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# The role of thermal convection in the dispersion of traffic-induced air pollutants in the urban environment



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# Model essentials



## Periodic geometry

- Periodic BCs at all lateral boundaries (x and y)
- Small domain: high resolution + high speed
- The max. size of flow structures is restricted



## Atmospheric wind

- Large-scale eddies: sudden changes in wind direction and magnitude
- Control term to include the effect of macroscale fluctuations in the small simulation domain



## Solar radiation and natural convection

- Bulk Richardson number:

$$Ri_b = \frac{gL\beta(T_{wall} - T_0)}{U_{ref}^2}$$

- Control term to eliminate artificial heating



## Traffic-related air pollution

- Multiple, time-dependent emissions
- Not periodic: pollutants can be dispersed beyond the physical boundaries of the domain

Turbulent scales can be divided into...

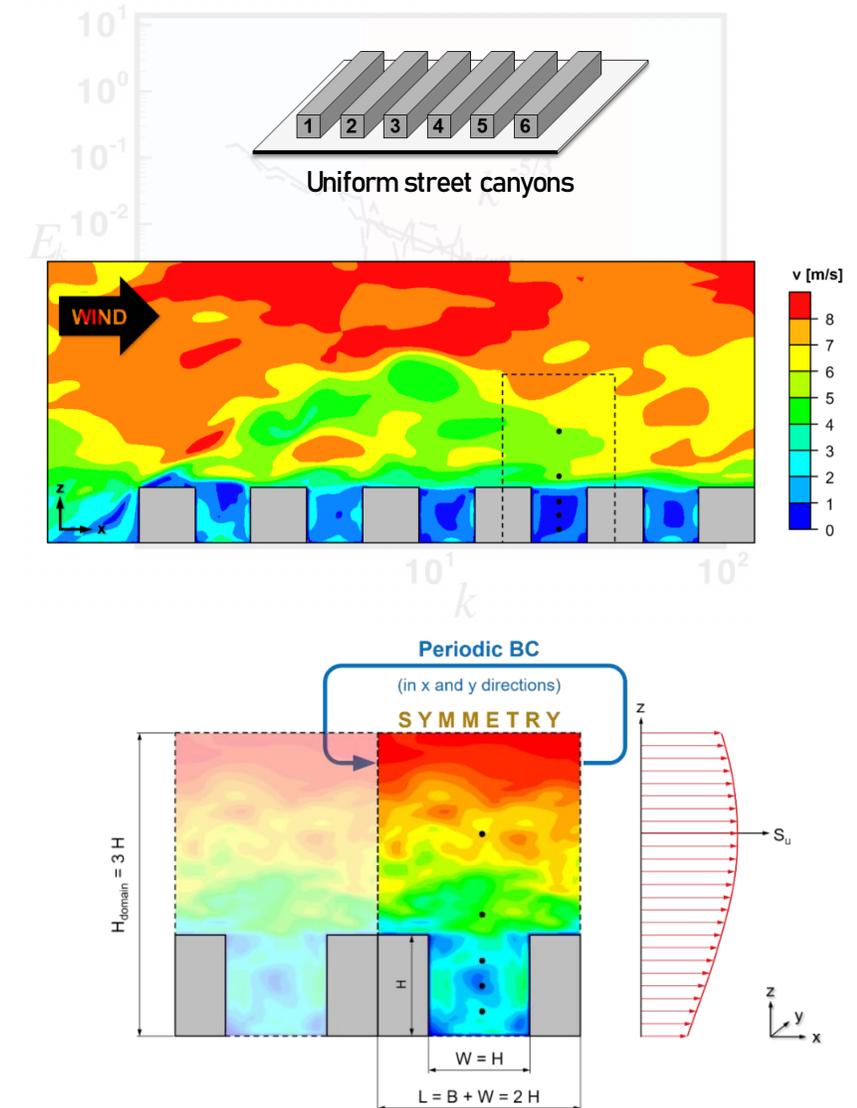
- **Macroscopic turbulence:**
  - Flow structures larger than the domain size
  - Rapid changes in wind direction and magnitude
  - Imposing measured  $u(t)$  and  $v(t)$  time series at the reference location within the periodic domain

- Transient Wind Forcing method: volume source of momentum

$$S_u(z, t) = \rho \cdot a(t) \cdot G(z) = \rho \cdot \frac{u_{meas}(t) - u_{CFD}(t)}{\tau(t)} \cdot e^{-\frac{1}{2} \left( \frac{z - z_{ref}}{L_0} \right)^2}$$

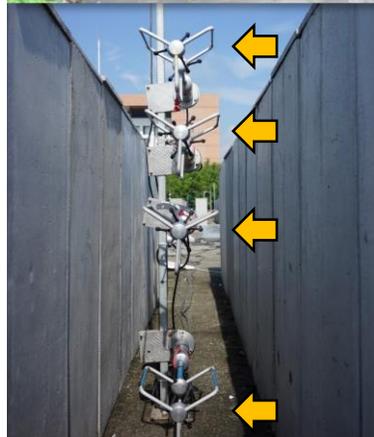
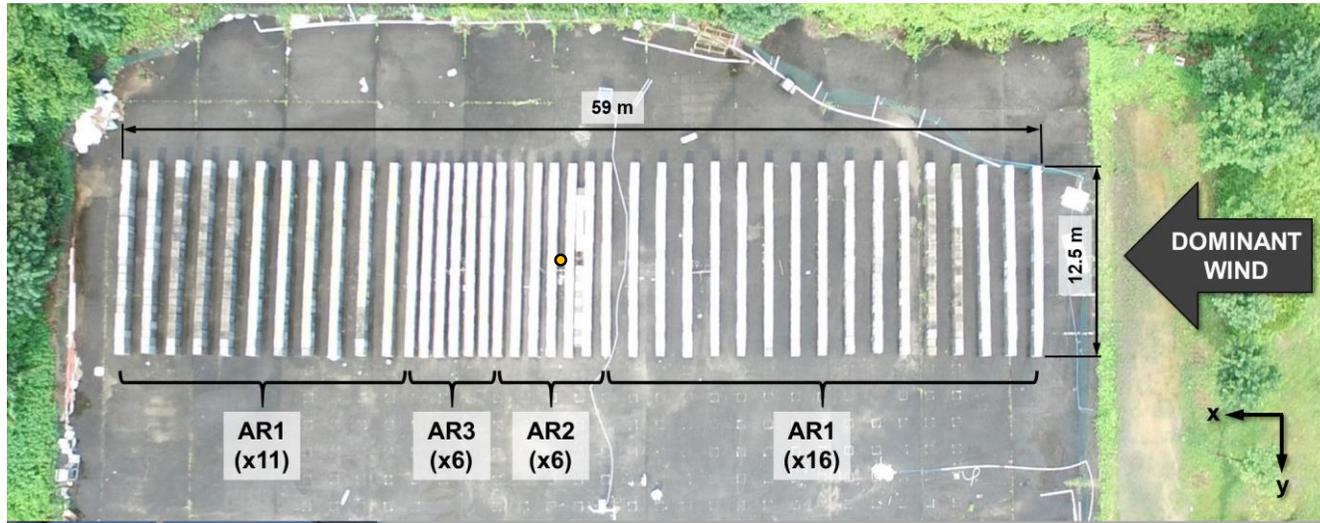
- Proportional control (flow-through time): minimizing the difference between measurement and simulation data

- **Mesosopic turbulence: unsteady velocity field (LES)**
- **Microscopic (unresolved) turbulence: captured by the sub-grid-scale stress (SGS) model**
  - Smagorinsky-Lilly model ( $C_s = 0.1$ )

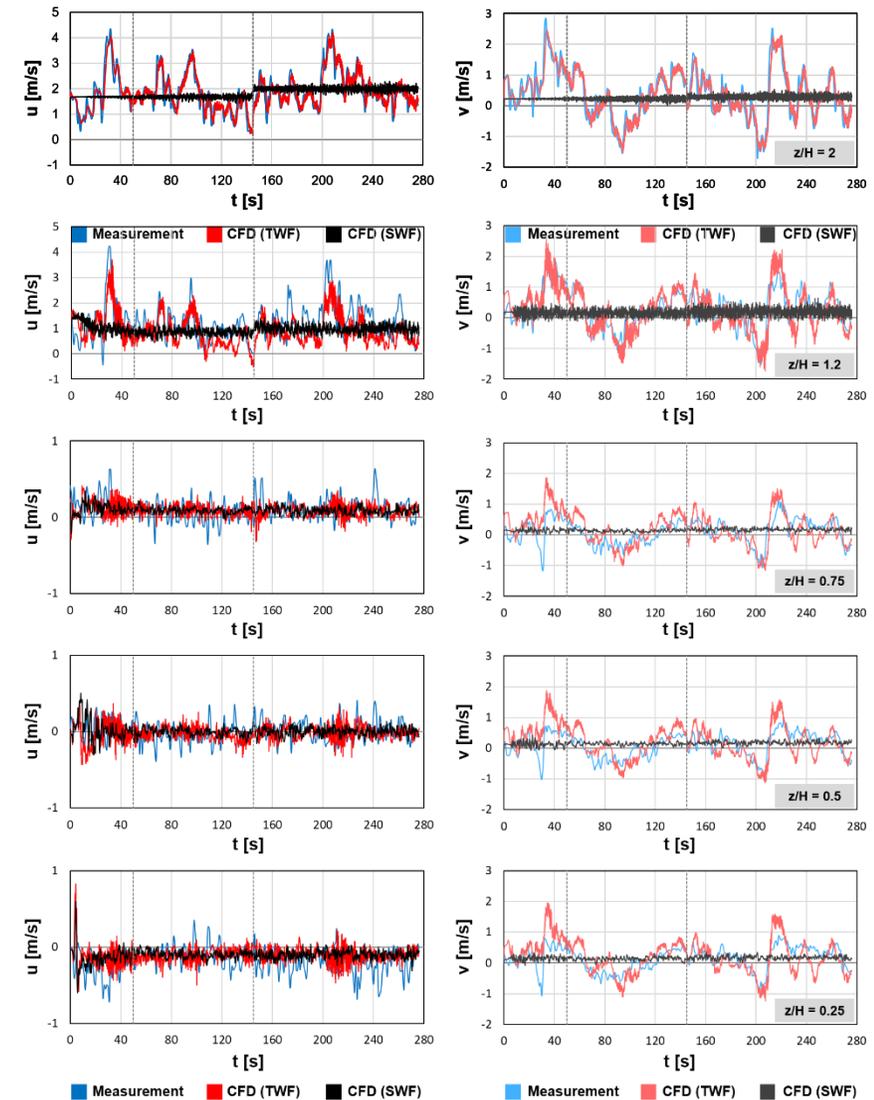


# Validation of the TWF model

Field measurements:  $u(t)$  and  $v(t)$  time series at  $z = 2H = 2.4$  m, over the street canyons (SYSU, China) → CFD model



- Comparison at 4 further gauging points below the reference location
  - Time average
  - Fluctuations
- The 3D turbulent flow field is reproduced with sufficient accuracy



# Temperature control

- Lower region of the atmospheric boundary layer

- Strong turbulent mixing
- Equilibrium of the sensible heat fluxes:

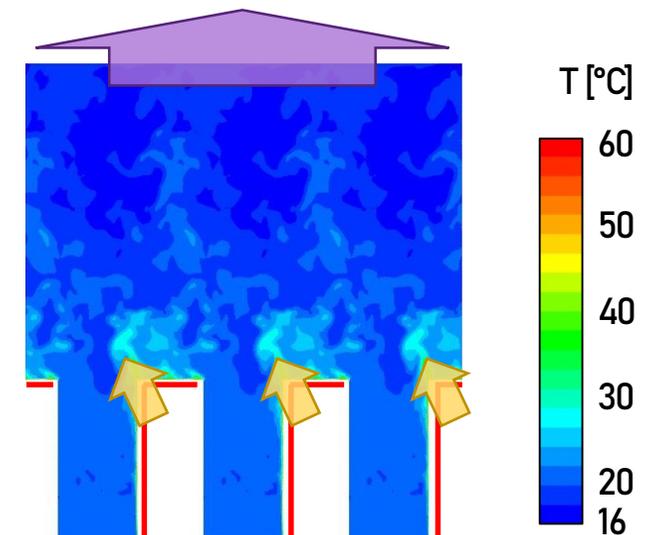
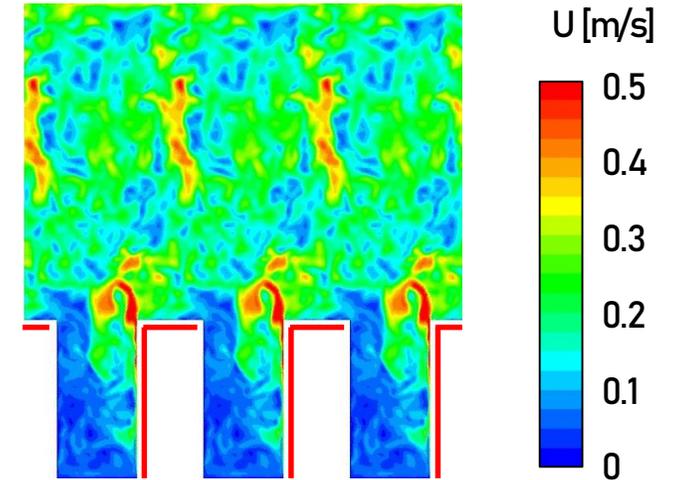
$$Q_{wall} = Q_{upper}$$

- Constant **average/bulk temperature**

- The heat introduced by the hot walls must be consumed by sinks

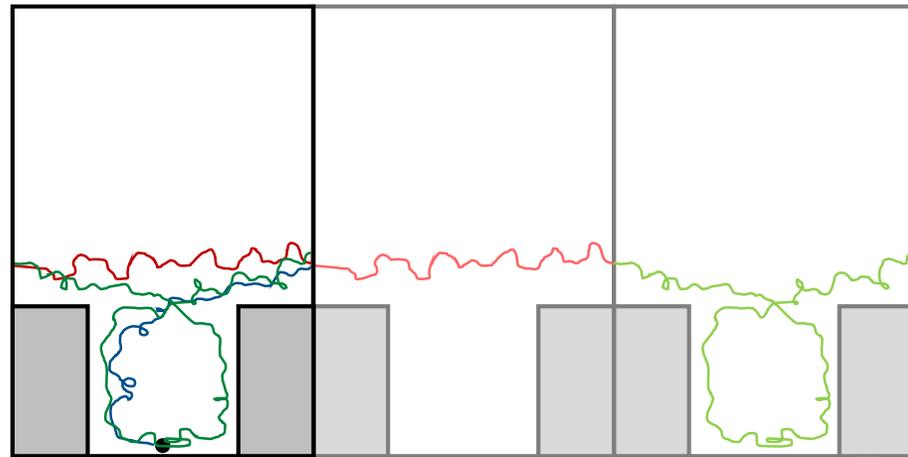
$$S_T(\vec{x}, t) = -\rho_0 c_v \cdot \frac{T_{avg}(t) - T_0}{\Delta x} \cdot [\vec{v}(\vec{x}, t) \cdot \vec{d}_0]$$

- Patankar et al. (1977): streamwise periodic, steady-state model for heat exchangers → extension to 2-way periodicity (XY)
  - **Wind direction:** time average or instantaneous
- The vertical temperature distribution is not modified, only shifted
    - Initial (reference) temperature:  $T_0 = 20 \text{ [}^\circ\text{C]} > T_{min}$



PATANKAR, S. V., LIU, C. H., & SPARROW, E. M. (1977). FULLY DEVELOPED FLOW AND HEAT TRANSFER IN DUCTS HAVING STREAMWISE-PERIODIC VARIATIONS OF CROSS-SECTIONAL AREA. JOURNAL OF HEAT TRANSFER, 99 (2)

Lagrangian particle tracking + counting the periodic jumps = far-field dispersion

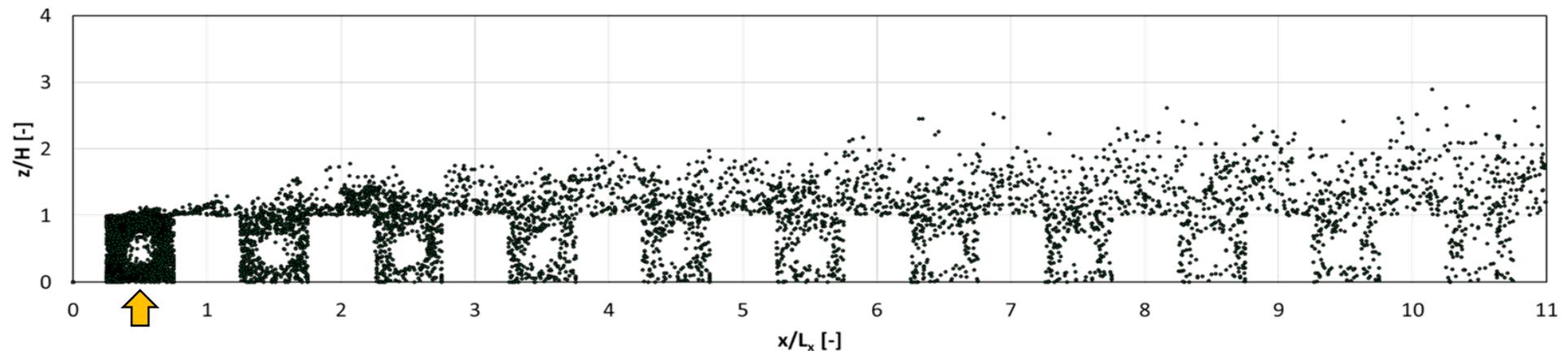


$X_{\text{jump}} = 0$

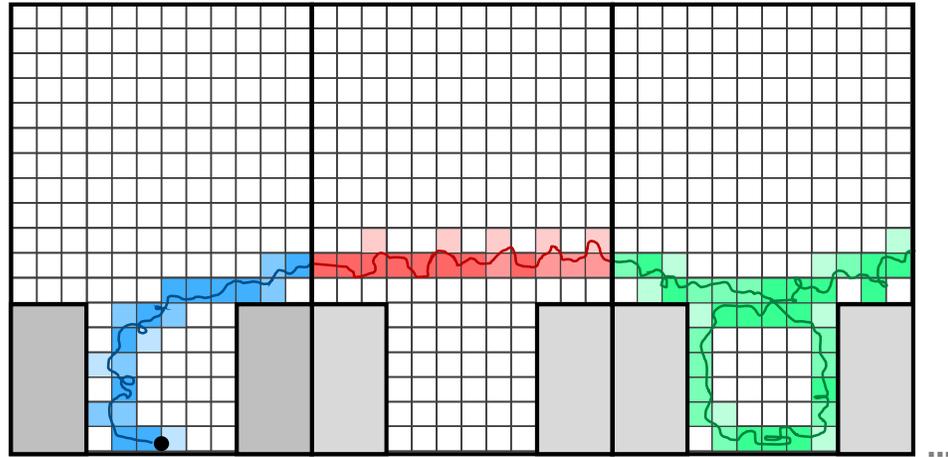
$X_{\text{jump}} = 1$

$X_{\text{jump}} = 2$

Instantaneous particle plume, emitted continuously from a single point source:



Dose field – recording the particles' footprints:

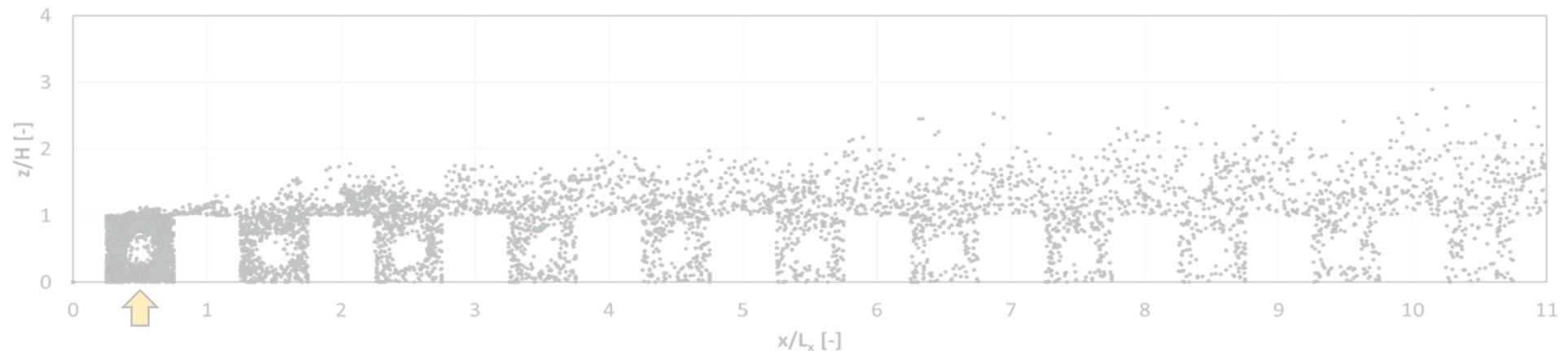


- User Defined Memory fields (ANSYS Fluent)
- Incrementing the cell values by  $\Delta t_{particle}/V_{cell}$

➤ Dose:  $d = \int c dt$

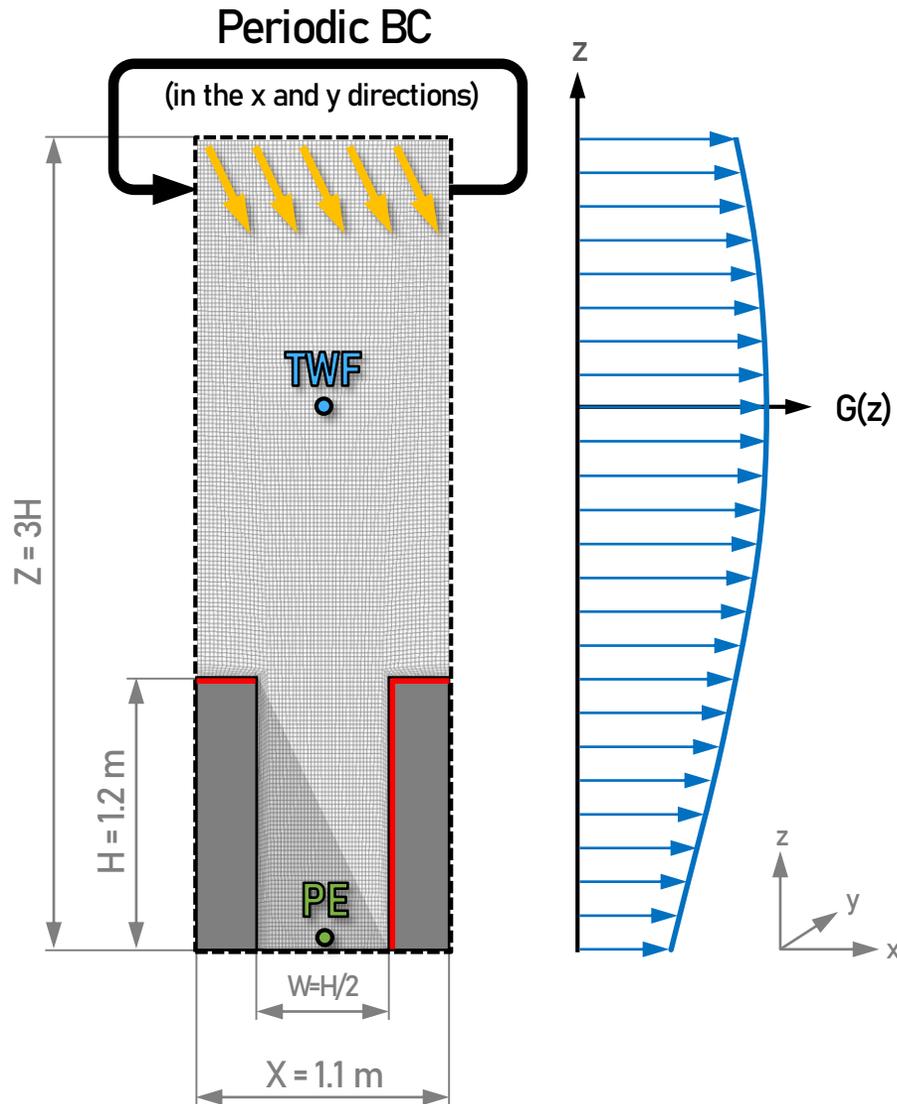
- The dispersion results are validated with data from wind tunnel measurements

Instantaneous particle plume, emitted continuously from a single point source:

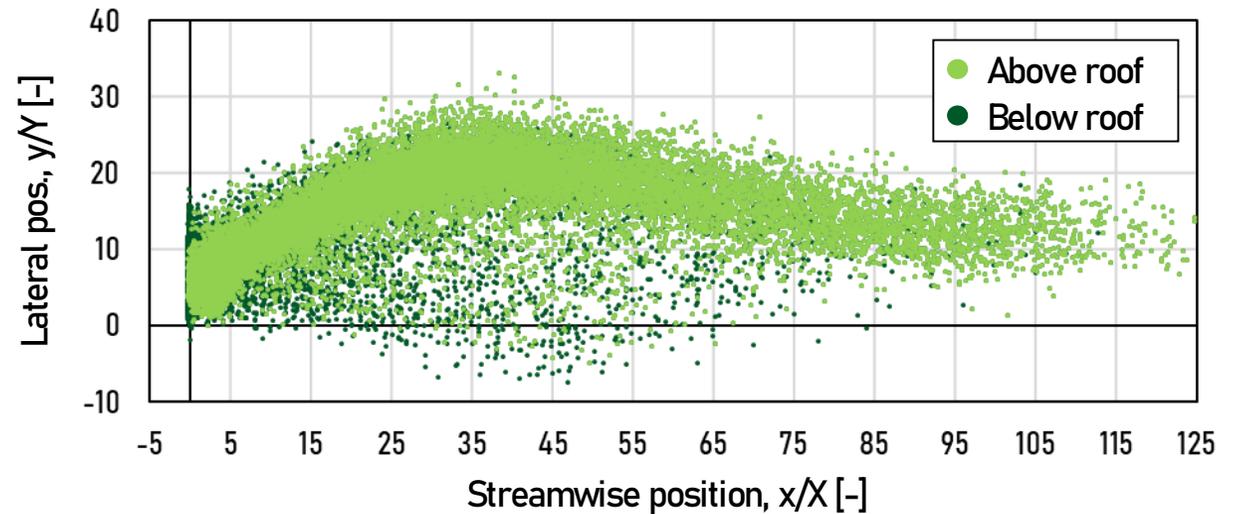




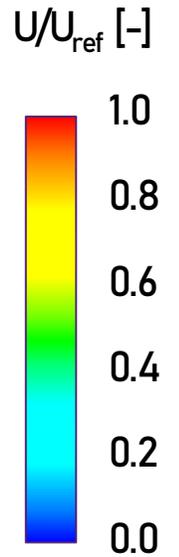
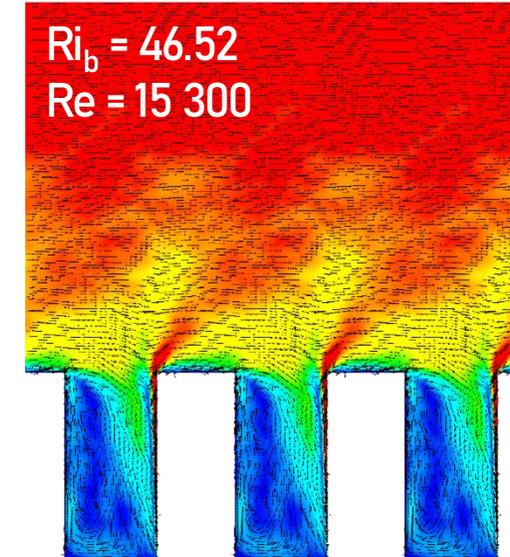
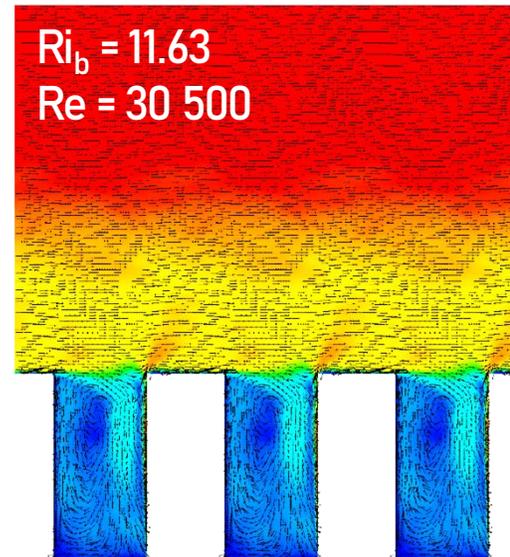
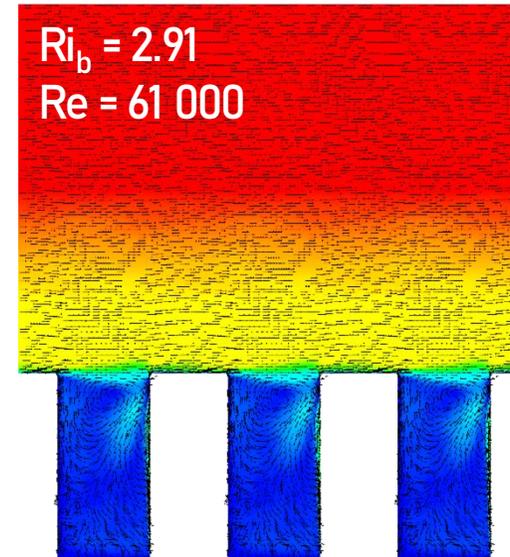
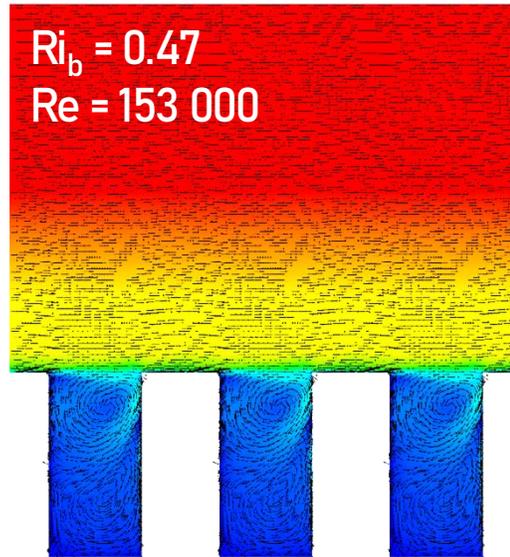
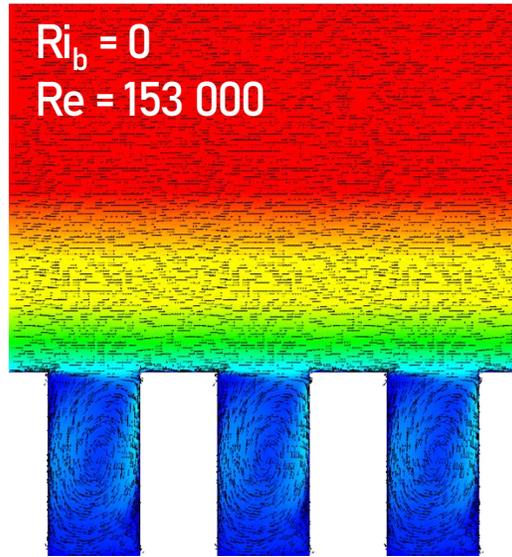
# Model overview (present study)



- Infinite series of parallel  $H/W = 2$  street canyons
- Mesh resolution:  $W/32$  + near-wall inflation
- TWF: measured time series (277 s) are imposed
- Particle emission: 50...150 s
- Solar radiation: roofs & downwind walls are heated (less favorable)



# The effect of the bulk Richardson number



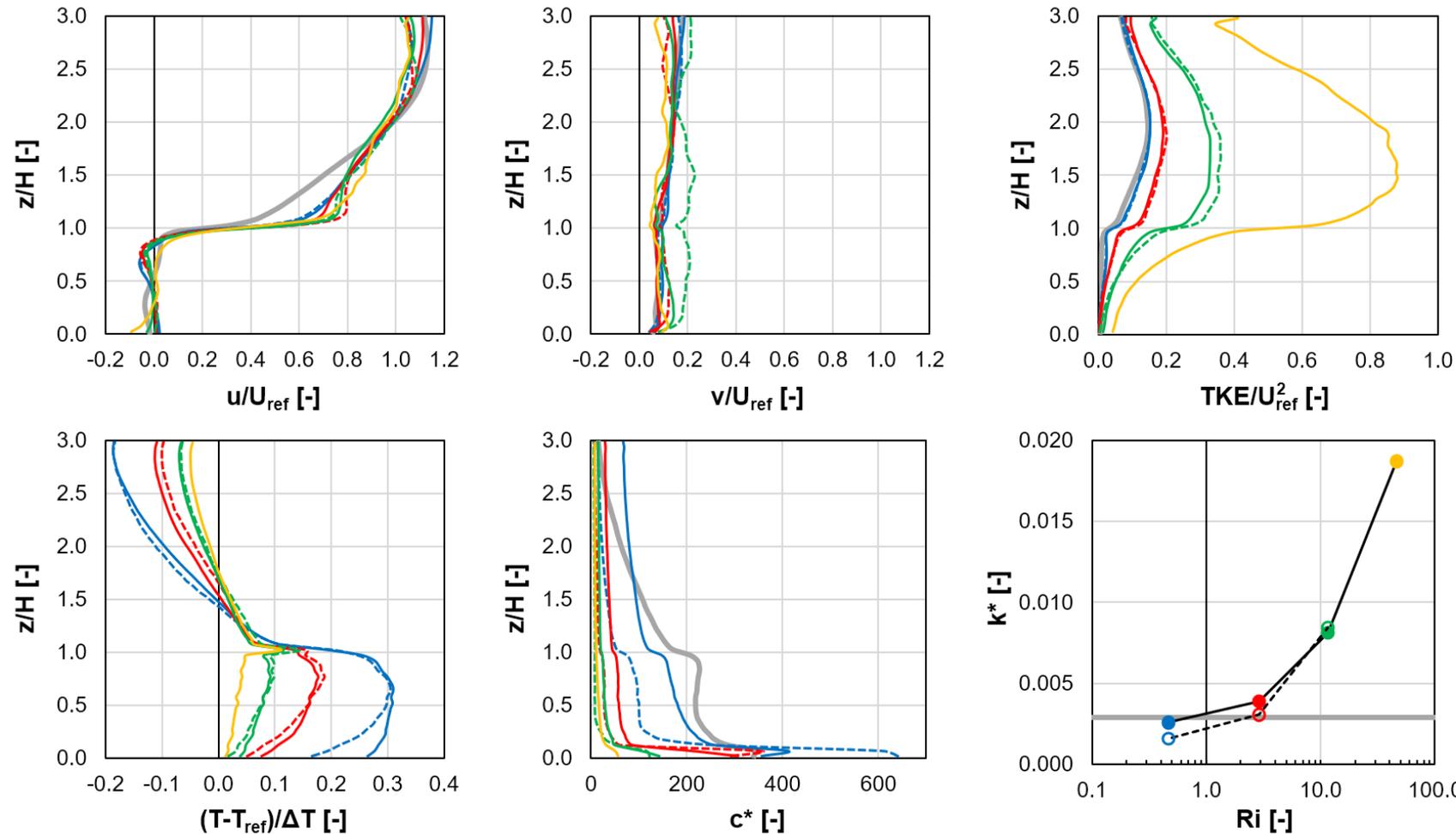
$U_{ref} = 0.187 \dots 1.87$  [m/s]  
 $\Delta T = 0$  &  $40$  [°C]

$(g > 0)$

$$Ri_b = \frac{gL\beta(T_{wall} - T_0)}{U_{ref}^2}$$

$$Re = \frac{LU_{ref}}{\nu}$$

# Characteristic vertical profiles



— Ri = 0 ( $\Delta T = 0^\circ\text{C}$ ,  $U_{ref}$ )      — Ri = 0.47 ( $\Delta T = 40^\circ\text{C}$ ,  $U_{ref}$ )      — Ri = 2.91 ( $\Delta T = 40^\circ\text{C}$ ,  $0.4U_{ref}$ )      — Ri = 11.63 ( $\Delta T = 40^\circ\text{C}$ ,  $0.2U_{ref}$ )  
 — Ri = 46.52 ( $\Delta T = 40^\circ\text{C}$ ,  $0.1U_{ref}$ )      - - Ri = 0.47 ( $\Delta T = 10^\circ\text{C}$ ,  $0.5U_{ref}$ )      - - Ri = 2.91 ( $\Delta T = 10^\circ\text{C}$ ,  $0.2U_{ref}$ )      - - Ri = 11.63 ( $\Delta T = 10^\circ\text{C}$ ,  $0.1U_{ref}$ )

Normalized concentration:

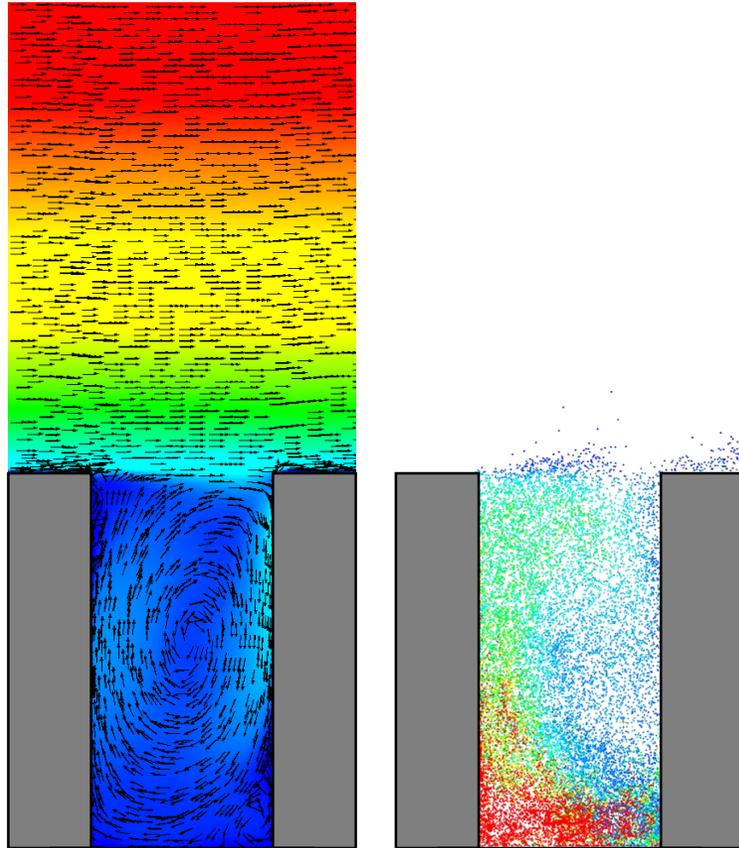
$$c^* = \frac{dU_{ref}A}{t_s/\Delta t} = \frac{dU_{ref}A}{N_p}$$

Ventilation efficiency:

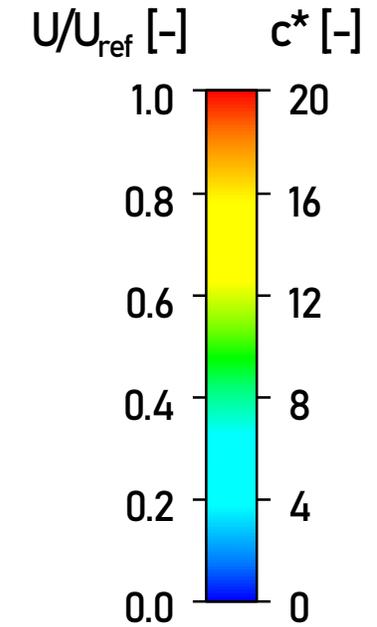
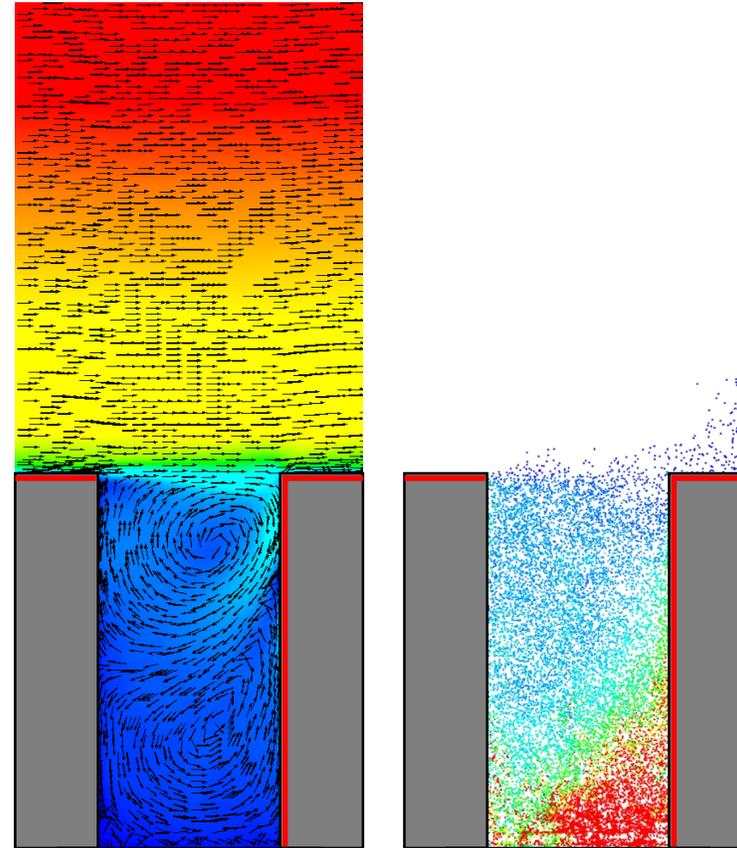
$$k^* = \frac{1}{c_{ng}^*}$$

# The effect of heated walls

Ri = 0 ( $\Delta T = 0^\circ\text{C}$ ,  $U_{\text{ref}}$ ), Re = 153 000



Ri = 0.47 ( $\Delta T = 40^\circ\text{C}$ ,  $U_{\text{ref}}$ ), Re = 153 000



$$c^* = \frac{dU_{\text{ref}}A}{t_s/\Delta t} = \frac{dU_{\text{ref}}A}{N_p}$$

XIE, X., HUANG, Z., WANG, J., & XIE, Z. (2005). THE IMPACT OF SOLAR RADIATION AND STREET LAYOUT ON POLLUTANT DISPERSION IN STREET CANYON. BUILDING AND ENVIRONMENT, 40(2), 201-212.

# Contributions & proposal for collaboration

- Periodic, measurement-driven LES model
  - Relatively small simulation domain
- The effects of natural wind can be taken into account
  - Transient Wind Forcing (TWF): imposing measured time series
  - The effects of flow structures exceeding the domain size can be modeled
- Long-distance dispersion can be calculated
  - Lagrangian particle tracking + counting the periodic jumps
  - Periodic flow field → aperiodic dispersion field
- Buoyancy and natural convection can also be modeled
- Validated for the isothermal cases (both velocity and dispersion)



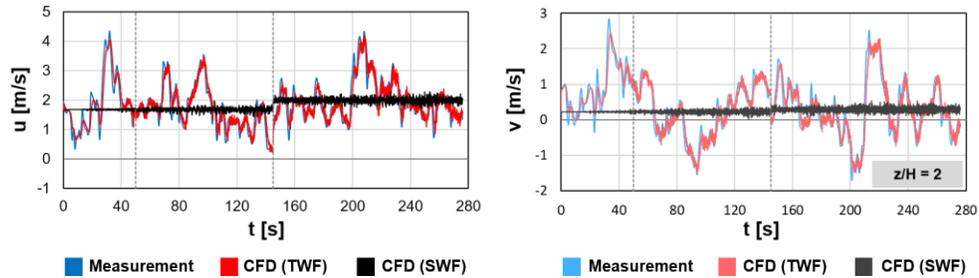
- For the validation of the thermal model, we need measurement data from new collaborators:
  - Field or wind tunnel experiments
  - Periodic or quasi-periodic geometry containing heated elements
  - High-frequency velocity time series for the TWF propulsion (full-scale: 1 Hz, covering 500...1000 flow-through times)
  - Time series from further gauging points for comparison of the velocity statistics and temperature results
  - The measurements may include concentration distributions as well

# Supplementary slides

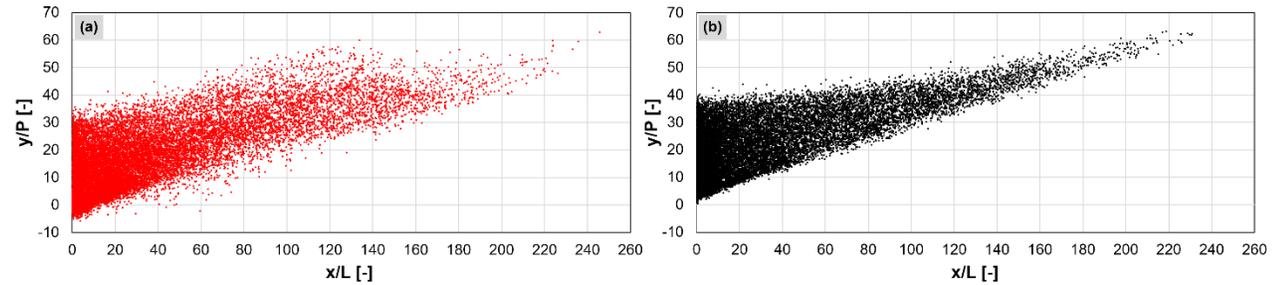


# How much do the macroscopic fluctuations matter?

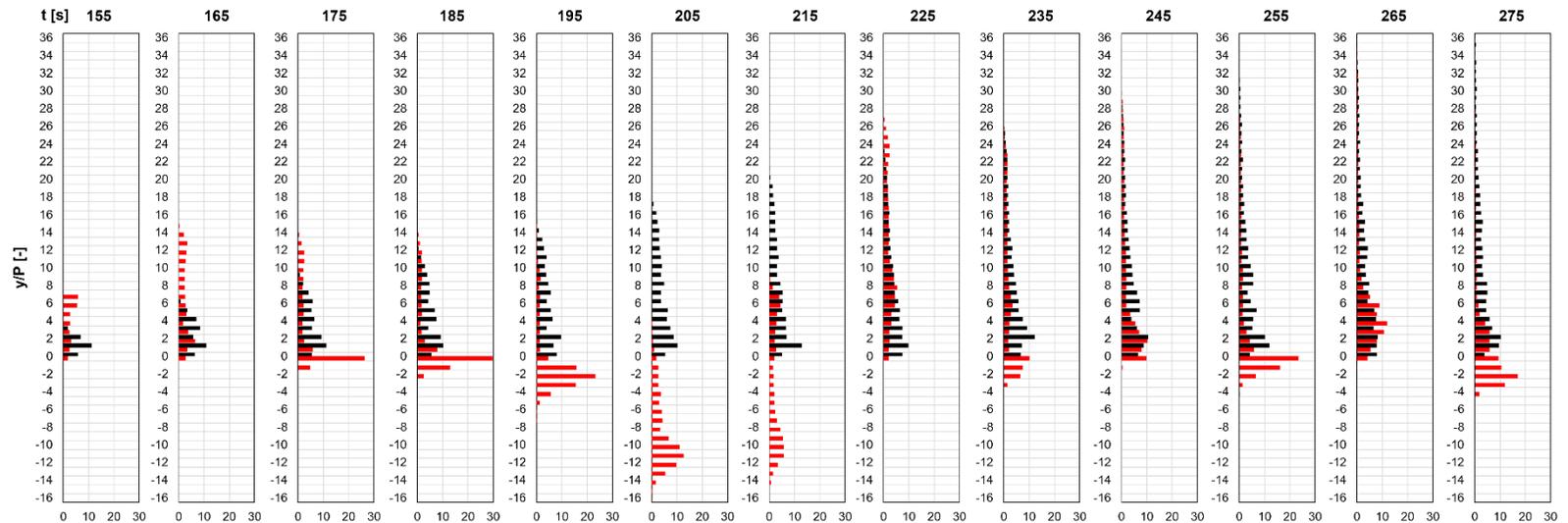
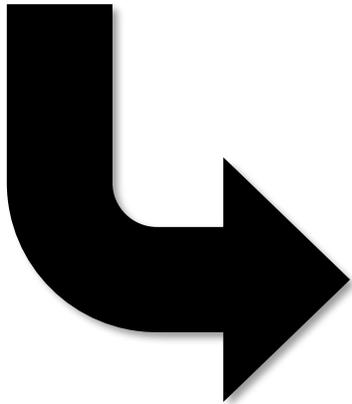
## Velocity time series at the propulsion center



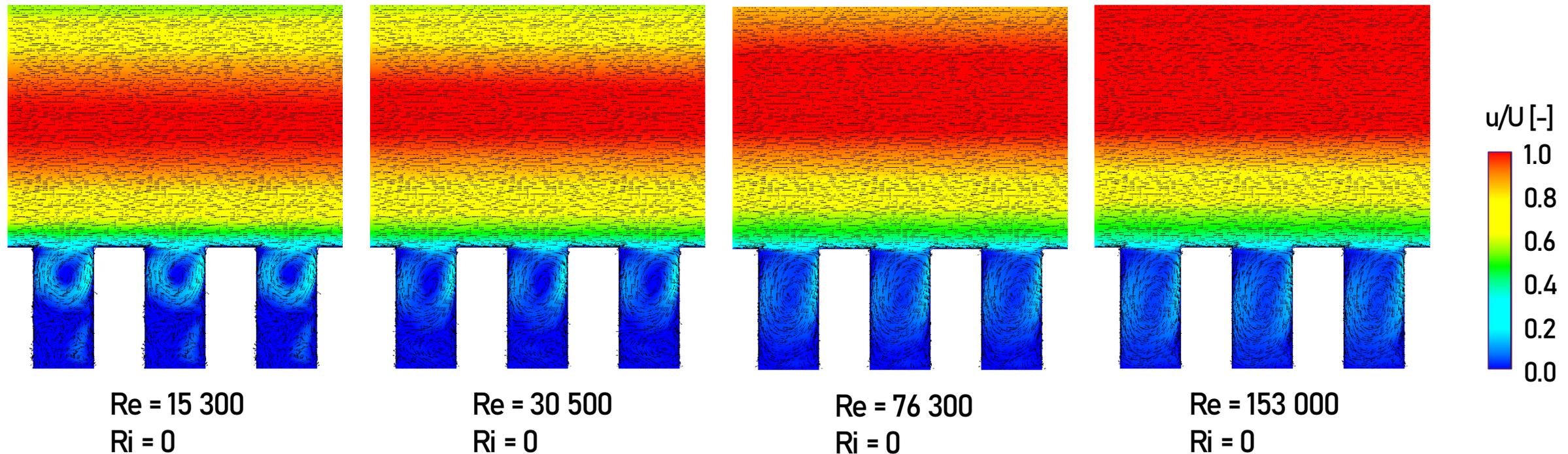
## Plume shapes over the first 250 canyons (bird's eye view)



## Lateral particle distributions in the first canyons over time



# The effect of the Reynolds number



$$U_{ref} = 0.187 \dots 1.87 \text{ [m/s]}$$
$$\Delta T = 0 \text{ [}^\circ\text{C]}$$

$$Re = \frac{LU_{ref}}{\nu}$$

$$Ri = \frac{gL\beta(T_{wall} - T_0)}{U_{ref}^2}$$

$$(g > 0)$$

HE, L., HANG, J., WANG, X., LIN, B., LI, X., & LAN, G. (2017). NUMERICAL INVESTIGATIONS OF FLOW AND PASSIVE POLLUTANT EXPOSURE IN HIGH-RISE DEEP STREET CANYONS WITH VARIOUS STREET ASPECT RATIOS AND VIADUCT SETTINGS. SCIENCE OF THE TOTAL ENVIRONMENT, 584, 189-206.