# THREE-DIMENSIONAL STREET CANYONS

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#### Abstract

is project focused on the pollutant transport in idealized three-dimensional (3D) street myons using computational fluid dynamics (CFD). A series of sensitivity tests were rformed to examine the effects of building-width-to-street-width ratio (WR) on the flutant removal behaviours. The results reveal the pollutant dispersion characteristics in building configuration, and how WR affects the upward and sideward pollutant removal, sed on the current findings, it is suggested that the CFD results for idealized 2D street myons should be interpreted with caution.

Free Stream

Interface

 $U(z) = U_H (z/H)^{0.15}$ 

Fig 1 Computational domain

Upward

Interface

Non-Slip Wall

# Methodology

CFD code: OpenFOAM-1.6

# Turbulence Model:

Unsteady Reynolds-averaged Navier-Stokes Renormalization group k-ɛ turbulence model

### Parameters for the Street Canyon:

Building length in x direction: w (1m, 2m)

Building length in y direction: a (1m)

Building height: h (1m)

Street width in x direction: b (1m)

Building-width-to-street-width ratio (WR): w/b

Domain height: 8×h
Number of buildings in x direction: 8

Number of buildings in y direction: 5

Parameters for the Flows:

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Characteristic length: h (1m);

Characteristic velocity:  $U_H(0.15m/s)$ ;

Reynolds number:  $U_H \times h/\nu = 1.5 \times 10^4$ 

Number of grid points: about 10 million

# Parameters for the Pollutant Transport:

Pollutant concentration: c

Average pollutant concentration inside the canyon:  $\langle c \rangle$ 

Pollutant exchange rate through an interface of area A: PCH

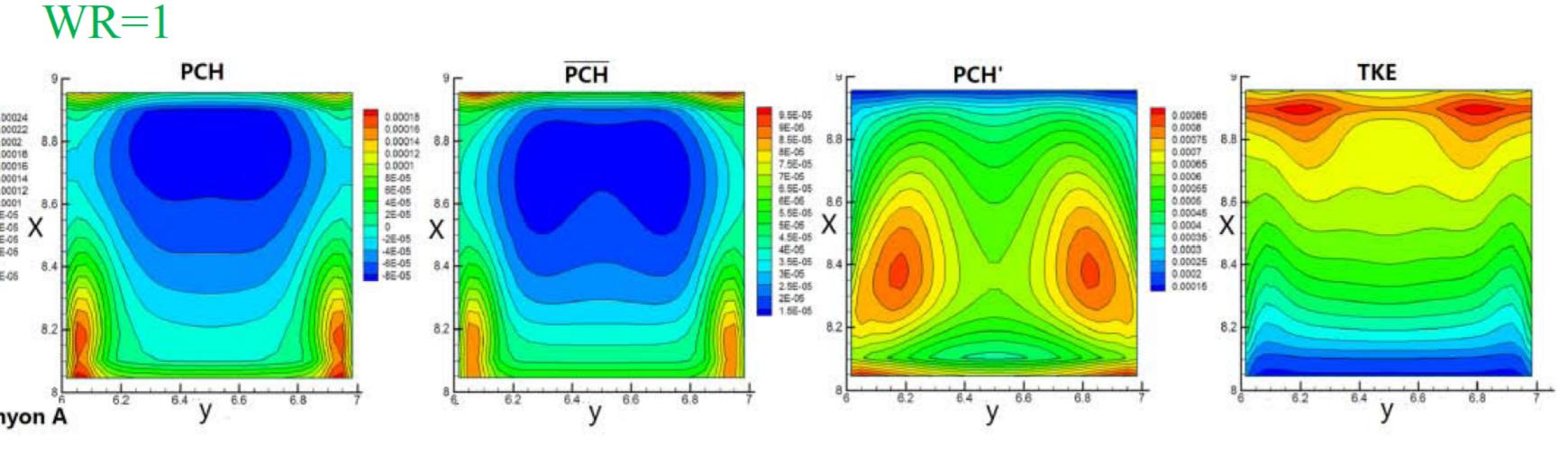
The total PCH is divided into two components:

$$\overline{PCH} = \int_{A} \overline{u_n} \overline{c} dA$$

PCH'=
$$-\int_A D_t \frac{\partial \bar{c}}{\partial n} dA$$

 $u_n$  is the velocity normal to the interface,  $D_t$  is the turbulent pollutant diffusivity. The mean part  $\overline{PCH}$  represents the pollutant transport by mean flow: The fluctuating part PCH' represents the pollutant transported by turbulence.

### Results and Discussions

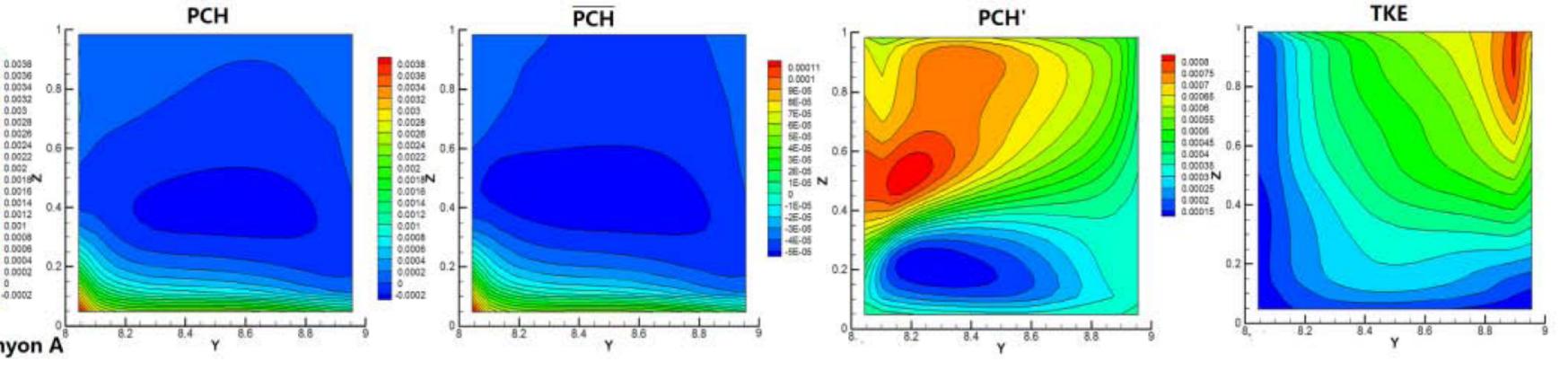


2 Contours on the upward interface of Canyon A of WR=1

The contours of PCH and PCH exhibit similar patterns, implying the dominance of PCH in the pollutant entrainment (most contours are negative).

On the other hand, PCH' is positive (upward transport) and large, dominating the pollutant removal from the street canyon.

PCH' is the correlation between the vertical velocity fluctuation and pollutant concentration. The peaks of PCH' and TKE locate differently, signifying the strong influence of pollutant concentration on PCH'.



3 Contours on the sideward interface of Canyon A of WR=1

The dominance of pollutant removal (positive contours) through the sideward interface near the ground level is a result of the street-level area pollutant source.

Though TKE is peaked at the windward roof level, pollutant accumulates near the leeward building leading to the elevated PCH'.

13th International Conference on Harmonisation within Atmospheric Dispersion Modelling for Regulatory Purposes

Paris, France, 1- 4 June 2010

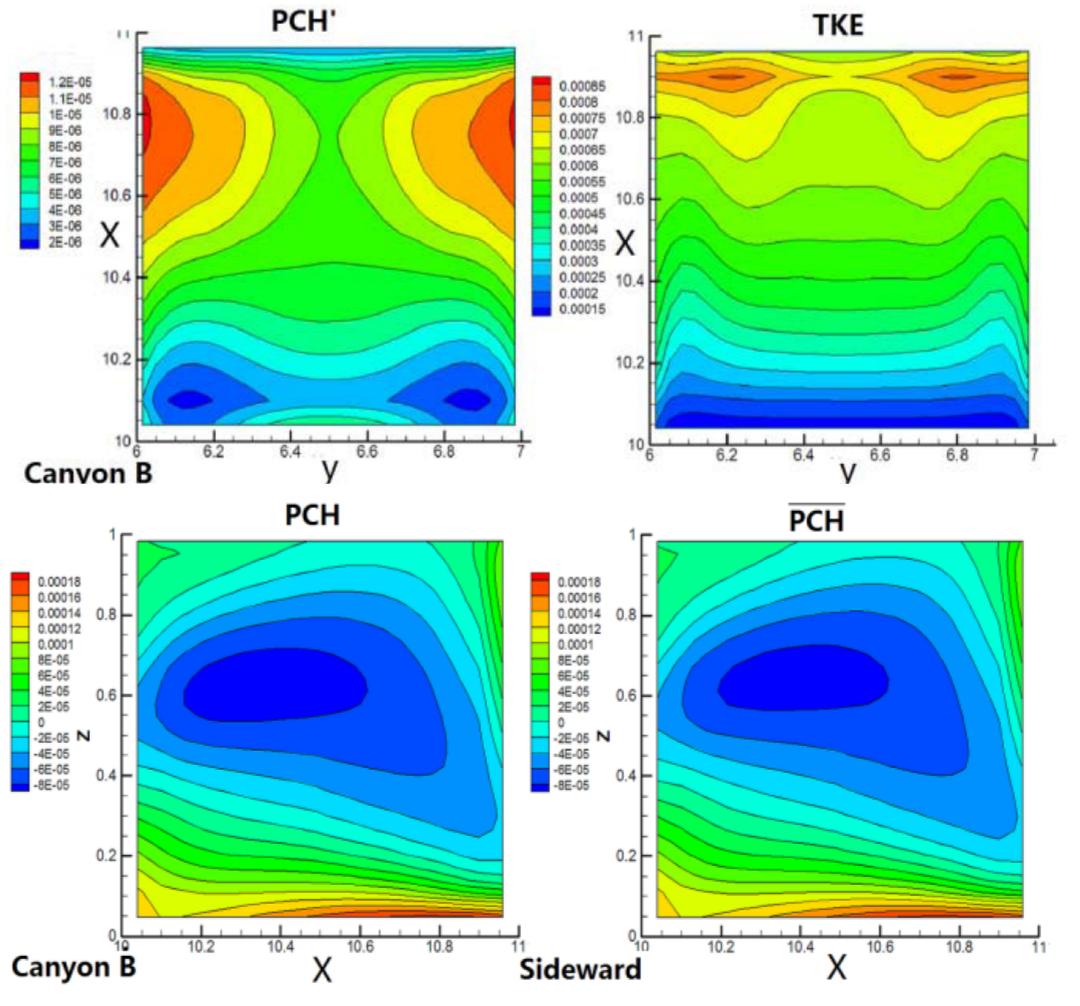


Fig 4 Contours on the upward interface of Canyon B of WR=1

The peaks of PCH' and TKE locate closely to each other on the sideward interface, signifying the stronger influence of turbulence of PCH'.

Fig 5 Contours on the sideward interface of Canyon B of WR=1

The pollutant from Canyon A is carried to the sideward interfaces of Canyon B. It enters into Canyon I following the mean flow (negative contours), recirculation inside the

street canyon and is finally removed from Canyon B through the upward interface b turbulence (positive contours in Fig 4).

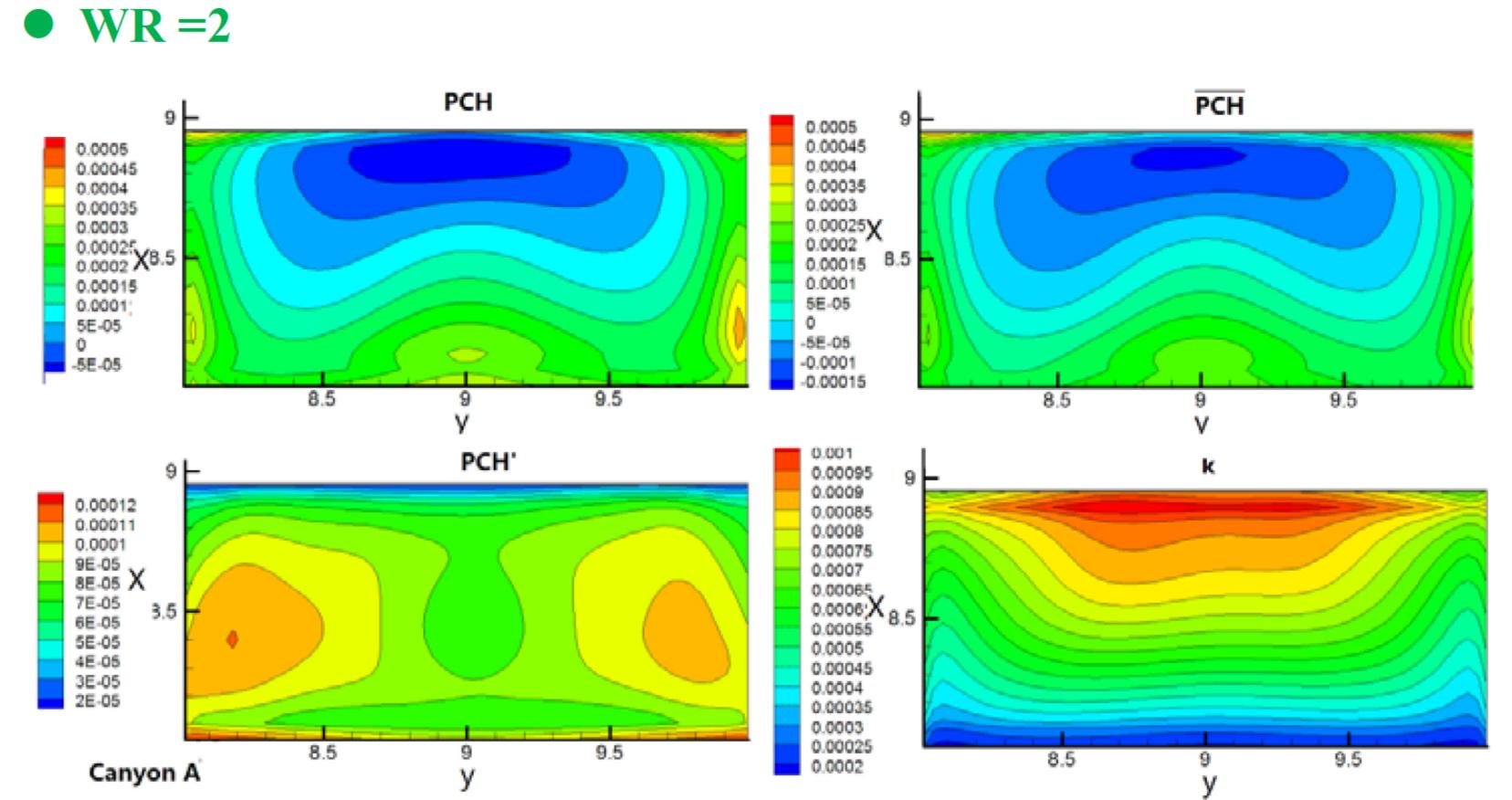


Fig 6 Contours on the upward interface of Canyon A of WR=2

- 1. Unlike WR = 1, the average  $\overline{PCH}$  on the upward interface is positive, demonstrating th importance of mean flow in pollutant removal from a wider street canyon.
- 2. Similar to WR = 1, the pollutant removal on the upward interface by PCH' (positive contours) peak near the sides of the street canyon which is likely the result of the recirculating flow inside the street canyon.

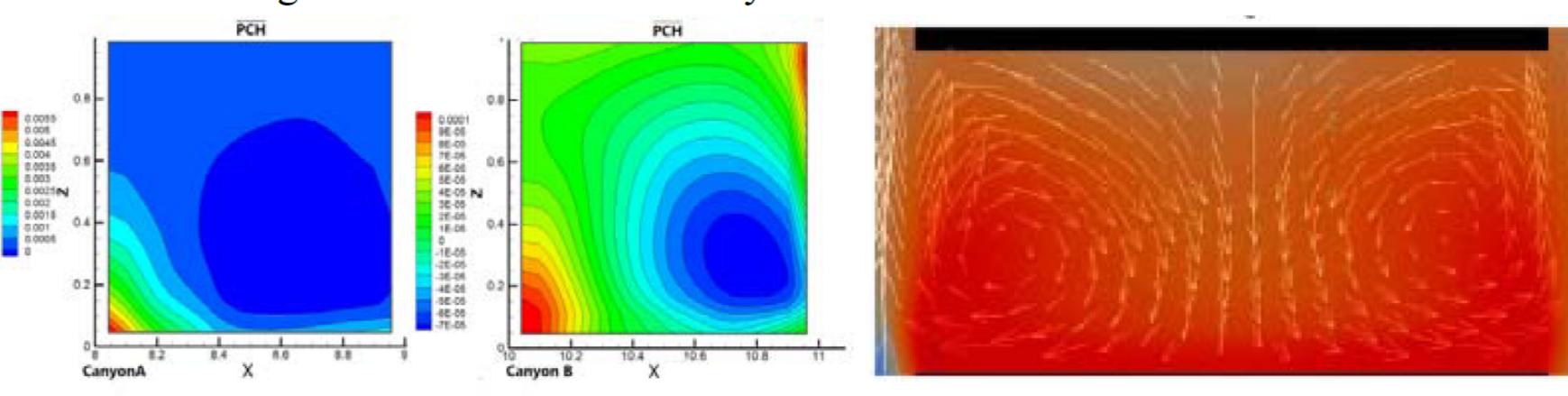


Fig7 Contours on the sideward interface of Canyon A&B of WR=2 Fig8 Vector profile sampled in h=0.5 for WR=2

Compare Fig 3, 5, 7, the pollutant removal in WR = 1 is distributed evenly at the groun level while in WR = 2 is shifted toward the leeward ground level. These dissimilar pollutar transport behaviours are caused by the recirculation of different nature (Fig 8).

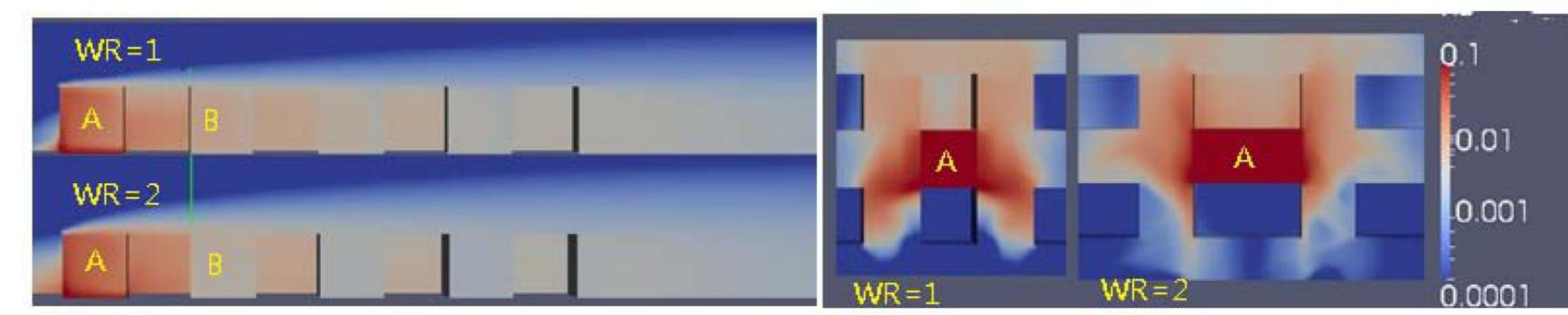


Fig 9 Pollutant concentration contours

In fact the pollutant could be transported opposite to the free-stream flow that goes intupstream along the street below the roof level. This re-entrainment mainly takes place through the sideward interfaces that is less significant in street canyons of larger WRs.

### **Conclusions**

- Generally, pollutant entrainment is dominated by mean flow while pollutant removal is dominated by turbulence.
- When WR is increased from 1 to 2, the wider canyon enhances the performance of PCI while PCH' remains the same pattern. Hence, PCH is improved.
- 3. In the roof level of Canyon A, the contribution of PCH' is mainly attributed to the peaks near the sideward interfaces. When the street is widened, these peaks affect less within a smaller region, the overall PCH' performance is weakened.
- 4. Pollutant could be carried into the upstream canyons which is a process governed by th sideward pollutant removal and entrainment



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