

POLLUTION DISPERSION PREDICTION FOR THE MUST WIND TUNNEL EXPERIMENT WITH ANISOTROPIC ALGEBRAIC MODELS FOR TURBULENT SCALAR FLUXES

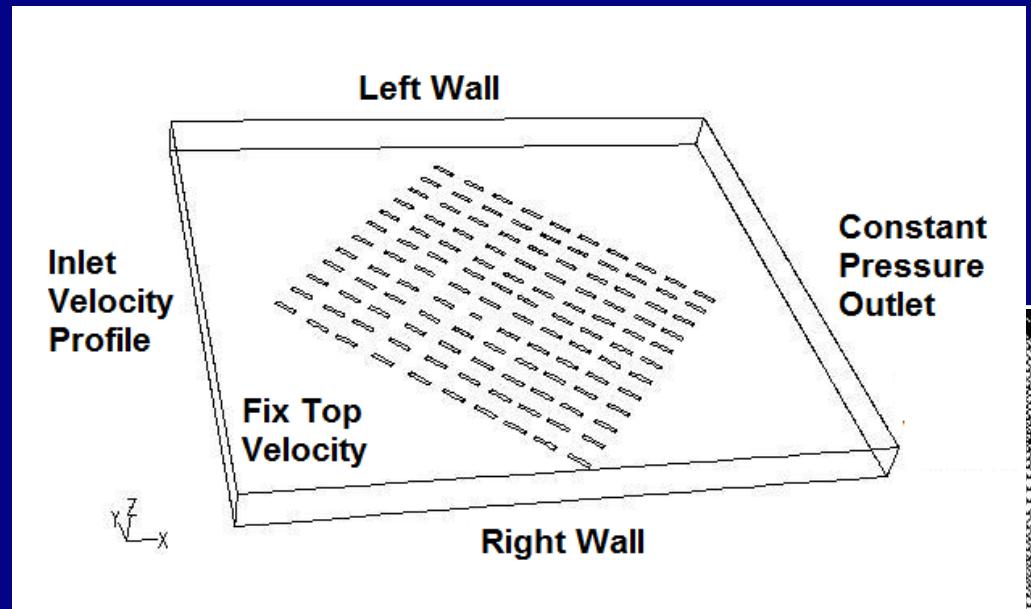
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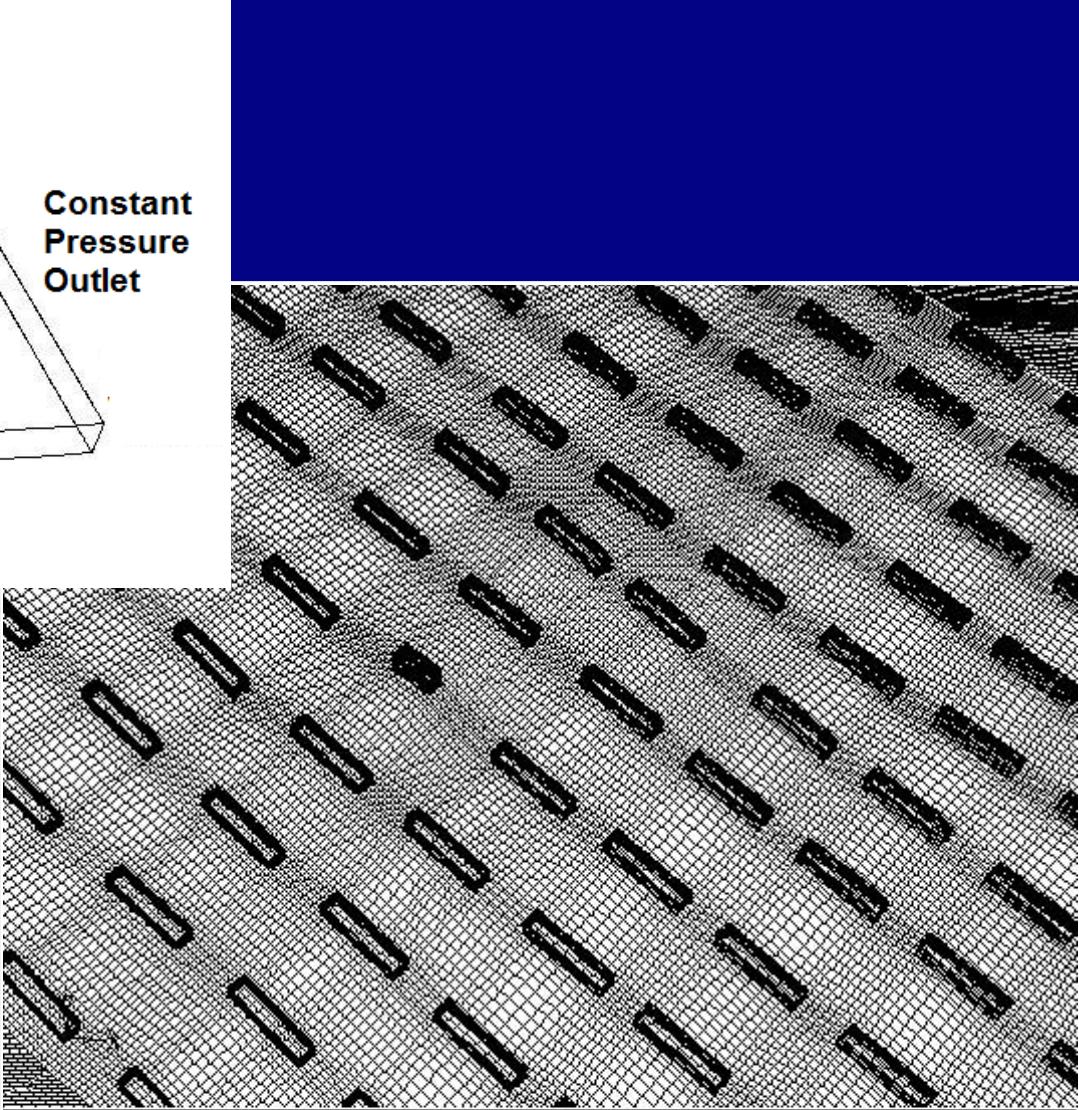
INTRODUCTION AND JUSIFICATION

- Reduce prediction uncertainties product of the different numerical parameter selection in the simulation of pollution dispersion.
- Improve the modeling capabilities of common practice modeling setup through the implementation and comparison of standard and advance scalar flux models.

COMPUTATIONAL DOMAIN, BC AND GRID



- Structured hexahedral grid
- 3.2 MM (fine), 1.6 MM (middle) and 0.8 MM (coarse) cells
- Min. wall cell size $1e-01$ m
- Expansion ratio $r \leq 1.3$



GOVERNING EQUATIONS

- RANS approach (Fluent V6.3)
- DSM (LRR-IP) and 2 Eq. turbulence model (Realizable k- ϵ)
- Pollutant Transport Equation

$$\frac{\partial}{\partial x_j} (\rho \bar{u}_j \bar{\phi}) - \frac{\partial}{\partial x_j} \left(\Gamma_\phi \frac{\partial \bar{\phi}}{\partial x_j} \right) = S_\phi - \frac{\partial}{\partial x_j} (\rho \bar{u}'_j \bar{\phi}') \quad \bar{u}' \bar{\theta}' = F \begin{pmatrix} \bar{u}' \bar{u}'_j, S_{i,j}, W_{i,j}, \bar{\phi}_{,j}, \rho, \\ \epsilon, \phi, g_i, \bar{\phi}^2, \frac{\partial P}{\partial x_j}, \frac{\partial \rho}{\partial x_j}, Ma \end{pmatrix}$$

- General Scalar Flux Models

$$-\bar{u}' \bar{\theta}' = \alpha_1 \frac{\partial \bar{\phi}}{\partial x_i} + \alpha_2 \bar{u}'_i \bar{u}'_j \frac{\partial \bar{\phi}}{\partial x_j} + \alpha_3 \bar{u}'_i \bar{u}'_k \bar{u}'_k \bar{u}'_j \frac{\partial \bar{\phi}}{\partial x_i}$$

	$\alpha 1$	$\alpha 2$	$\alpha 3$
SED	$\mu_t \cdot Sc_t^{-1}$	0	0
GGDH	0	0.3τ	0
ABE-SUGA	0	0	$0.45\tau k^{-1}$
ABE	0	0.22τ	$0.45\tau k^{-1}$

$$\tau = \text{Max} [k \epsilon^{-1}, 6 \cdot (\mu_L (\epsilon^* \rho)^{-1})^{1/2}];$$

MODEL EVALUATION METRICS

FRANKE ET. AL. (2007)

Factor of two FAC2
($\text{FAC2} > 0.5$)

$$\text{FAC2} = \text{fraction of data with } 0.5 \leq \frac{C_p^*}{C_o^*} \leq 2$$

Fractional Bias
($|\text{FB}| < 0.3$)

$$FB = \frac{\overline{C_o^*} - \overline{C_p^*}}{0.5(\overline{C_o^*} + \overline{C_p^*})}$$

Normalized Mean Square Error
($\text{NMSE} < 4$)

$$NMSE = \frac{\overline{(C_o^* - C_p^*)^2}}{\overline{C_o^*} \cdot \overline{C_p^*}}$$

Geometric Mean:
($0.7 < MG < 1.3$)

$$MG = \exp\left(\overline{\ln C_o^*} - \overline{\ln C_p^*}\right)$$

Geometric Variance VG
($VG < 1.6$)

$$VG = \exp\left[\overline{(\ln C_o^* - \ln C_p^*)^2}\right]$$

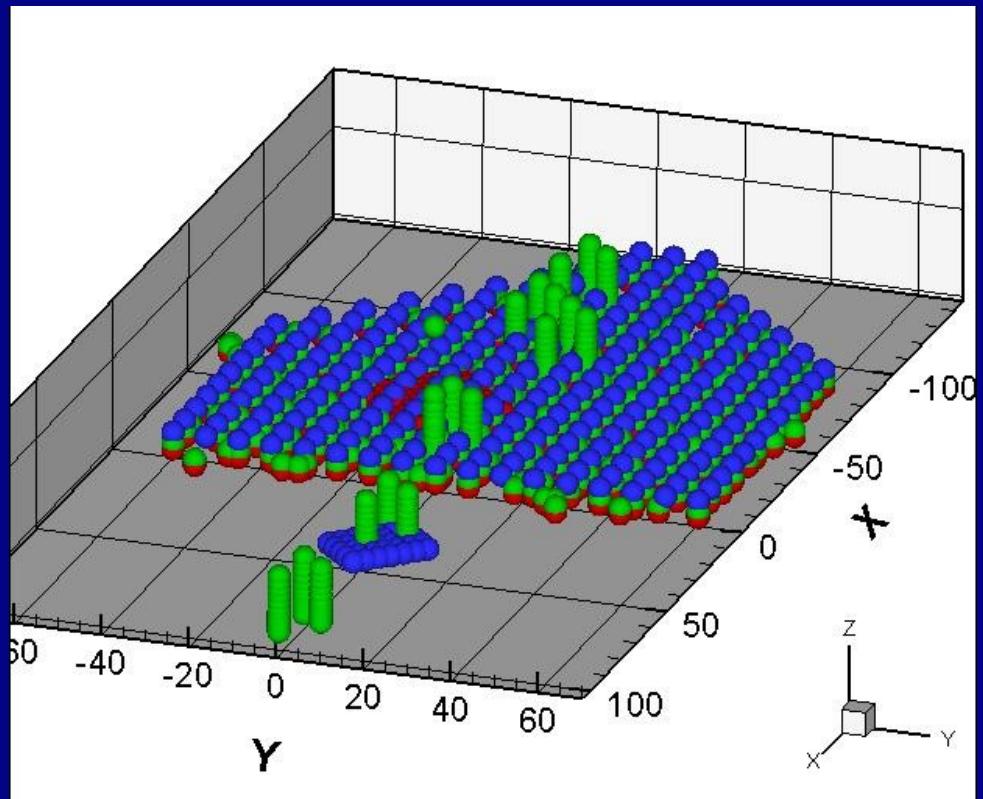
Hit Rate
($q \geq 0.66$)

$$q = \frac{1}{N} \sum_{n=1}^N i_n \quad , \quad i_n = \begin{cases} 1 & \text{if } |(O_n - P_n)/O_n| \leq D \text{ or } |O_n - P_n| \leq W \\ 0 & \text{otherwise} \end{cases}$$

RESULTS: VELOCITY FIELD

HIT RATE (q)

	LRR-IP	RKE
U	0.94	0.86
V	0.37	0.39
W	0.15	0.16
Urms	0.71	0.46
Vrms	0.64	0.58
Wrms	0.72	0.94
u'v'	0.20	0.41
u'w'	0.12	0.47
k(u'v')	0.48	0.20
k((u'w'))	0.41	0.31



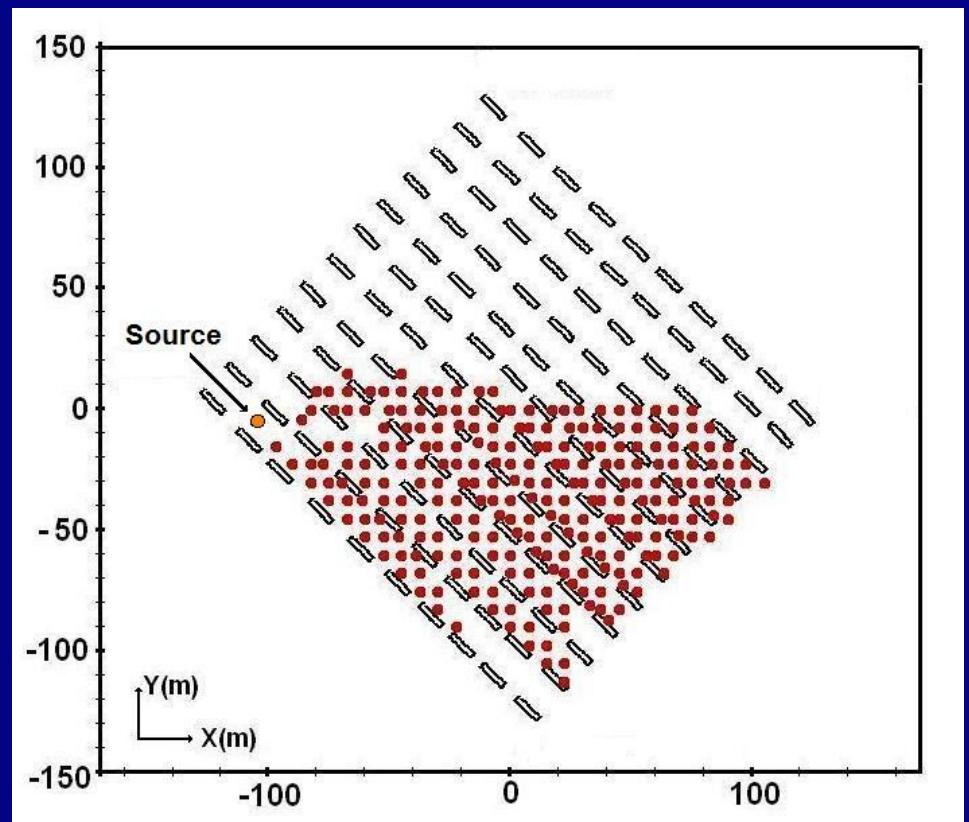
Flow Field Measurement Points

CONCENTRATIONS

Non-dimensional
concentration (C^*)

$$C^* = \frac{C_{mean} \cdot U_{ref} \cdot H^2}{Q_S}$$

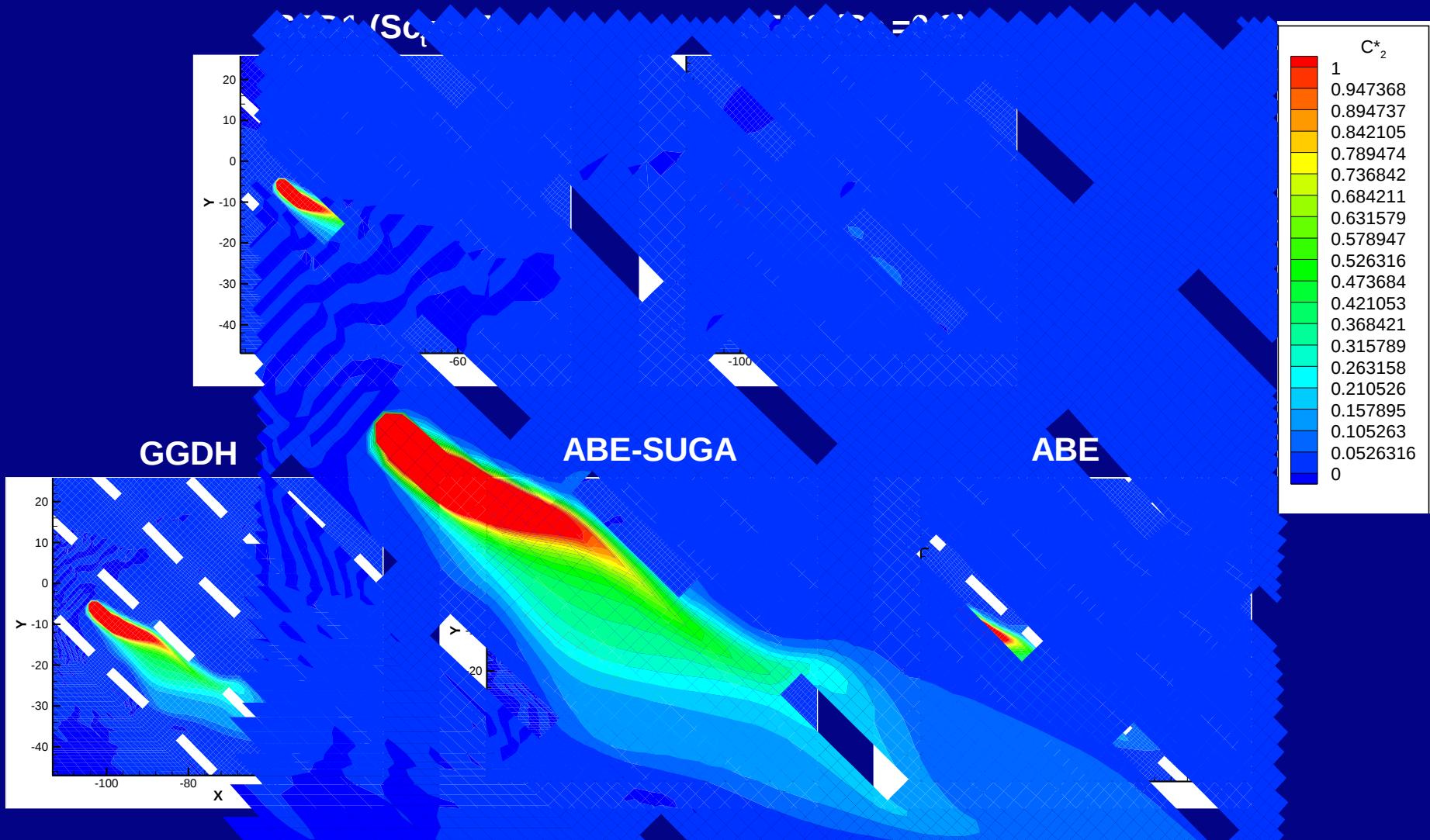
- C_{mean} (ppm)
- U_{ref} (m/s)
- H (m)
- Q_S (m^3/s)



Dispersion Measurement Points ($z=1.275\text{m}$)

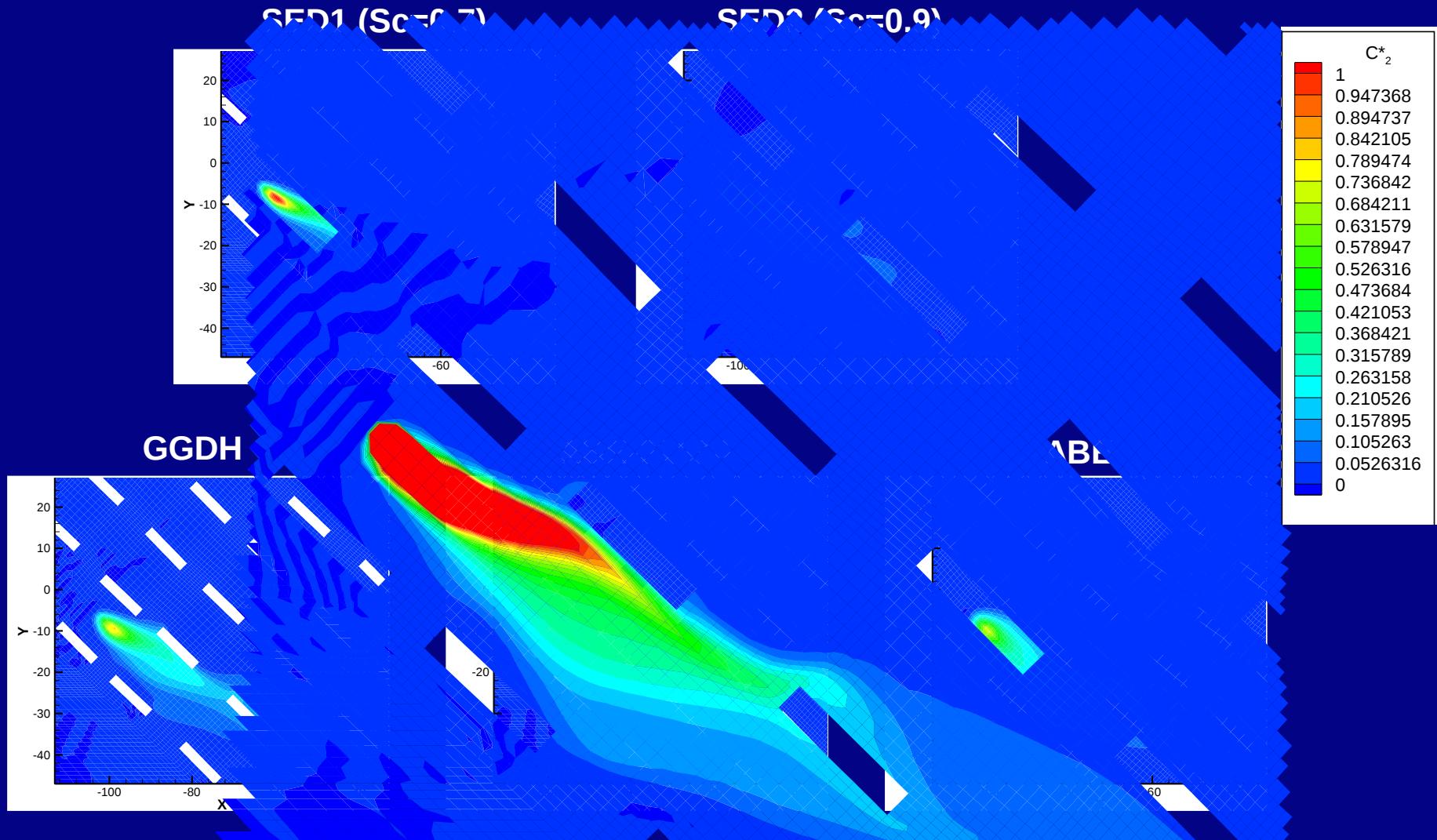
RESULTS: POLLUTION DISPERSION

PLANE Z=0.175m



RESULTS: POLLUTION DISPERSION

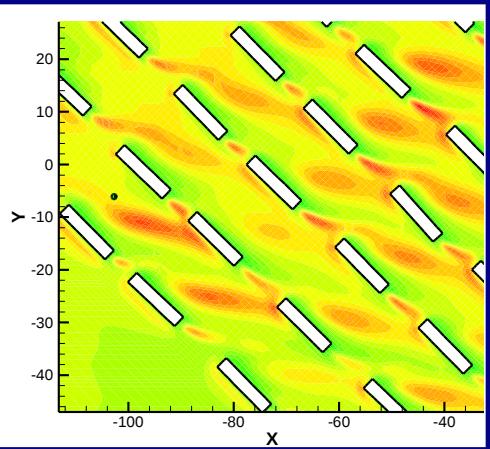
PLANE Z=1.275m



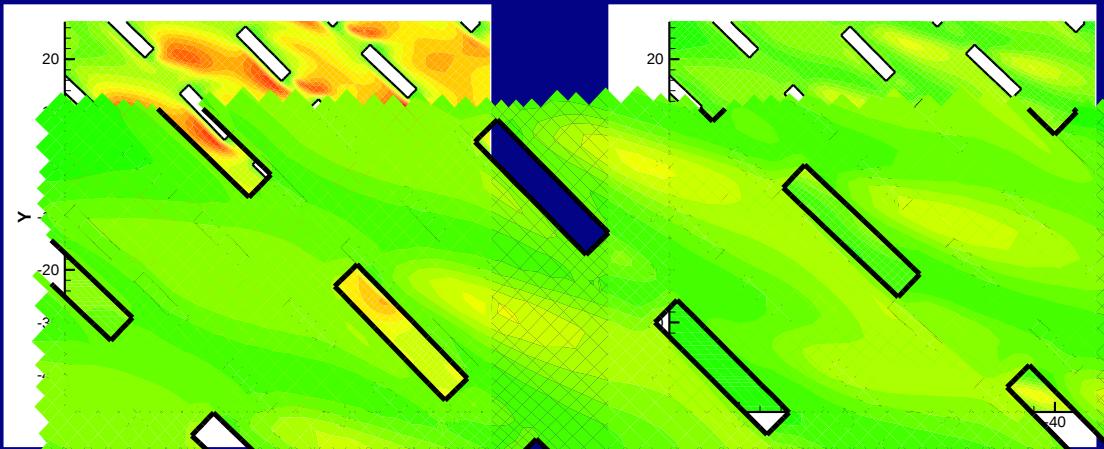
RESULTS: REYNOLDS STRESSES

PLANE Z=1.275m

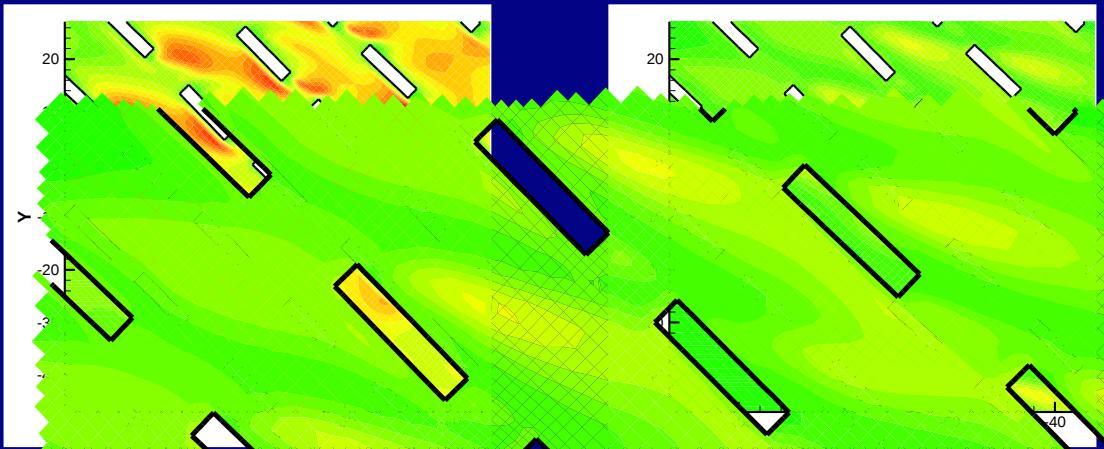
uu



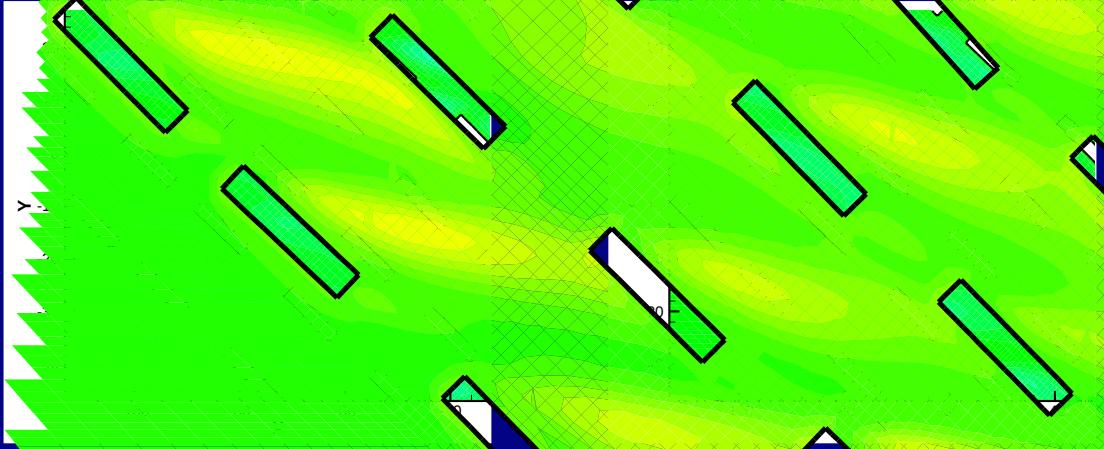
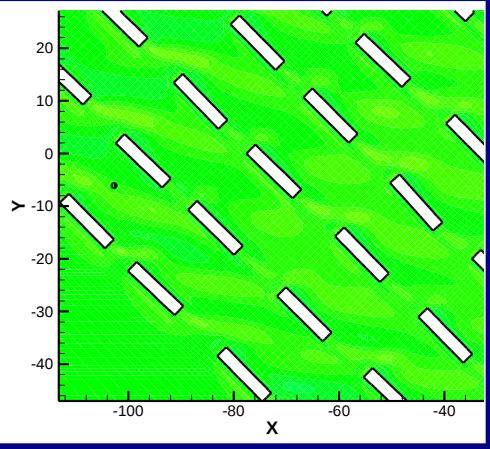
vv



ww



uv



RESULTS: CONCENTRATION METRICS

RECOMMENDED

RANGE:

(Chang & Hanna 2004)

|FB|<0.3

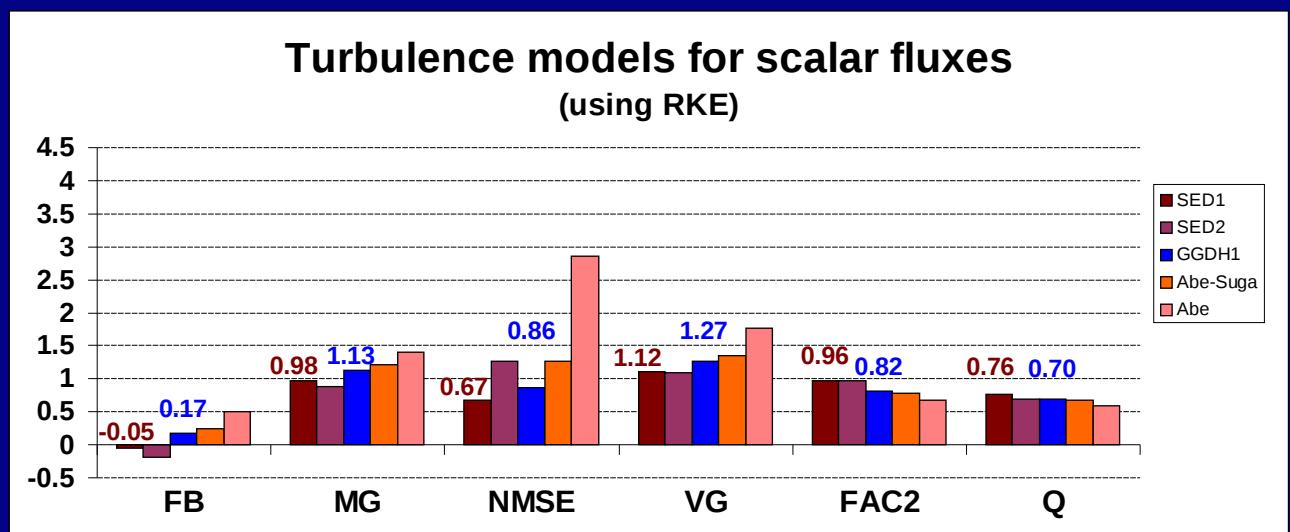
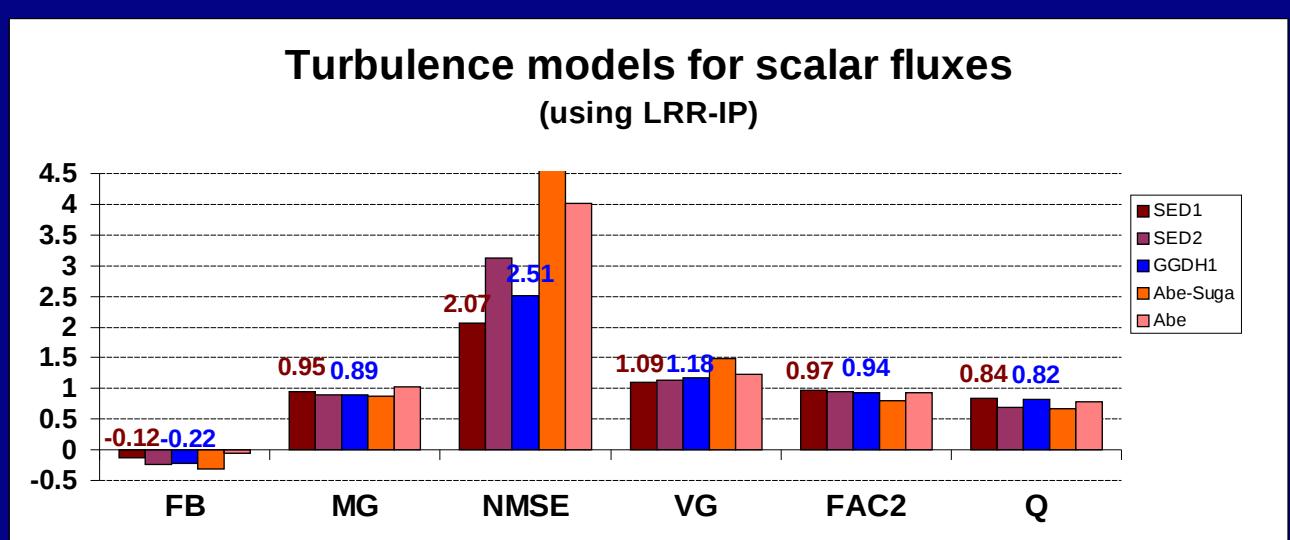
0.7 < MG < 1.3

NMSE < 4

VG < 1.6

FAC2>0.5

Q>0.66



Metrics Tolerance:

D=25%

W=0.003

CONCLUSIONS

- Statistical metrics are a useful tool to quantify the prediction capability of different scalar flux models for the evaluation of the MUST wind tunnel test experiment.
- As was expected, the dispersion predictions using SED model gives satisfactory results for most of the metrics for a given specific $Sc_t (=0.7)$. However, the performance is highly dependent of the selected Sc_t .
- It was found that the modeling of turbulent scalar fluxes by anisotropic models is highly related to the prediction accuracy of the Reynolds stresses.
- Better model does not mean always better metrics.

THANK YOU

FOR YOUR ATTENTION