some ideas behind the action

- test different modeling technologies at local scale
- build test cases in order to perform such comparisons

Being the same model technology available from different research groups, a «sensitivity analysis» was conducted in order to evaluate the effects of different configurations of the models and different initial conditions.

How the model setup generated independently by different users can affect output results



Wind tunnel experiments (EWTL, Inst. Met., Hamburg University)

Michelstadt (Wind tunnel)



A **typical European urban site** is reproduced.

Several **continuous** and **puff releases** from six different source locations: concentration measured at more than 30 points

Non-blind and **blind** tests

CUTE 3 (Wind Tunnel)



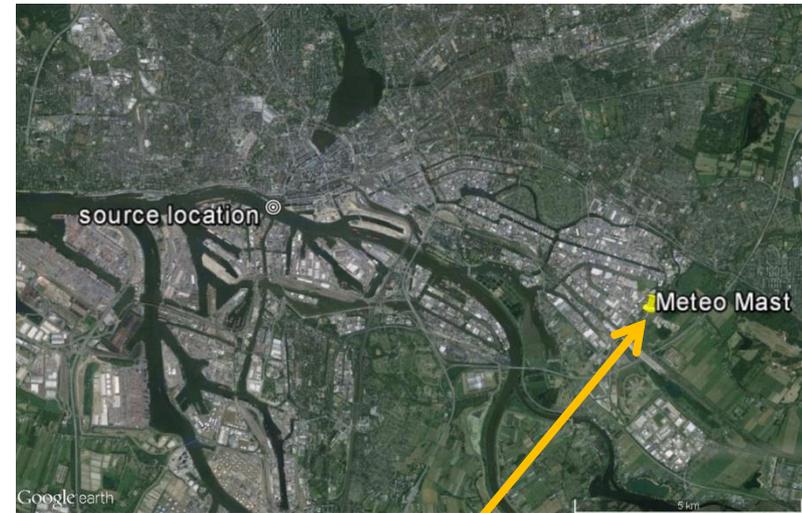
A **real European city** is reproduced.

Several **continuous** and **puff releases** from three different source location: concentration measured at more than 30 points

Blind tests

CUTE 1 (real atmosphere)

Different meteo data available



Continuous 45-minutes release of SF6 with a flow rate of 2 g/s, from a boat towards the harbor area.

Concentration detected by 20 measurement stations located at different positions.

Each measurement station had 9 bag samplers. Each bag was filled for 10 minutes => 10-minute average values. Only **Blind** tests

10, 50, 110, **175**, 250m

COST ES1006 took into account in general three type of models

Model type	Flow modelling approach	Dispersion modelling approach
Type I	models that do not resolve the flow between buildings	Gaussian
Type II	models for which the flow is resolved diagnostically or empirically, although not dynamically resolving the flow between buildings	Lagrangian
Type III	models that resolve the flow between buildings	Eulerian

this particular activity considered only one Lagrangian Particle Dispersion Model driven by a diagnostic flow model

**the *SPRAY* stochastic LPDM
in its microscale version with obstacles**

General configuration of sensitivity experiments

1. Michelstadt experiment

- Different modeling setup given by 3 independent groups
 - ✓ wind speed vertical profiles
 - ✓ background turbulence
 - ✓ horizontal and vertical model resolution
 - ✓ time step for particle advancing
 - ✓ number of particles

2. CUTE 1 experiment

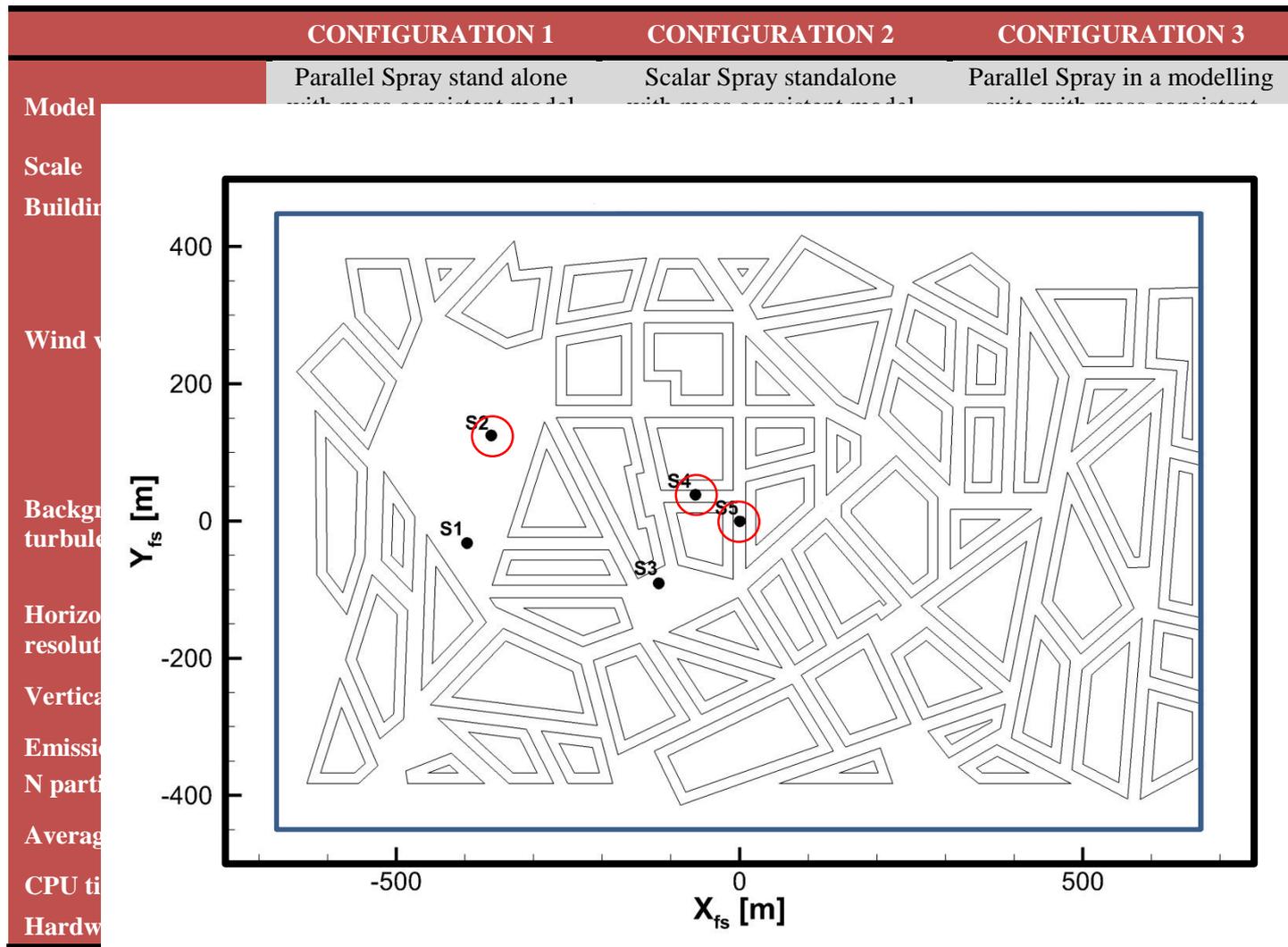
- One group produced simulations using different entering flow
 - ✓ vertical profile derived from one distributed wind speed and direction
 - ✓ vertical wind profile (speed and direction) measured by a meteorological mast

2. CUTE 1 and CUTE 3 experiments

- One group produced simulations using different turbulence levels due to a different terrain roughness considered
 - ✓ $z_0 = 1$ m
 - ✓ $z_0 = 0.1$ m

Michelstadt experiment

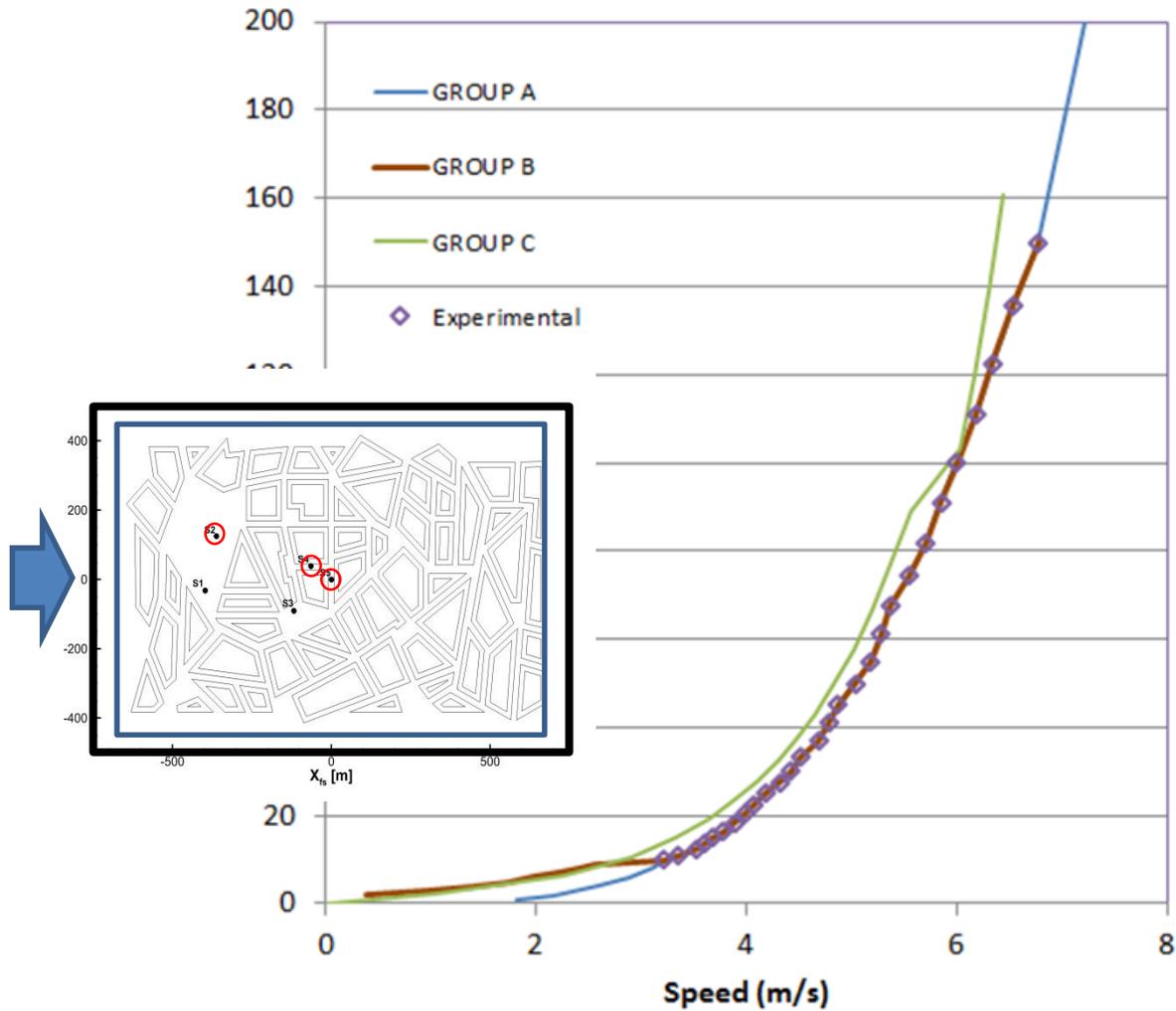
Three different configurations (1)



Continuous (S2, S4, S5) non-blind releases

Michelstadt experiment

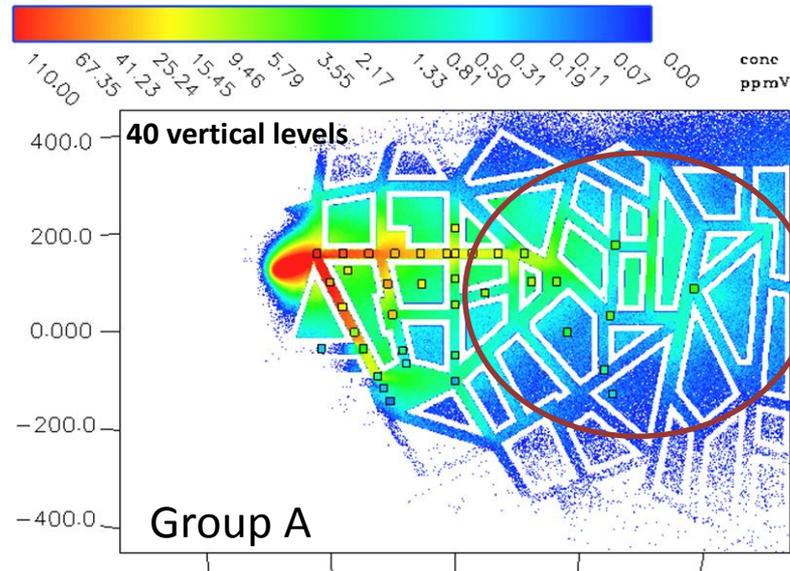
Three different configurations (2)



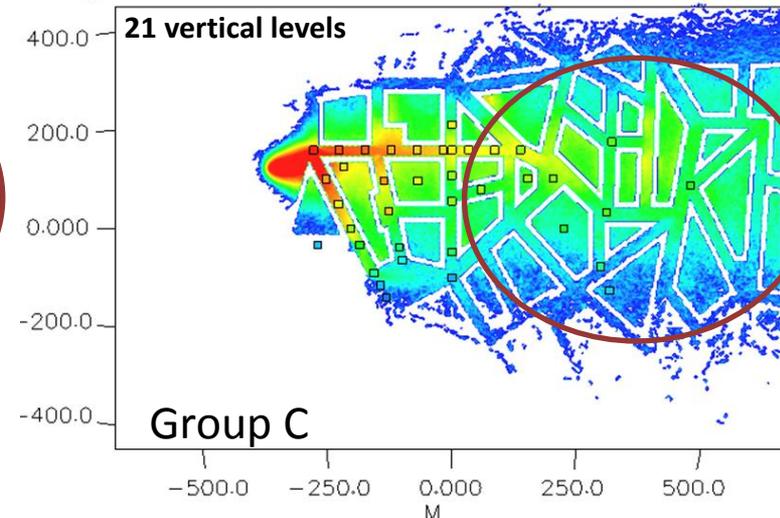
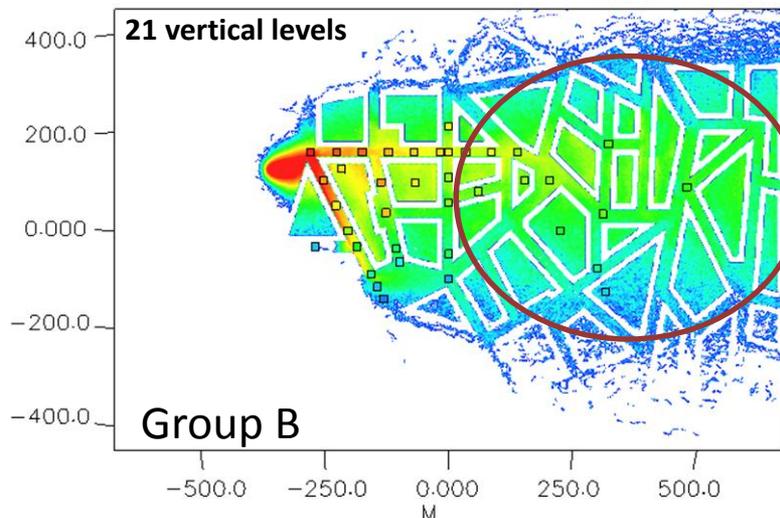
Inlet wind speed profiles

Michelstadt experiment

Results – ground level concentration maps vs experimental data (1)

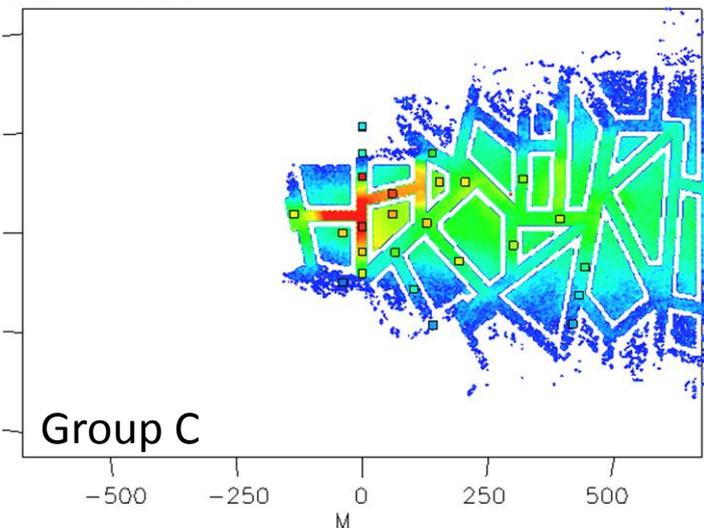
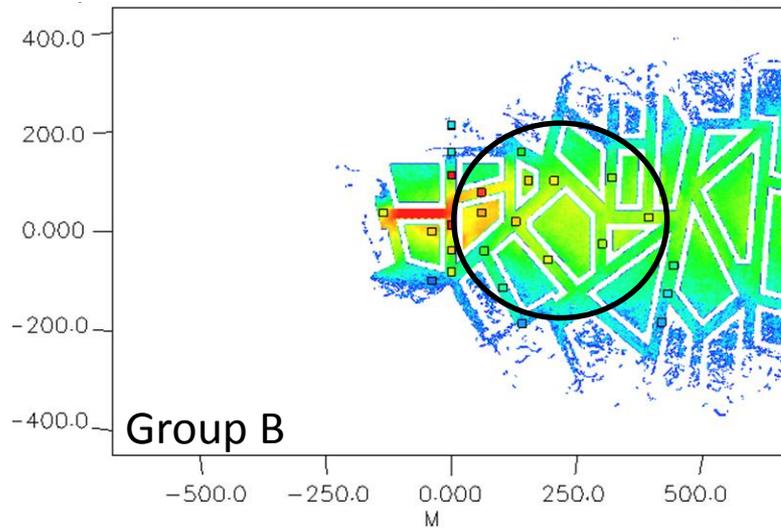
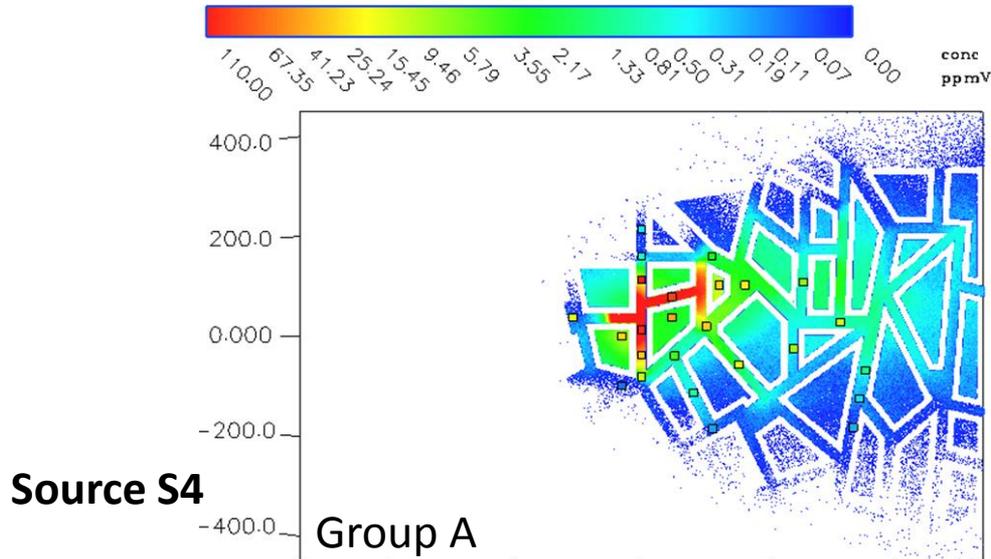


Different behaviors far from the source
Group A has a finer vertical mesh



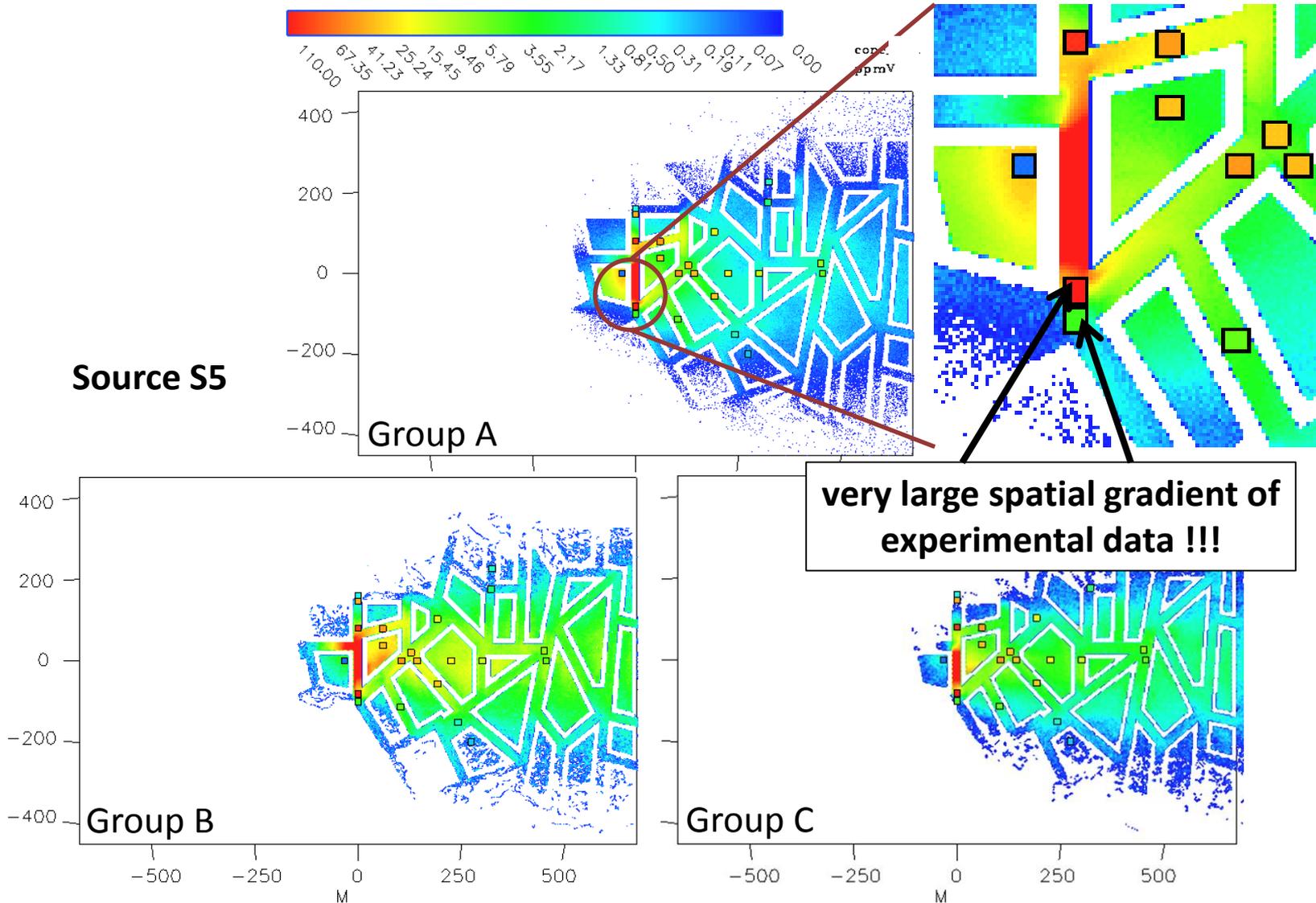
Michelstadt experiment

Results – ground level concentration maps vs experimental data (2)



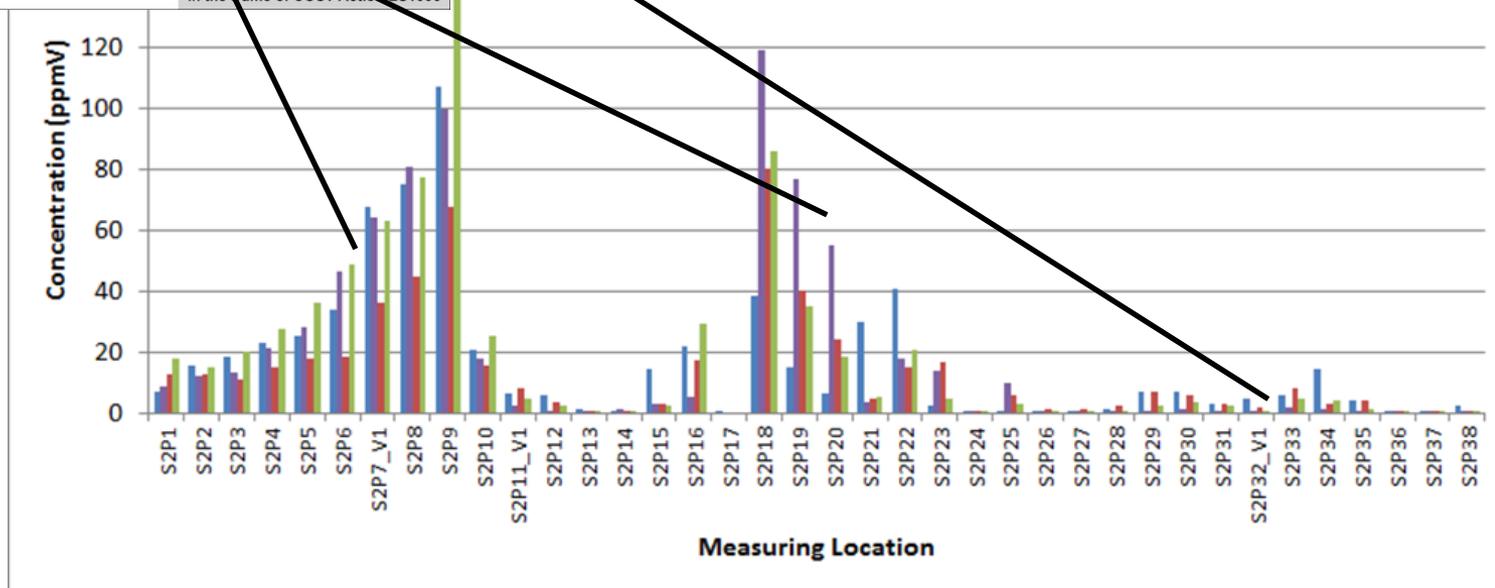
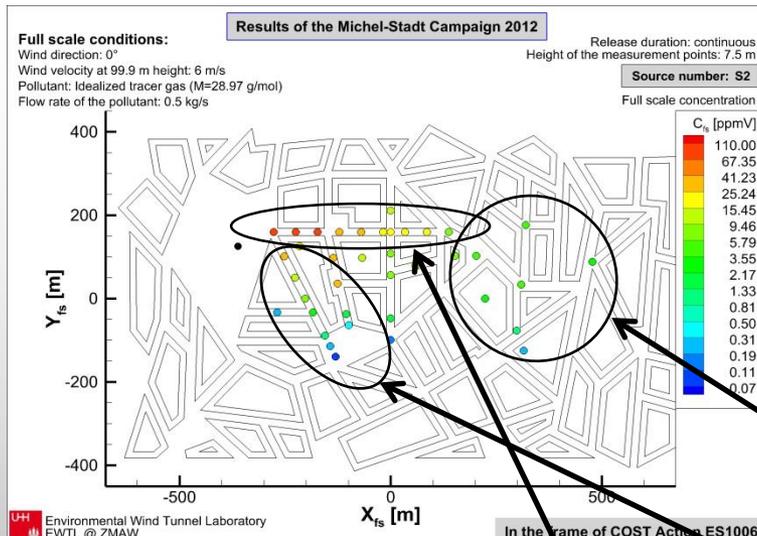
Michelstadt experiment

Results – ground level concentration maps vs experimental data (3)



Michelstadt experiment

Results – point to point variability – Source S2 continuous



COST Action ES1006



Michelstadt experiment

Results – model to model variability

The following Index of Agreement IA has been computed for each pair of models

$$IA = 1 - \left[\frac{\sum_{i=1}^N (C'_{Gx_i} - C'_{Gy_i})^2}{\sum_{i=1}^N (|C'_{Gx_i}| + |C'_{Gy_i}|)^2} \right]$$

$N = \text{Number of concentration pairs}$
 $0 < IA < 1$

Doran, J.E. and T.W. Horst (1985): An evaluation of Gaussian plume-depletion models with dual-tracer field measurements. Atmos. Environ. 19, 939-951

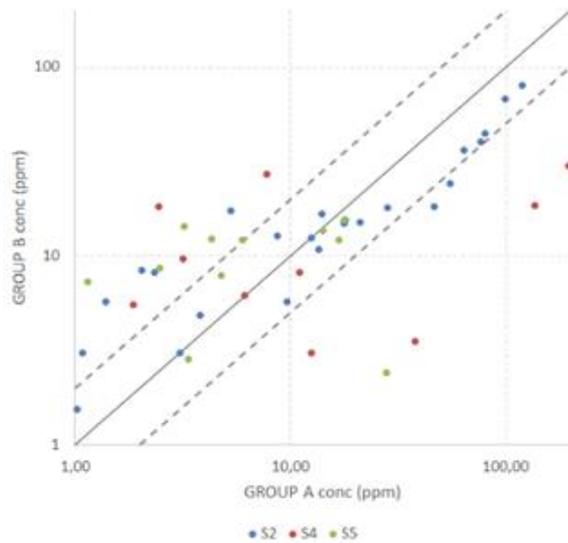
where $C'_{G_i} = C_{G_i} - \overline{C_{G_i}}$ is the deviation of the concentration for each Group x or y

IA	GROUPS		
	A vs B	A vs C	B vs C
Source S2	0.92	0.95	0.90
Source S4	0.40	0.91	0.54
Source S5	0.63	0.74	0.94
All sources	0.69	0.93	0.80

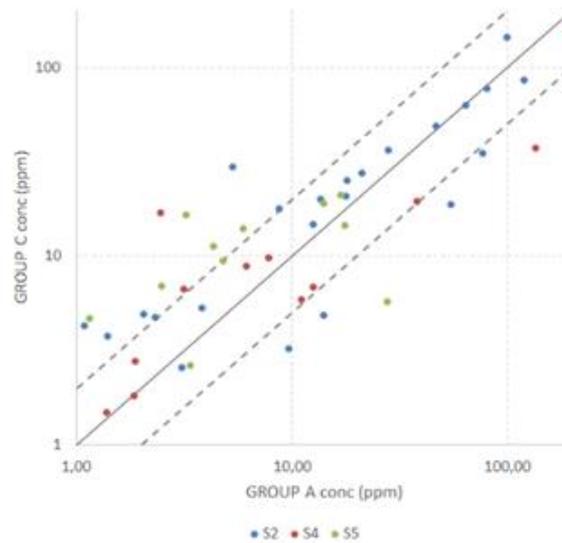
Michelstadt experiment

Results – Group-to-Group scatter diagrams

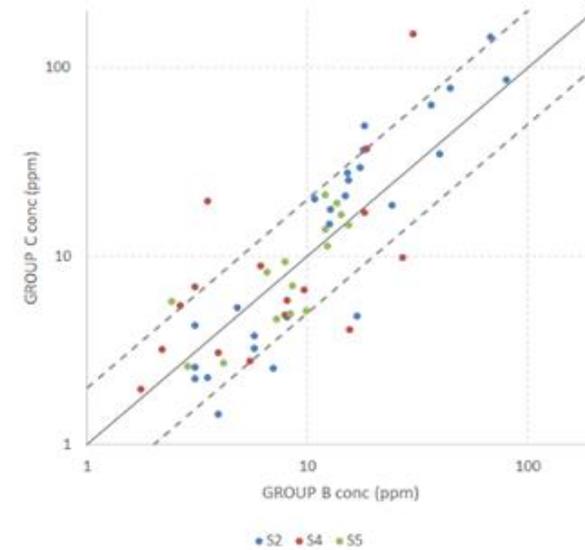
Group A vs Group B



Group A vs Group C

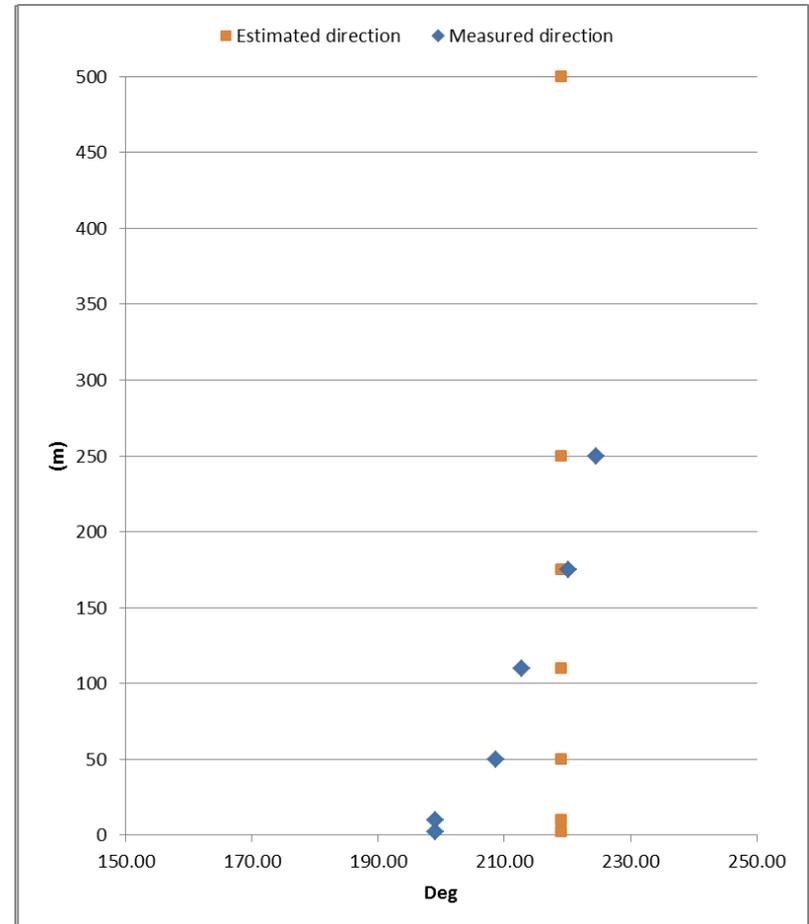
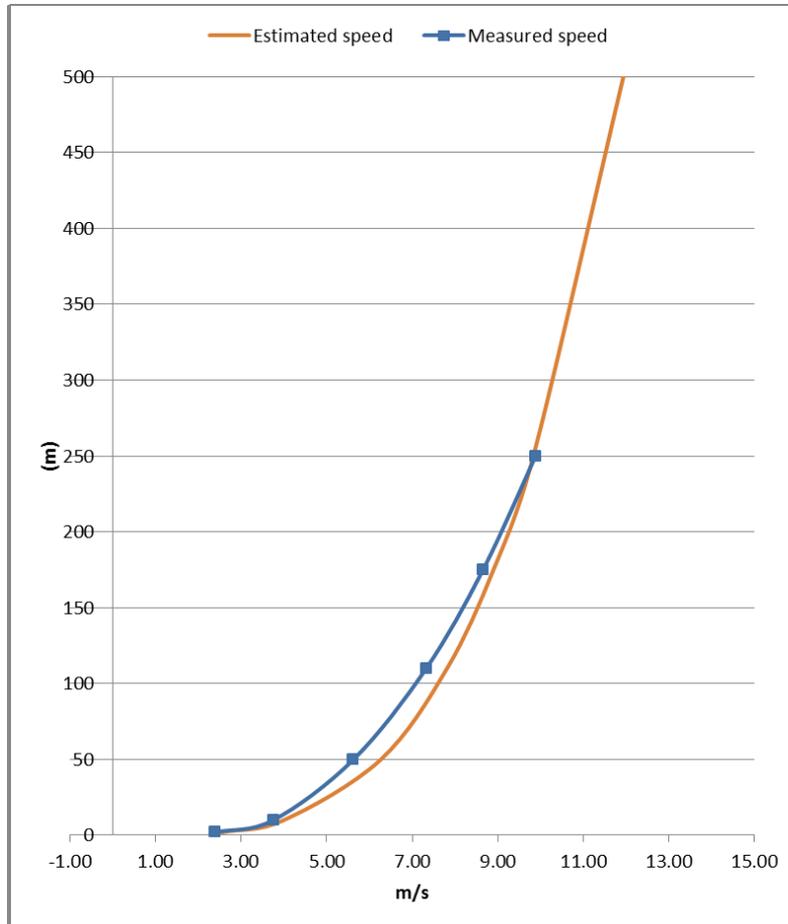


Group B vs Group C



CUTE 1 experiment

Two different inlet wind profiles



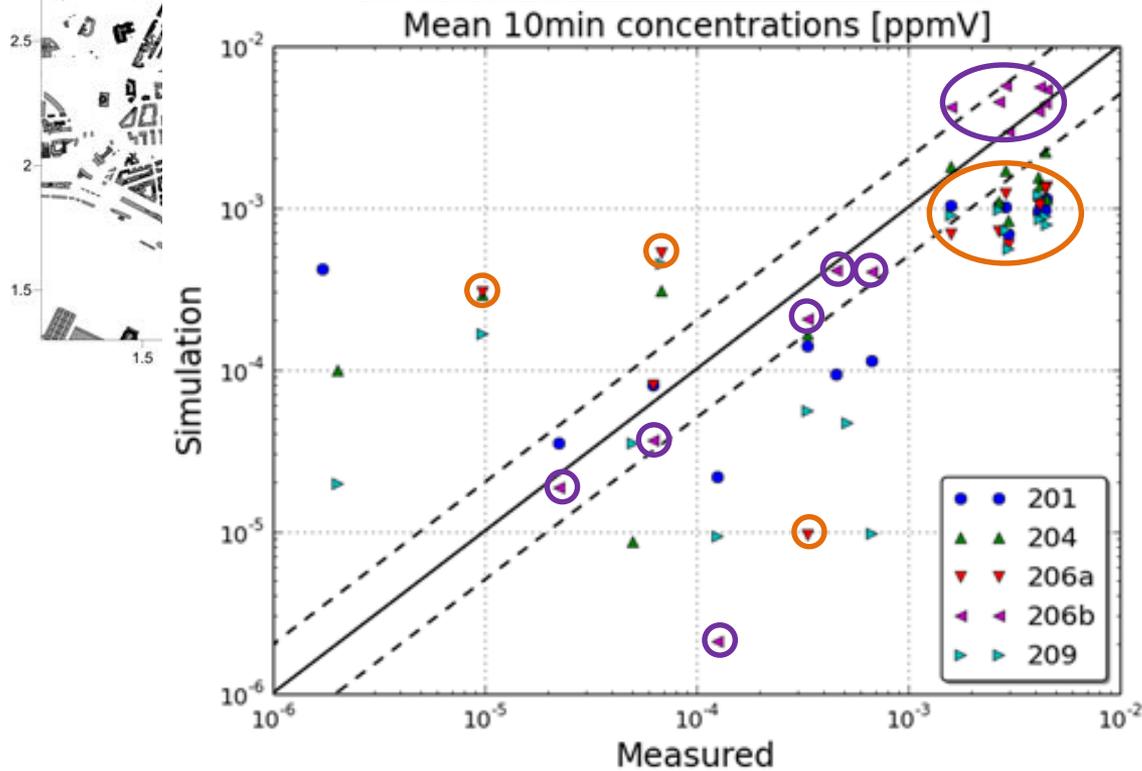
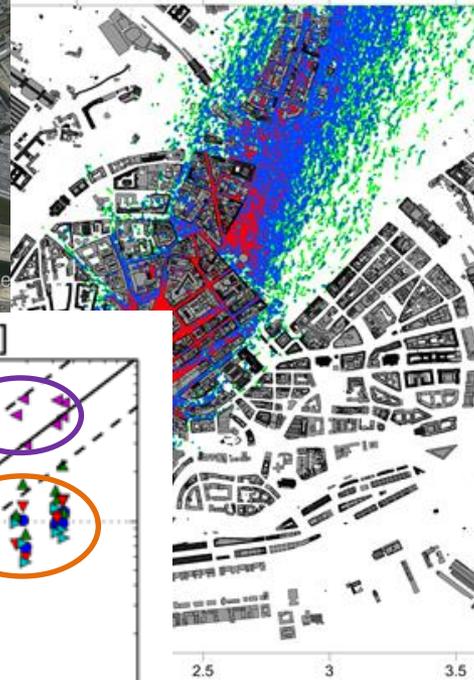
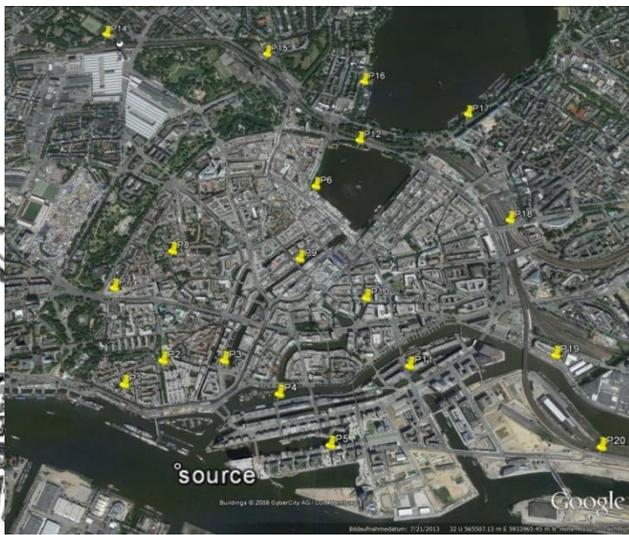
Wind direction given at 175 m above ground= 219 °

Wind direction measured by the mast = from 199 ° to 224 °

profile 1

profile 2

ent



wind profile 2

Wind Profile 1
Wind Profile 2

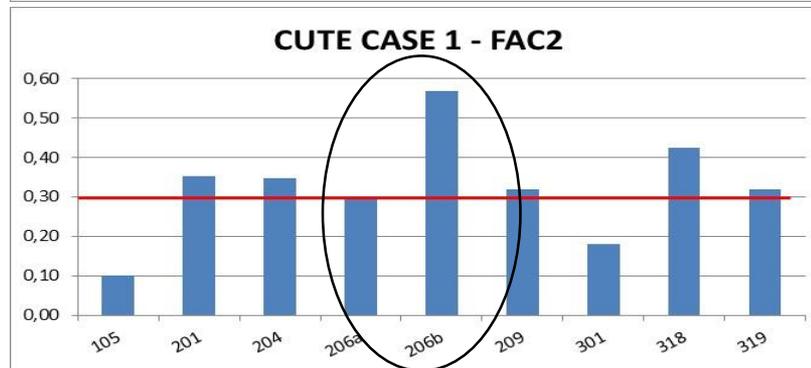
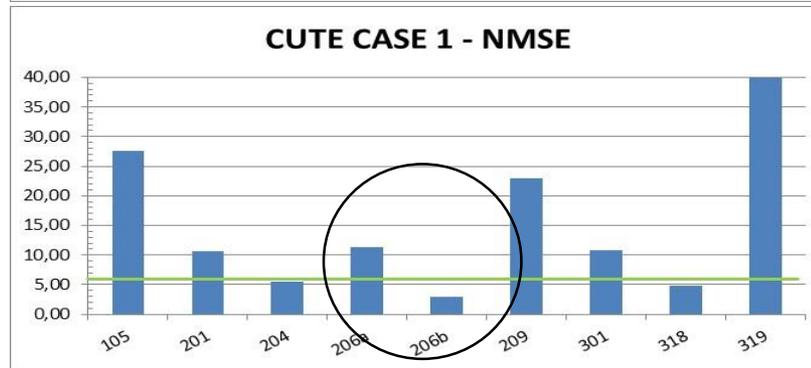
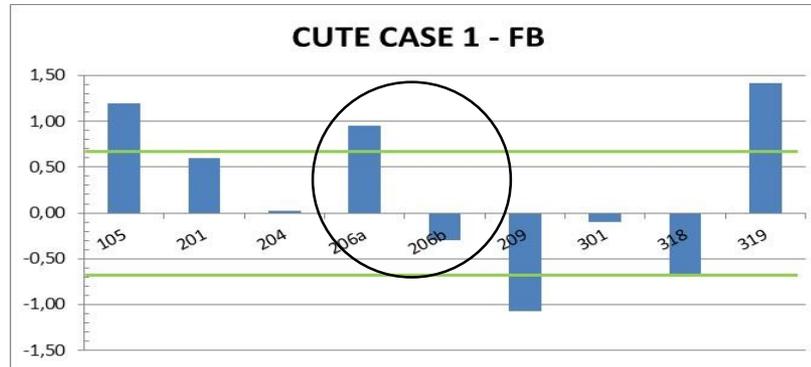
CUTE 1 experiment

Results – statistical indexes

$$FB = \frac{\overline{\Phi_o} - \overline{\Phi_p}}{0.5(\overline{\Phi_o} + \overline{\Phi_p})} = \frac{\overline{\Phi_o - \Phi_p}}{0.5(\overline{\Phi_o} + \overline{\Phi_p})}$$

$$NMSE = \frac{(\overline{\Phi_o} - \overline{\Phi_p})^2}{\overline{\Phi_o} \cdot \overline{\Phi_p}}$$

fraction of data that satisfy $0.5 \leq \frac{\Phi_p}{\Phi_o} \leq 2$



206b (Wind Profile 2)
shows the best
performance



CUTE 1 and CUTE 3 experiments

Two different inlet turbulence profiles



For both case Neutral Atmosphere – two different roughness values

Turbulence profile 1 - $z_0=1\text{m}$:

CUTE 1 (Field case)

$u_* = 1.31 \text{ m/s}$; $\text{TKE}(z=10 \text{ m}) = 6.4 \text{ m}^2/\text{s}^2$

CUTE 3 (Wind tunnel case)

$u_* = 1.26 \text{ m/s}$; $\text{TKE}(z=10 \text{ m}) = 5.9 \text{ m}^2/\text{s}^2$

Turbulence profile 2 - $z_0=0.1\text{m}$:

CUTE 1

$u_* = 0.33 \text{ m/s}$; $\text{TKE}(z=10 \text{ m}) = 0.4 \text{ m}^2/\text{s}^2$

CUTE 3

$u_* = 0.31 \text{ m/s}$; $\text{TKE}(z=10 \text{ m}) = 0.39 \text{ m}^2/\text{s}^2$

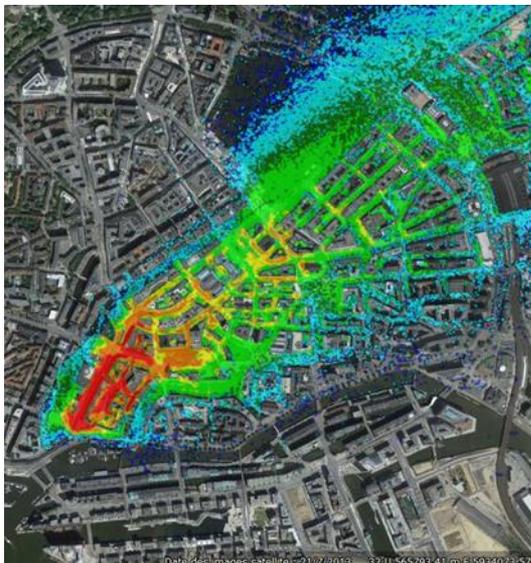
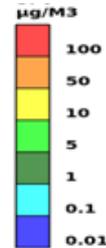
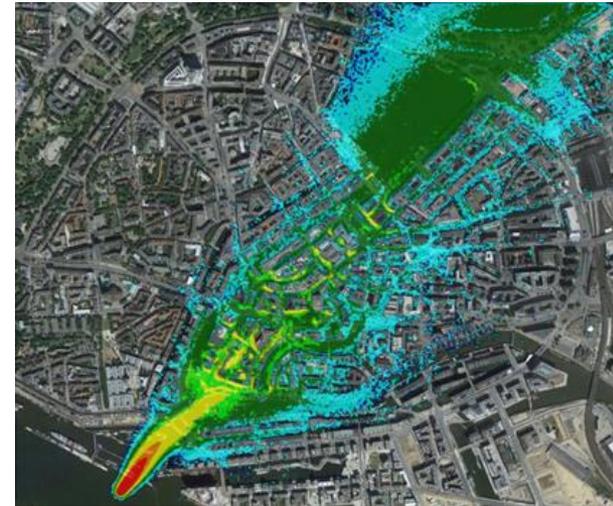
Variation is quite large

CUTE 1 and CUTE 3 experiments

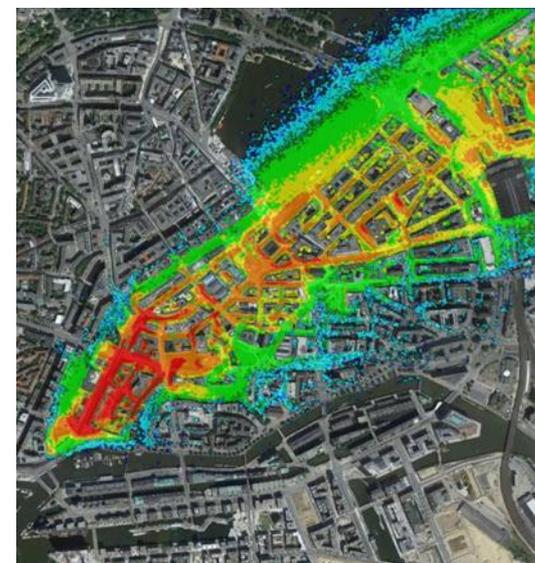
Results – concentration maps



CUTE 1



CUTE 3



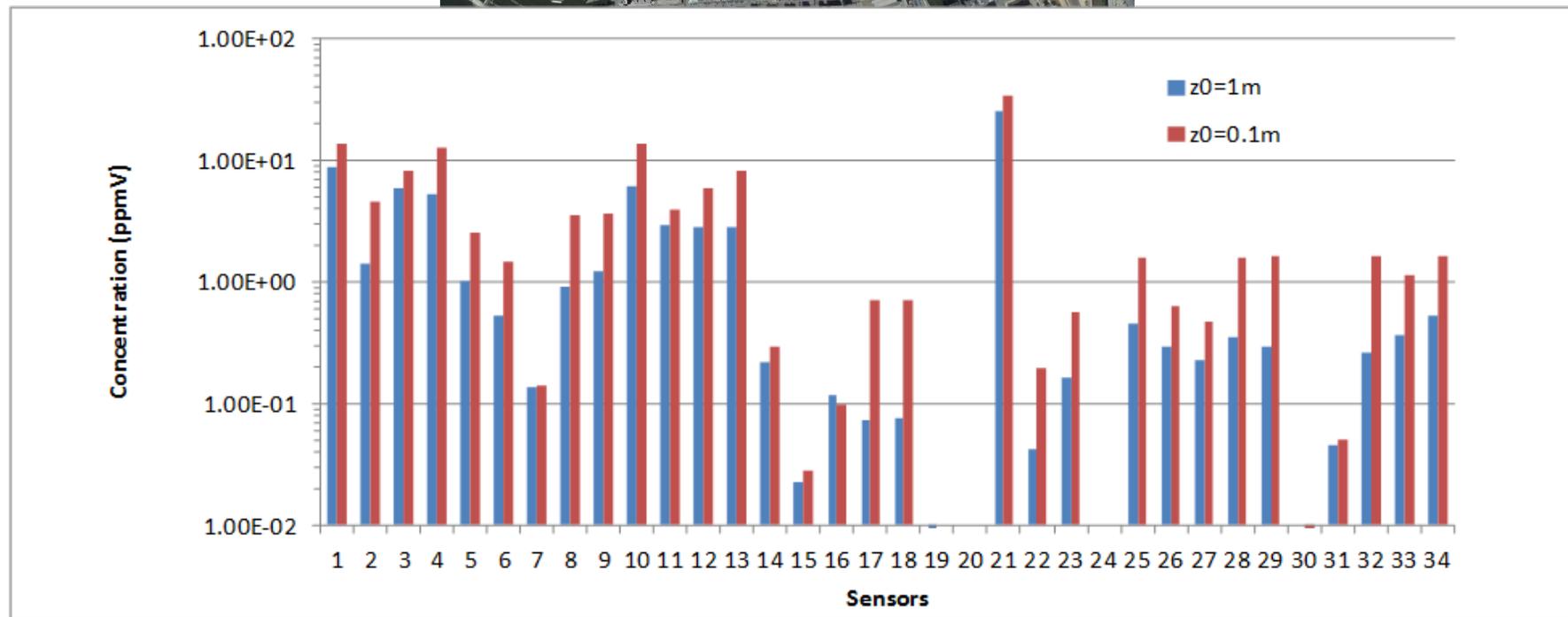
Inlet turbulence profile 1

Inlet turbulence profile 2



Cute 3 experiment

Results – Concentrations at sampler positions



maximum variation of the order of 25/30 %, but not for larger concentration values

SOME CONCLUSIONS

This cannot be a 'conclusive' work, but even with such a small number of analyzed cases, some useful tips can be taken

- besides the physical quantities, there are key quantities handled by the users changing and improving the performances, such as the number of particles, horizontal and vertical grid resolutions
- a parallel configuration allows for substantial reduction of the computational time allowing the use of more refined parameters or faster simulations
- the availability of more precise or sophisticated data (wind profiles, turbulence characterization) can also improve simulation results, but sometimes not in a decisive manner.

In spite of the highlighted differences, the tested dispersion models show at the end to be robust. Even using independent different configurations, the quality of the results is comparable and the simulations provide overall consistent output

